



**MQFL-28VE-28S**

**Single Output**

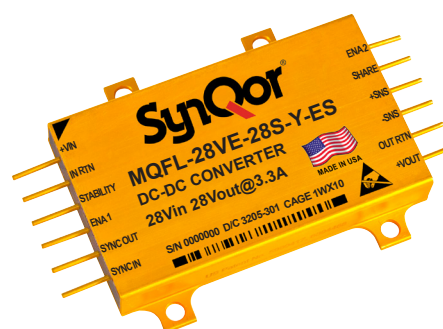
## High Reliability DC-DC Converter

<b>16-70V</b> Continuous Input	<b>5.5-80V</b> Transient Input	<b>28V</b> Output	<b>3.3A</b> Output	<b>89% @ 1.65A / 88% @ 3.3A</b> Efficiency
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**FULL POWER OPERATION: -55°C TO +125°C**

The MilQor® series of high-reliability DC-DC converters brings SynQor's field proven high-efficiency synchronous rectifier technology to the Military/Aerospace industry. SynQor's innovative QorSeal® packaging approach ensures survivability in the most hostile environments. Compatible with the industry standard format, these converters operate at a fixed frequency, have no opto-isolators, and follow conservative component derating guidelines. They are designed and manufactured to comply with a wide range of military standards.

**MilQor®**



**Meets all -704 and -1275D under-voltage transients**

### Design Process

MQFL series converters are:

- Designed for reliability per NAVSO-P3641-A guidelines
- Designed with components derated per:
  - MIL-HDBK-1547A
  - NAVSO P-3641A

### Qualification Process

MQFL series converters are qualified to:

- MIL-STD-810F
  - consistent with RTCA/DO-160E
- SynQor's First Article Qualification
  - consistent with MIL-STD-883F
- SynQor's Long-Term Storage Survivability Qualification
- SynQor's on-going life test

### In-Line Manufacturing Process

- AS9100 and ISO 9001 certified facility
- Full component traceability
- Temperature cycling
- Constant acceleration
- 24, 96, 160 hour burn-in
- Three level temperature screening

DESIGNED & MANUFACTURED IN THE USA  
FEATURING QORSEAL® HI-REL ASSEMBLY

### Features

- Fixed switching frequency
- No opto-isolators
- Parallel operation with current share
- Remote sense
- Clock synchronization
- Primary and secondary referenced enable
- Continuous short circuit and overload protection
- Input under-voltage and over-voltage shutdown

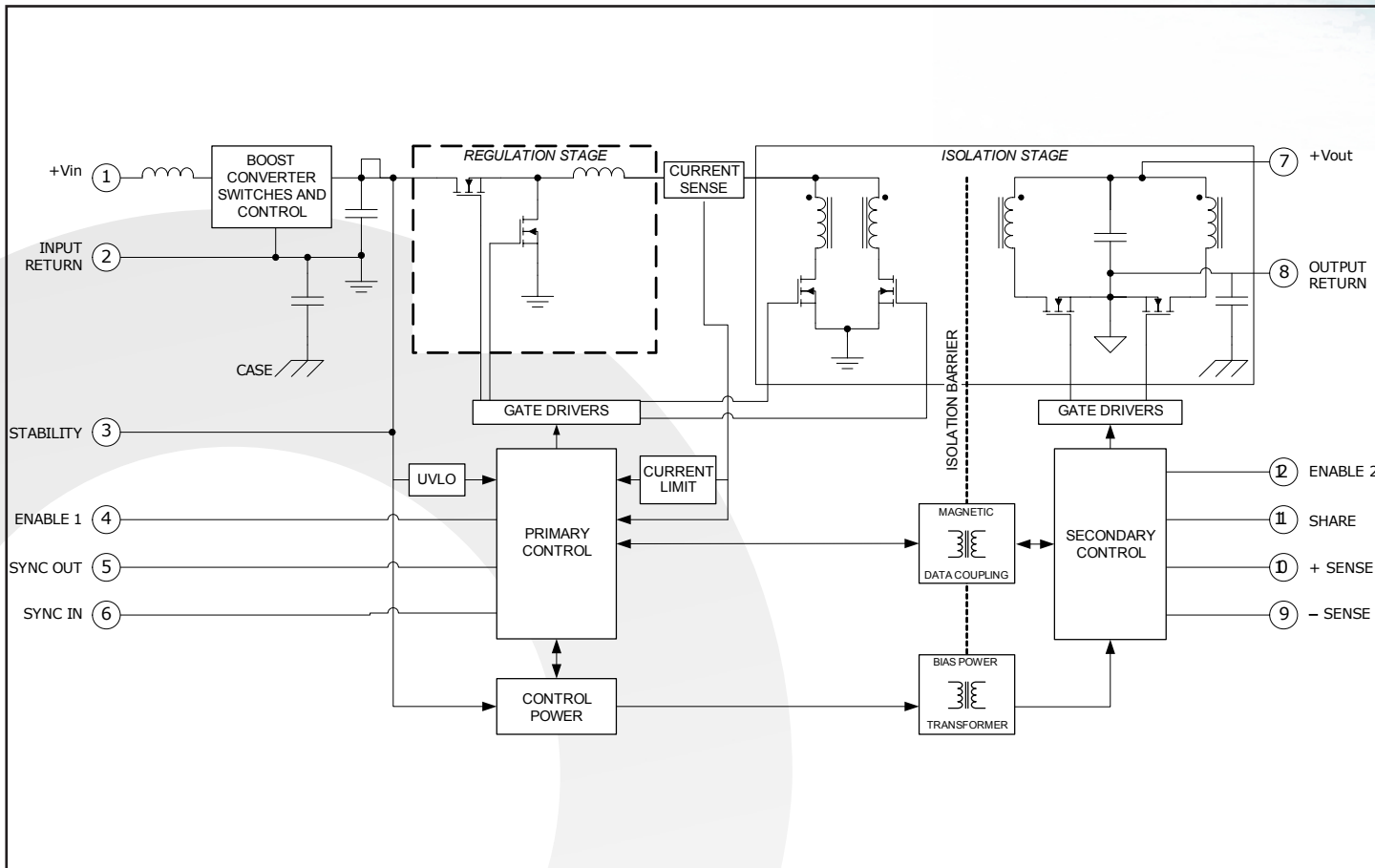
### Specification Compliance

MQFL series converters (with MQME filter) are designed to meet:

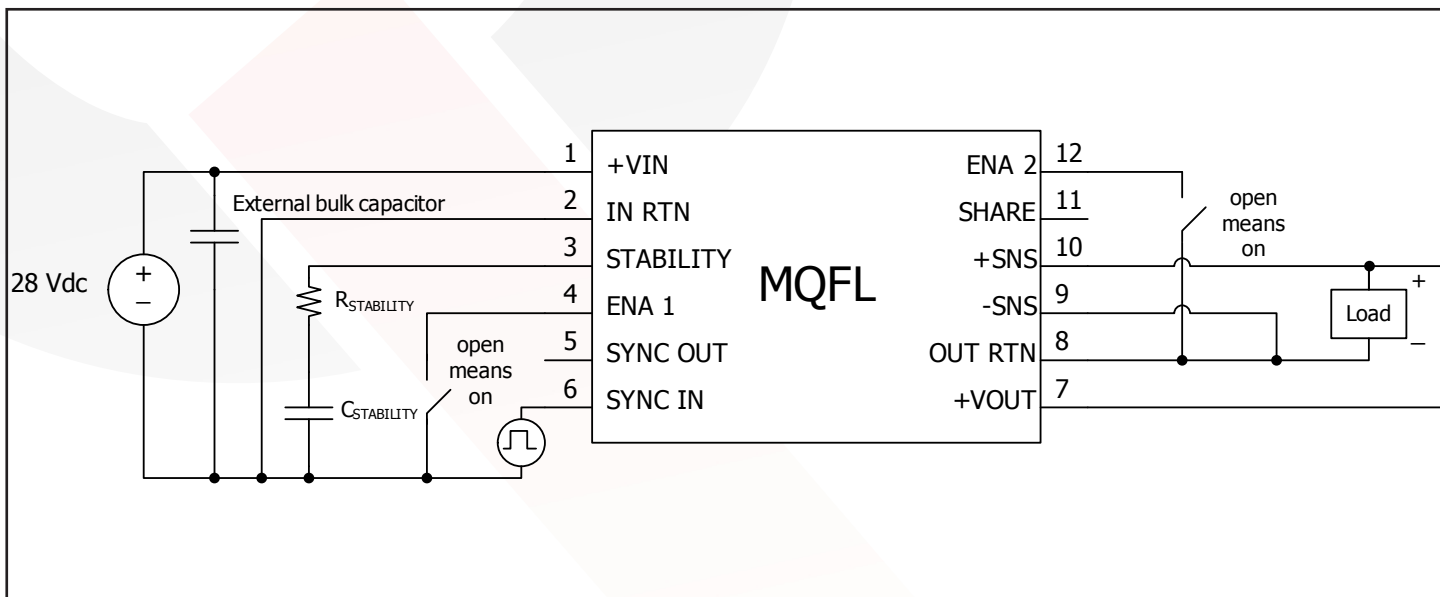
- MIL-HDBK-704-8 (A through F)
- RTCA/DO-160 Section 16, 17, 18
- MIL-STD-1275 (B, D)
- DEF-STAN 61-5 (part 6)/(5, 6)
- MIL-STD-461 (C, D, E, F)
- RTCA/DO-160(E, F, G) Section 22



### BLOCK DIAGRAM

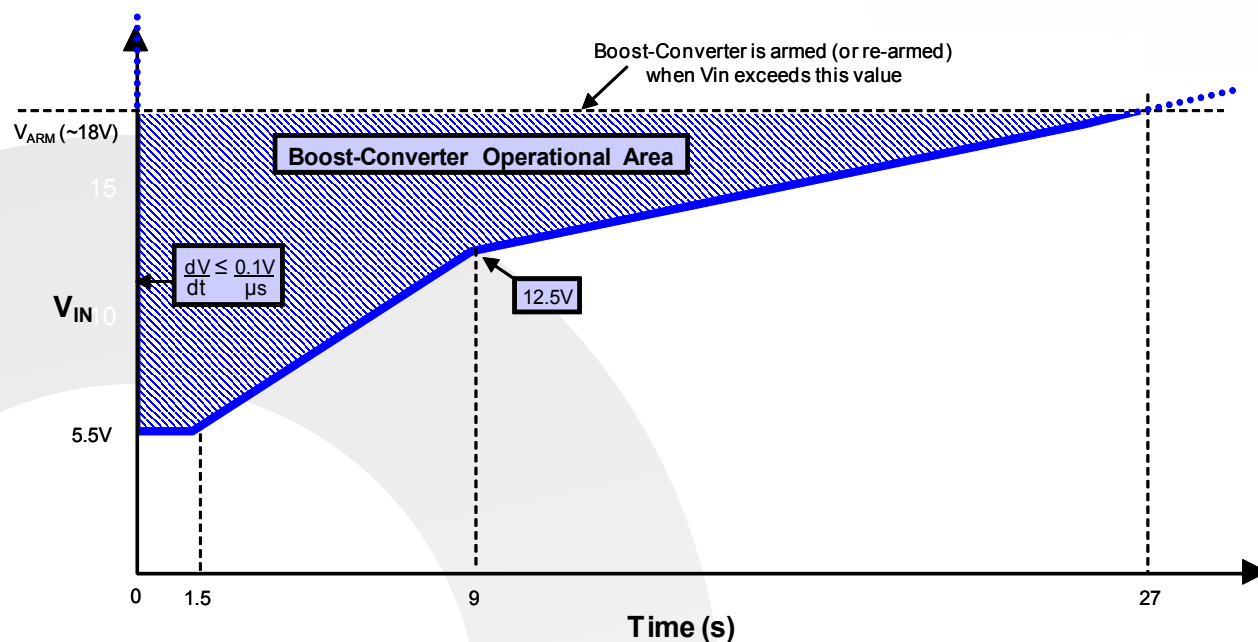


### TYPICAL CONNECTION DIAGRAM





## Under-Voltage Transient Profile



Under-Voltage Transient Profile showing when the boost-converter is guaranteed to be operational. Before the boost converter will operate, it must first be armed (or re-armed) by making  $V_{IN}$  greater than  $V_{ARM}$ .

### Note:

This Under-Voltage Transient Profile is designed to comply (with appropriate margins) with all initial-engagement surges, starting or cranking voltage transients and under-voltage surges specified in:

- MIL-STD-704-8 (A through F)
- RTCA/DO-160
- MIL-STD-1275
- DEF-STAN 61-5 (part 6)/5 (operational portions)





**MQFL-28VE-28S**

**Output: 28V**

**Current: 3.3A**

# Technical Specification

## MQFL-28VE-28S ELECTRICAL CHARACTERISTICS

Parameter	Min.	Typ.	Max.	Units	Notes & Conditions	Group A Subgroup
Specifications subject to change without notice					Vin=28V dc ±5%, Iout=3.3A, CL=0μF, free running (see Note 10) boost-converter non-operational unless otherwise specified	(see Note 13)
ABSOLUTE MAXIMUM RATINGS						
Input Voltage						
Non-Operating			100	V	See Note 1	
Operating			100	V		
Reverse Bias (Tcase = 125°C)			-0.8	V		
Reverse Bias (Tcase = -55°C)			-1.2	V		
Isolation Voltage (I/O to case, I to O)						
Continuous	-500		500	V	HB Grade Products, See Notes 2 & 16	
Transient (≤100μs)	-800		800	V		
Operating Case Temperature	-55		125	°C		
Storage Case Temperature	-65		135	°C		
Lead Temperature (20s)			300	°C		
Voltage at ENA1, ENA2	-1.2		50	V		
INPUT CHARACTERISTICS						
Operating Input Voltage Range						
	16	28	70	V	Continuous	1, 2, 3
	5.5	28	80	V	Transient, 1s; see Under-Voltage Transient Profile	
Input Under-Voltage Lockout						
Turn-On Voltage Threshold	14.75	15.50	16.00	V	See Note 3	1, 2, 3
Turn-Off Voltage Threshold	13.80	14.40	15.00	V		1, 2, 3
Lockout Voltage Hysteresis	0.50	1.10	1.80	V		
Input Over-Voltage Shutdown						
Turn-Off Voltage Threshold	90.0	95.0	100.0	V	See Note 15	
Turn-On Voltage Threshold	82.0	86.0	90.0	V		
Shutdown Voltage Hysteresis	3.0	9.0	15.0	V		
Input Filter Component Values (L\C)						
		1.0\20.2		μH\μF	Internal Values	
Maximum Input Current			7.5	A	Vin = 16V; Iout = 3.3A	See Note 5
No Load Input Current (operating)		110	160	mA		1, 2, 3
Disabled Input Current (ENA1)		2	5	mA		1, 2, 3
Disabled Input Current (ENA2)		25	50	mA		1, 2, 3
Input Terminal Current Ripple (pk-pk)		80	120	mA	Bandwidth = 100kHz – 10MHz; see Figure 14	1, 2, 3
OUTPUT CHARACTERISTICS						
Output Voltage Set Point (Tcase = 25°C)						
	27.72	28.00	28.28	V	Vout at sense leads	1
Output Voltage Set Point Over Temperature	27.60	28.00	28.40	V	"	2, 3
Output Voltage Line Regulation	-20	0	20	mV	"	1, 2, 3
Output Voltage Load Regulation	120	135	150	mV	" ; Vout @ (Iout=0 A) - Vout @ (Iout=3.3A)	1, 2, 3
Total Output Voltage Range	27.44	28.00	28.56	V	"	1, 2, 3
Output Voltage Ripple and Noise Peak to Peak		30	100	mV	Bandwidth = 10 MHz; CL=11μF	1, 2, 3
Operating Output Current Range	0		3.3	A		1, 2, 3
Operating Output Power Range	0		92.4	W		1, 2, 3
Output DC Current-Limit Inception	3.4	3.8	5.0	A	See Note 4	1, 2, 3
Short Circuit Output Current	3.7	4.1	5.6	A	Vout ≤ 1.2V	See Note 5
Back-Drive Current Limit while Enabled		1		A		1, 2, 3
Back-Drive Current Limit while Disabled		10	50	mA		1, 2, 3
Maximum Output Capacitance			3,000	μF		See Note 5
DYNAMIC CHARACTERISTICS						
Output Voltage Deviation Load Transient						
For a Pos. Step Change in Load Current	-1200	-400		mV	See Note 6	4, 5, 6
For a Neg. Step Change in Load Current		400	1200	mV	Total Iout step = 1.65A↔3.3A, 0.33A↔1.65A; CL=11μF	
Settling Time (either case)		50	200	μs	"	
Output Voltage Deviation Line Transient						
For a Pos. Step Change in Line Voltage	-800		800	mV	See Note 7	4, 5, 6
For a Neg. Step Change in Line Voltage	-800		800	mV	Vin step = 16V↔50V; CL=11μF; see Note 8	
Settling Time (either case)		250	500	μs	See Note 7	
Turn-On Transient						
Output Voltage Rise Time		6	10	ms	Vout = 2.8V→25.2V	4, 5, 6
Output Voltage Overshoot		0	2	%		See Note 5
Turn-On Delay, Rising Vin		5.5	8.0	ms	ENA1, ENA2 = 5V; see Notes 9 & 12	4, 5, 6
Turn-On Delay, Rising ENA1		3.0	6.0	ms	ENA2 = 5V; see Note 12	4, 5, 6
Turn-On Delay, Rising ENA2		1.5	3.0	ms	ENA1 = 5V; see Note 12	4, 5, 6
EFFICIENCY						
Iout = 3.3A (16Vin)	83	88		%		1, 2, 3
Iout = 1.65A (16Vin)	87	90		%		
Iout = 3.3A (28Vin)	83	88		%		
Iout = 1.65A (28Vin)	86	89		%		
Iout = 3.3A (40Vin)	82	87		%		
Iout = 1.65A (40Vin)	85	88		%		
Iout = 3.3A (70Vin)	79	84		%		



**MQFL-28VE-28S**

**Output: 28V**

**Current: 3.3A**

## Technical Specification

### MQFL-28VE-28S ELECTRICAL CHARACTERISTICS (Continued)

Parameter	Min.	Typ.	Max.	Units	Notes & Conditions	Group A Subgroup (see Note 13)
Specifications subject to change without notice						
<b>ISOLATION CHARACTERISTICS</b>						
Isolation Voltage					Dielectric strength	
Input RTN to Output RTN	500			V		1
Any Input Pin to Case	500			V		1
Any Output Pin to Case	500			V		1
Isolation Resistance (in rtn to out rtn)	100			MΩ		1
Isolation Resistance (any pin to case)	100			MΩ		1
Isolation Capacitance (in rtn to out rtn)		44		nF		1
<b>FEATURE CHARACTERISTICS</b>						
Switching Frequency (free running)	500	550	600	kHz		1, 2, 3
Synchronization Input						
Frequency Range	500		600	kHz		1, 2, 3
Logic Level High	2.0		10	V		1, 2, 3
Logic Level Low	-0.5		0.8	V		1, 2, 3
Duty Cycle	20		80	%		See Note 5
Synchronization Output						
Pull Down Current	20			mA	VSYNC OUT = 0.8V	See Note 5
Duty Cycle	25		75	%	Output connected to SYNC IN of other MQFL unit	See Note 5
Enable Control (ENA1 and ENA2)						
Off-State Voltage			0.8	V		1, 2, 3
Module Off Pulldown Current	80			μA	Current drain required to ensure module is off	See Note 5
On-State Voltage	2			V		1, 2, 3
Module On Pin Leakage Current			20	μA	I <sub>max</sub> draw from pin allowed with module still on	See Note 5
Pull-Up Voltage	3.2	4.0	4.5	V	See Figure A	1, 2, 3
Load Fault Power Dissipation		14	24	W	I <sub>out</sub> at current limit inception point; See Note 4	1
Short Circuit Power Dissipation		16	24	W	V <sub>out</sub> ≤ 1.2V	1
<b>BOOST-CONVERTER OPERATION</b>						
Input Voltage Arming Value	17.5	18.0	18.8	V		1, 2, 3
Switching Frequency	600	670	740	kHz		1
Input Terminal Current Ripple (RMS)		1.4		A	V <sub>in</sub> = 16V; I <sub>out</sub> = 3.3A	
Total Converter Efficiency						
I <sub>out</sub> = 1.65A (10V <sub>in</sub> )		85		%		1
I <sub>out</sub> = 1.65A (16V <sub>in</sub> )		87		%		
I <sub>out</sub> = 3.3A (16V <sub>in</sub> )		86		%		1
<b>RELIABILITY CHARACTERISTICS</b>						
Calculated MTBF (MIL-STD-217F2)						
GB @ T <sub>case</sub> = 70°C		2200		10 <sup>3</sup> Hrs.		
AIF @ T <sub>case</sub> = 70°C		390		10 <sup>3</sup> Hrs.		
<b>WEIGHT CHARACTERISTICS</b>						
Device Weight		79		g		

#### Electrical Characteristics Notes

1. Converter will undergo input over-voltage shutdown.
2. Derate output power for continuous operation per Figure 5. 135°C is above specified operating range.
3. High or low state of input voltage must persist for about 200μs to be acted on by the lockout or shutdown circuitry.
4. Current limit inception is defined as the point where the output voltage has dropped to 90% of its nominal value.
5. Parameter not tested but guaranteed to the limit specified.
6. Load current transition time ≥ 10μs.
7. Settling time measured from start of transient to the point where the output voltage has returned to ±1% of its final value.
8. Line voltage transition time ≥ 100μs.
9. Input voltage rise time ≤ 250μs.
10. Operating the converter at a synchronization frequency above the free running frequency will cause the converter's efficiency to be slightly reduced and it may also cause a slight reduction in the maximum output current/power available. For more information consult the factory.
11. SHARE pin outputs a power failure warning pulse during a fault condition. See Current Share section of the Control Features description.
12. After a disable or fault event, module is inhibited from restarting for 300ms. See Shut Down section of the Control Features description.
13. Only the ES and HB grade products are tested at three temperatures. The C- grade products are tested at one temperature. Please refer to the Construction and Environmental Stress Screening Options table for details.
14. These derating curves apply for the ES and HB grade products. The C- grade product has a maximum case temperature of 70°C.
15. Input Over Voltage Shutdown test is run at no load, full load is beyond derating condition and could cause damage at 125°C.
16. The specified operating case temperature for ES grade products is -45°C to 100°C. The specified operating case temperature for C- grade products is 0°C to 70°C.

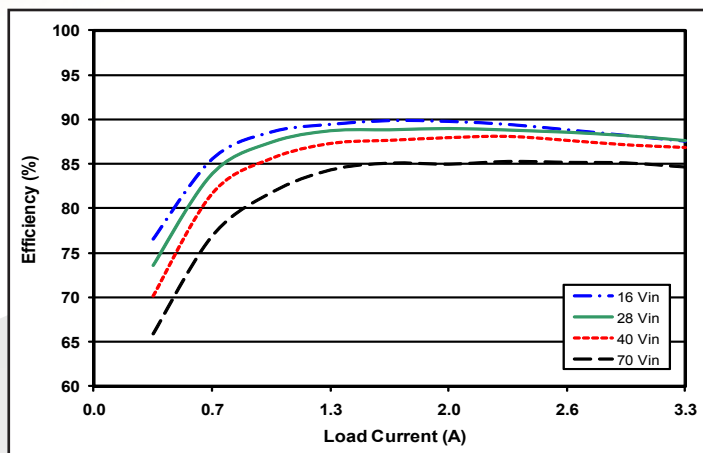


Figure 1: Efficiency at nominal output voltage vs. load current for minimum, nominal, and maximum input voltage at Tcase=25°C.

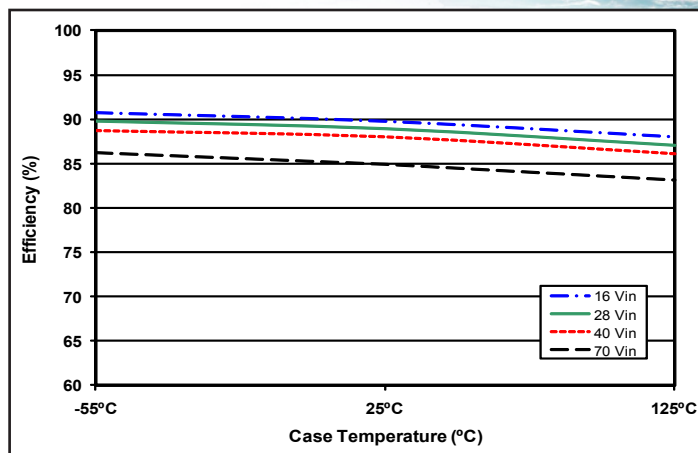


Figure 2: Efficiency at nominal output voltage and 60% rated power vs. case temperature for input voltage of 16V, 28V, and 70V.

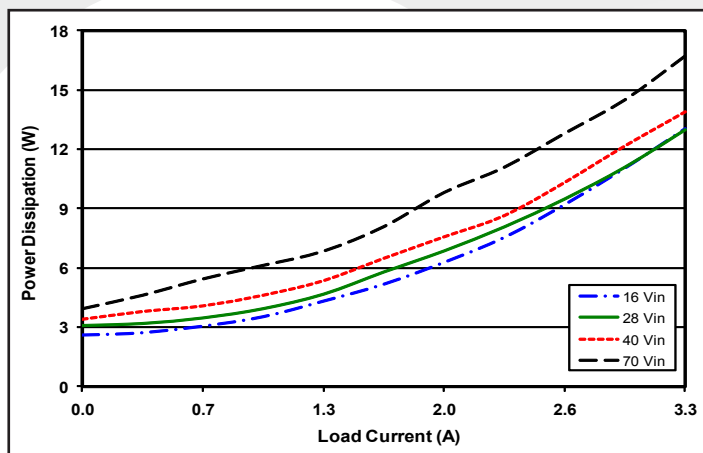


Figure 3: Power dissipation at nominal output voltage vs. load current for minimum, nominal, and maximum input voltage at Tcase=25°C.

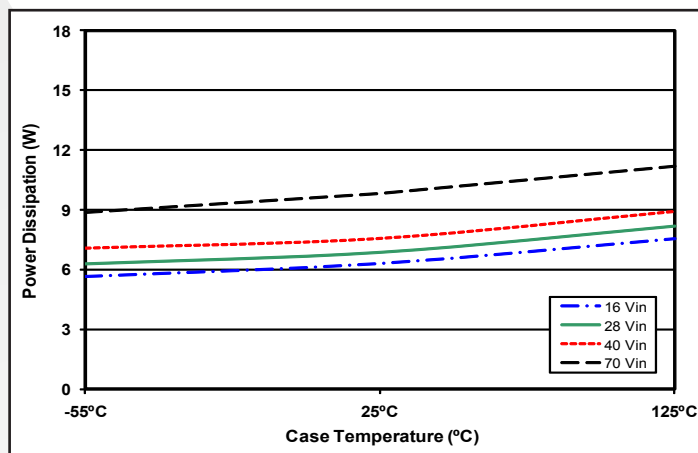


Figure 4: Power dissipation at nominal output voltage and 60% rated power vs. case temperature for input voltage of 16V, 28V, and 70V.

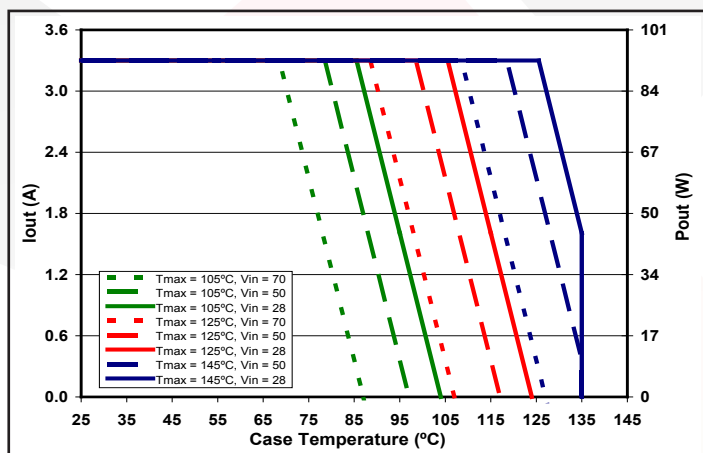


Figure 5: Output Current / Output Power derating curve as a function of Tcase and the Maximum desired power MOSFET junction temperature at Vin = 28V (see Note 14).

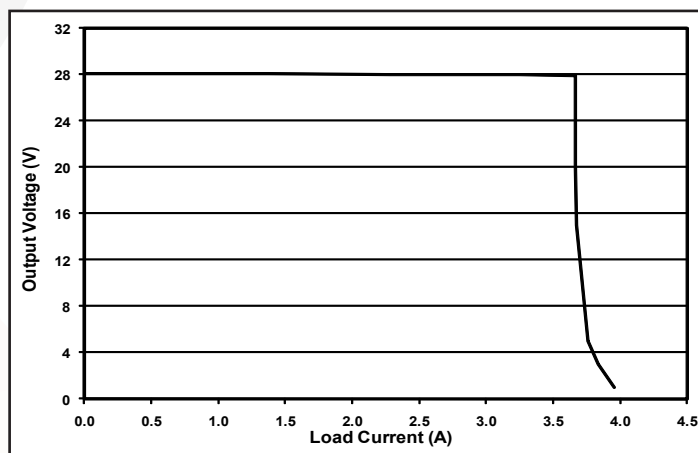


Figure 6: Output voltage vs. load current showing typical current limit curves at Vin = 28V.



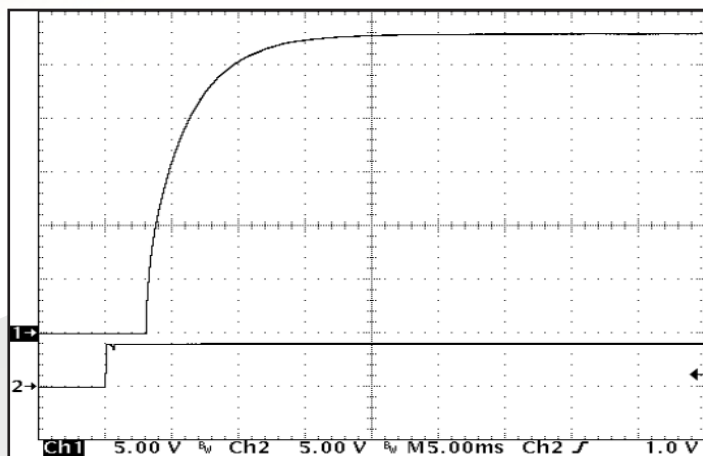


Figure 7: Turn-on transient at full resistive load and zero output capacitance initiated by ENA1. Input voltage pre-applied. Ch 1: Vout (5V/div). Ch 2: ENA1 (5V/div).

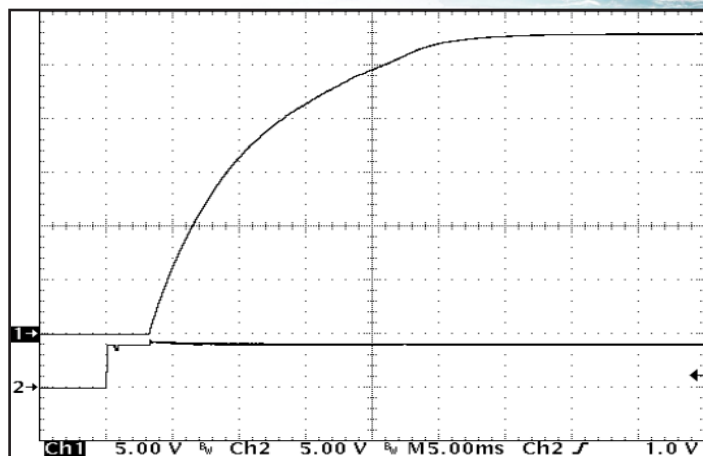


Figure 8: Turn-on transient at full resistive load and 3mF output capacitance initiated by ENA1. Input voltage pre-applied. Ch 1: Vout (5V/div). Ch 2: ENA1 (5V/div).

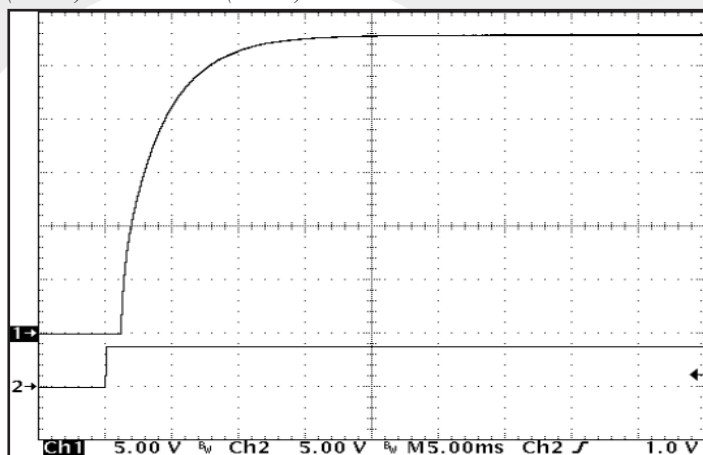


Figure 9: Turn-on transient at full resistive load and zero output capacitance initiated by ENA2. Input voltage pre-applied. Ch 1: Vout (5V/div). Ch 2: ENA2 (5V/div).

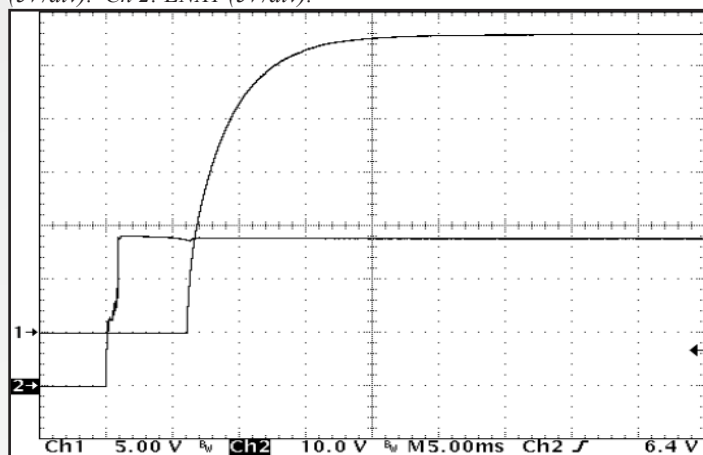


Figure 10: Turn-on transient at full resistive load and zero output capacitance initiated by Vin. ENA1 and ENA2 both previously high. Ch 1: Vout (5V/div). Ch 2: Vin (10V/div).

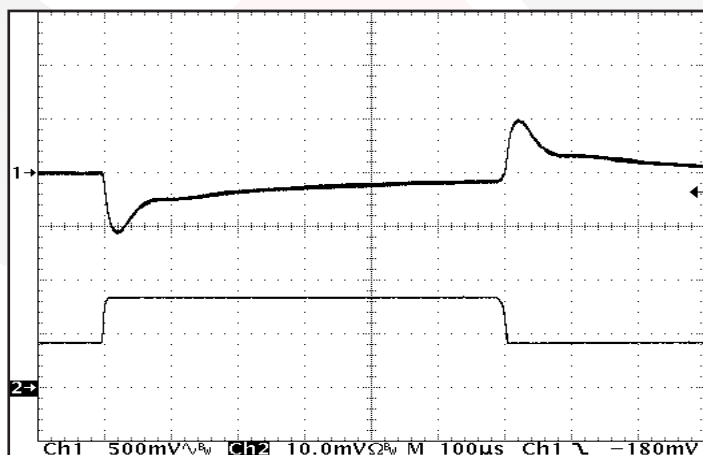


Figure 11: Output voltage response to step-change in load current 50%-100%-50% of Iout (max). Load cap: 1μF ceramic cap and 10μF, 100mΩ ESR tantalum cap. Ch 1: Vout (500mV/div). Ch 2: Iout (2A/div).

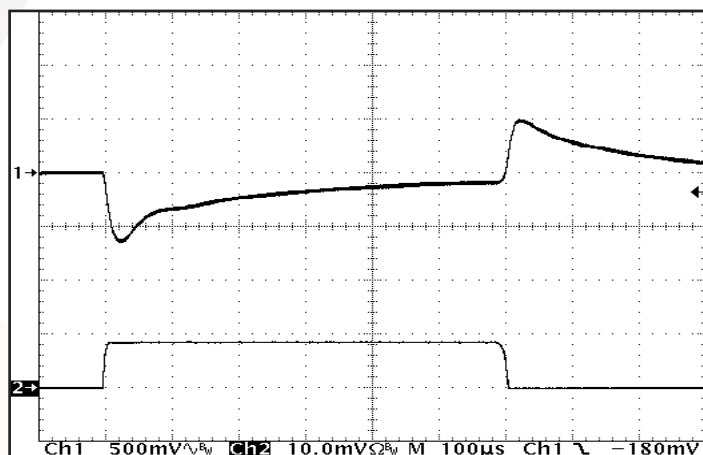


Figure 12: Output voltage response to step-change in load current 0%-50%-0% of Iout (max). Load cap: 1μF ceramic cap and 10μF, 100mΩ ESR tantalum cap. Ch 1: Vout (500mV/div). Ch 2: Iout (2A/div).

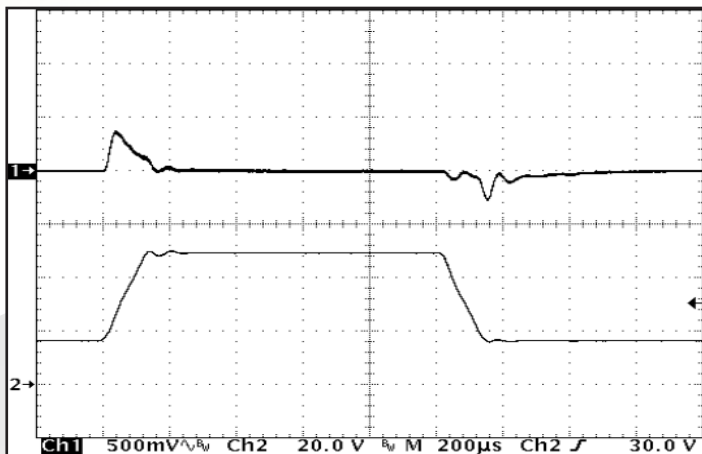


Figure 13: Output voltage response to step-change in input voltage (16V - 50V - 16V). Load cap: 10 $\mu$ F, 100m $\Omega$  ESR tantalum cap and 1 $\mu$ F ceramic cap. Ch 1: Vout (500mV/div). Ch 2: Vin (20V/div).

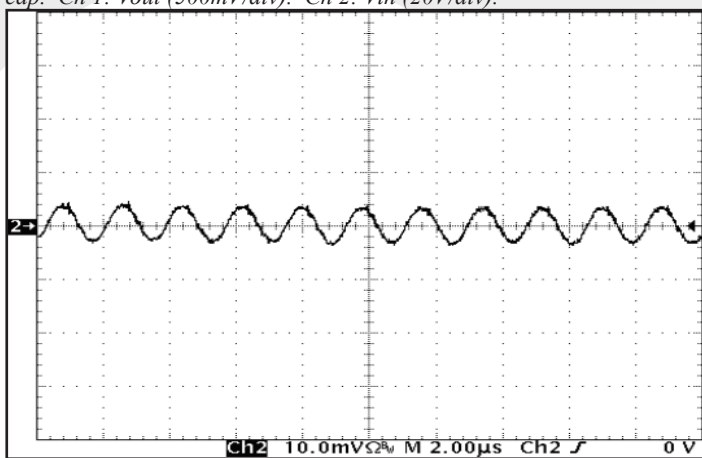


Figure 15: Input terminal current ripple,  $i_c$ , at full rated output current and nominal input voltage with SynQor MQ filter module (50mA/div). Bandwidth: 20MHz. See Figure 14.

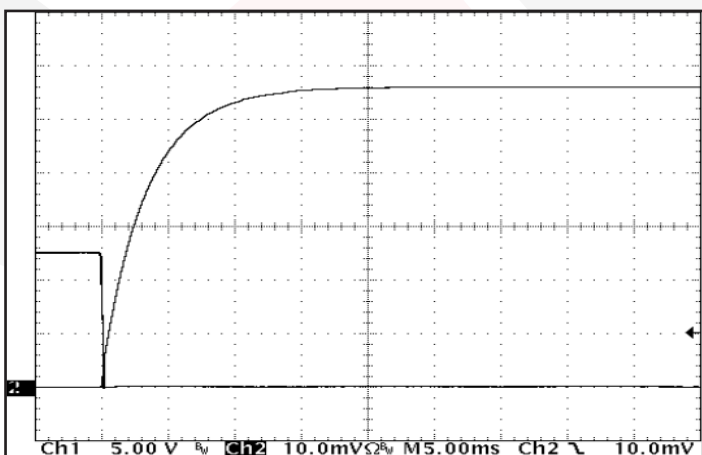


Figure 17: Rise of output voltage after the removal of a short circuit across the output terminals. Ch 1: Vout (5V/div). Ch 2: Iout (2A/div).

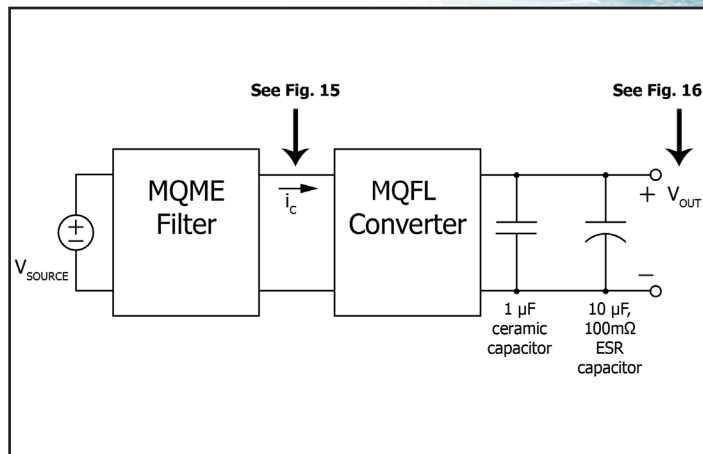


Figure 14: Test set-up diagram showing measurement points for Input Terminal Ripple Current (Figure 15) and Output Voltage Ripple (Figure 16).

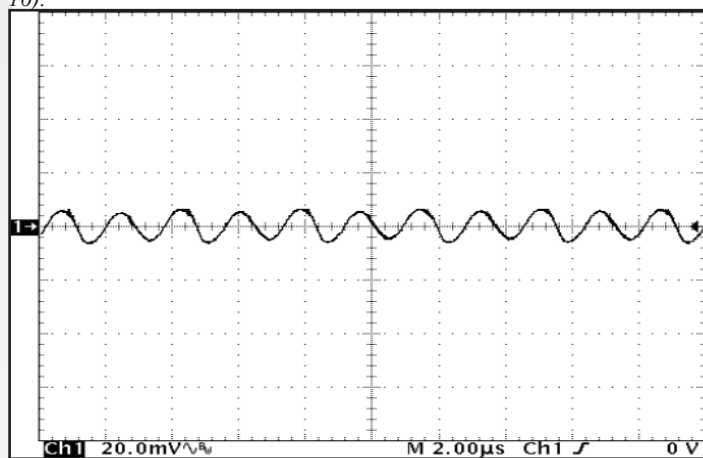


Figure 16: Output voltage ripple, Vout, at nominal input voltage and rated load current (20mV/div). Load capacitance: 1 $\mu$ F ceramic capacitor and 10 $\mu$ F tantalum capacitor. Bandwidth: 10MHz. See Figure 14.

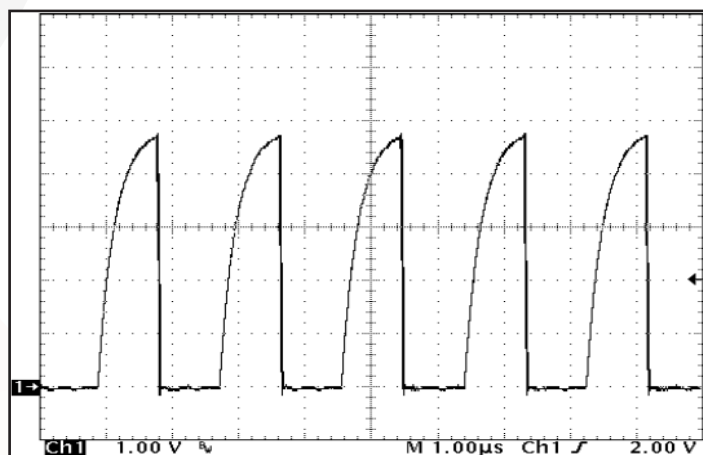


Figure 18: SYNC OUT vs. time, driving SYNC IN of a second SynQor MQFL converter. Ch1: SYNC OUT: (1V/div).



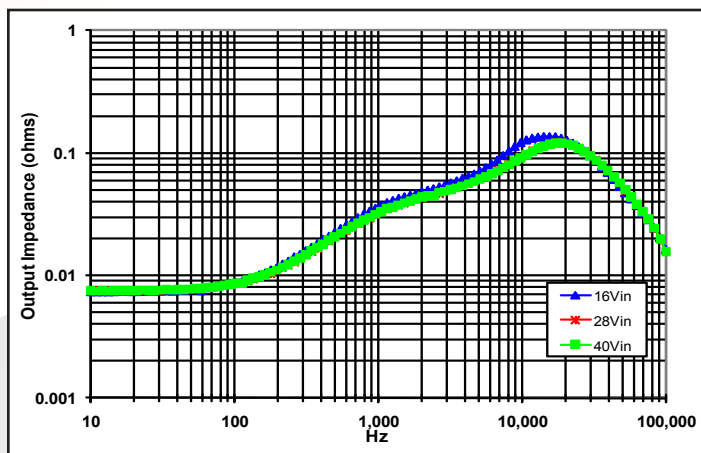


Figure 19: Magnitude of incremental output impedance ( $Z_{out} = v_{out}/i_{out}$ ) for minimum, nominal, and maximum input voltage at full rated power.

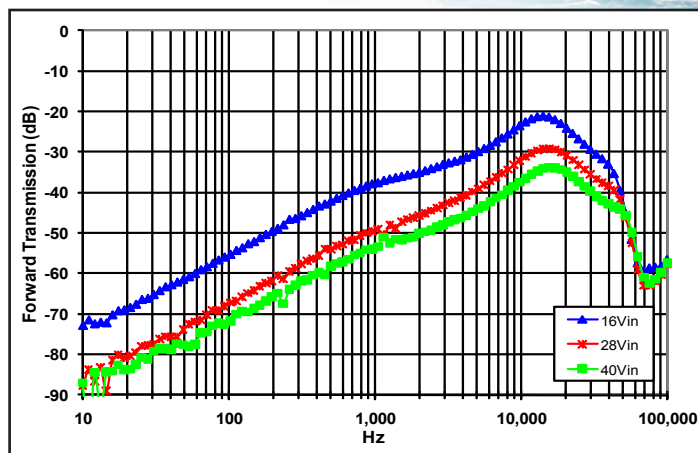


Figure 20: Magnitude of incremental forward transmission ( $FT = v_{out}/v_{in}$ ) for minimum, nominal, and maximum input voltage at full rated power.

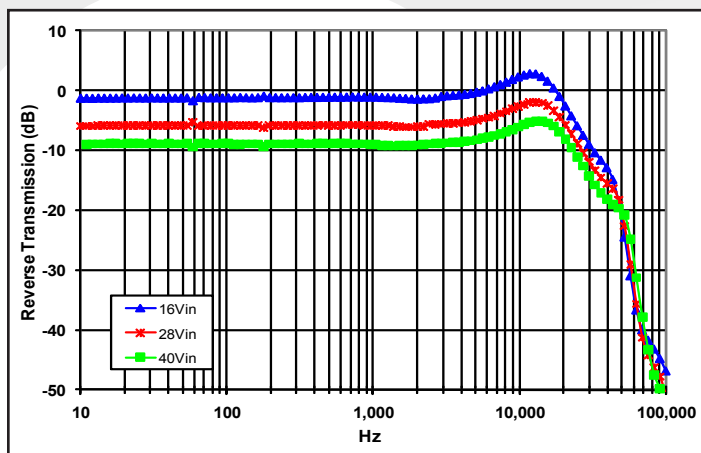


Figure 21: Magnitude of incremental reverse transmission ( $RT = i_{in}/i_{out}$ ) for minimum, nominal, and maximum input voltage at full rated power.

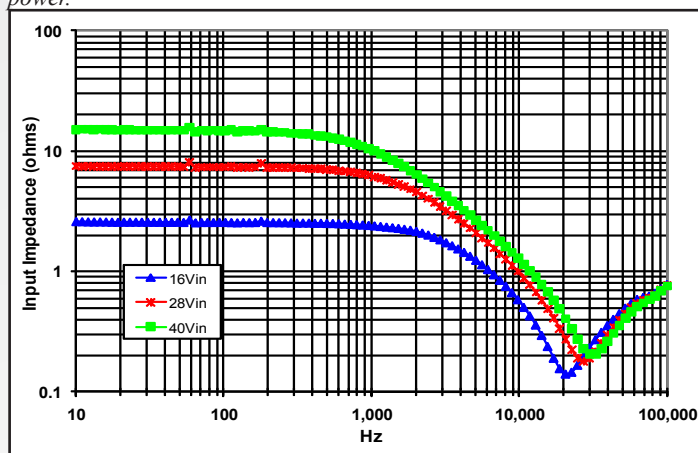


Figure 22: Magnitude of incremental input impedance ( $Z_{in} = v_{in}/i_{in}$ ) for minimum, nominal, and maximum input voltage at full rated power.

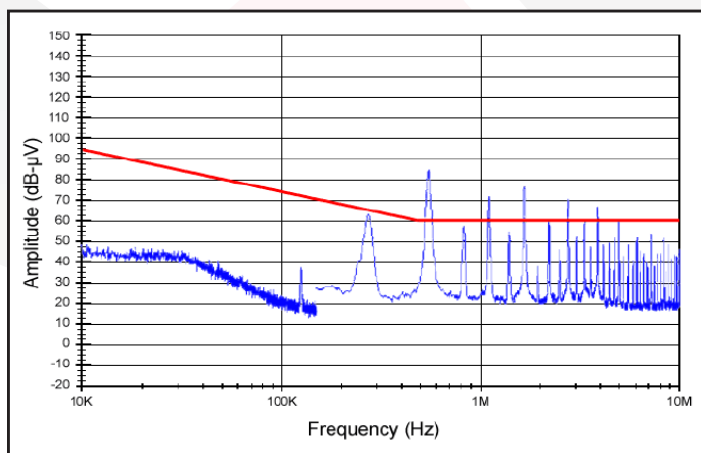


Figure 23: High frequency conducted emissions of standalone MQFL-28-05S, 5Vout module at 120W output, as measured with Method CE102. Limit line shown is the 'Basic Curve' for all applications with a 28V source.

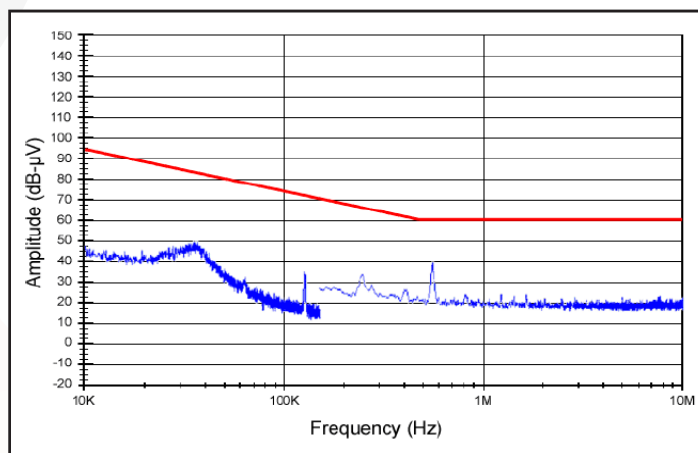


Figure 24: High frequency conducted emissions of MQFL-28-05S, 5Vout module at 120W output with MQME-28-P filter, as measured with Method CE102. Limit line shown is the 'Basic Curve' for all applications with a 28V source.



## BASIC OPERATION AND FEATURES

The MQFL DC-DC converter uses a two-stage power conversion topology. The first, or regulation, stage is a buck-converter that keeps the output voltage constant over variations in line, load, and temperature. The second, or isolation, stage uses transformers to provide the functions of input/output isolation and voltage transformation to achieve the output voltage required.

In the MQFL-28VE series of converters the regulation stage is preceded by a boost-converter that permits these converters to operate through various Military and Aircraft under-voltage transients. Further discussion of this feature can be found later in these notes.

Both the regulation and the isolation stages switch at a fixed frequency for predictable EMI performance. The isolation stage switches at one half the frequency of the regulation stage, but due to the push-pull nature of this stage it creates a ripple at double its switching frequency. As a result, both the input and the output of the converter have a fundamental ripple frequency of about 550 kHz in the free-running mode.

Rectification of the isolation stage's output is accomplished with synchronous rectifiers. These devices, which are MOSFETs with a very low resistance, dissipate far less energy than would Schottky diodes. This is the primary reason why the MQFL converters have such high efficiency, particularly at low output voltages.

Besides improving efficiency, the synchronous rectifiers permit operation down to zero load current. There is no longer a need for a minimum load, as is typical for converters that use diodes for rectification. The synchronous rectifiers actually permit a negative load current to flow back into the converter's output terminals if the load is a source of short or long term energy. The MQFL converters employ a "back-drive current limit" to keep this negative output terminal current small.

There is a control circuit on both the input and output sides of the MQFL converter that determines the conduction state of the power switches. These circuits communicate with each other across the isolation barrier through a magnetically coupled device. No opto-isolators are used.

A separate bias supply provides power to both the input and output control circuits. Among other things, this bias supply permits the converter to operate indefinitely into a short circuit and to avoid a hiccup mode, even under a tough start-up condition.

An input under-voltage lockout feature with hysteresis is provided, as well as an input over-voltage shutdown. There is also an output current limit that is nearly constant as the load impedance decreases to a short circuit (i.e., there is not fold-back or fold-forward characteristic to the output current under this condition). When a load fault is removed, the output voltage rises exponentially to its nominal value without an overshoot.

The MQFL converter's control circuit does not implement an output over-voltage limit or an over-temperature shutdown.

The following sections describe the use and operation of additional control features provided by the MQFL converter.

## UNDER-VOLTAGE TRANSIENTS

The MQFL-28VE series of DC-DC converters incorporate a special "boost-converter" stage that permits the converters to deliver full power through transients where its input voltage falls to as low as 5.5 V. Normally, the boost-converter is non-operational, and the converter's input voltage is passed directly to its pre-regulation stage (see the Block Diagram). When an under-voltage transient occurs, the boost-converter becomes operational, and it steps-up the input voltage to a value greater than 16 V so that the nominal output voltage can be sustained.

It is important to note that the boost-converter stage must first become "armed" before it can become operational. This "arming" occurs when the converter's input voltage exceeds approximately 18 V. The boost-converter then becomes operational whenever the input voltage drops below the arming voltage, and it will remain operational as long as the input voltage remains within the region shown in the Under-Voltage Transient Profile Page. If the input voltage drops below this transient profile, the boost-converter stage is not guaranteed to continue operating (it may, but it will protect itself from excessive stresses). Once the boost-converter stops operating, the converter's input voltage will be reconnected directly to the input of the pre-regulator stage. The output voltage will therefore collapse unless the input voltage is 16 V, or greater.

Note: the boost-converter will not become re-armed for the next transient unless the input voltage once again exceeds approximately 18 V.

The transient profile shown on the Under-Voltage Transient Profile page is designed to comply (with appropriate margins) with all initial-engagement surges, starting or cranking voltage transients, and under-voltage surges specified in:

- MIL-STD-704-8 (A through F)
- RTCA/DO-160
- MIL-STD-1275
- DEF-STAN 61-5 (Part 6)/5 (operational portions)

Any input voltage transient that fits within the Under-Voltage Transient Profile can be repeated after a delay that is at least four times longer than the duration of the previous transient.

During the time when the boost-converter stage is operational, the converter's efficiency is reduced and the input ripple current is increased. The lower the input voltage, the more these parameters are affected.





**MQFL-28VE-28S**

**Output: 28V**

**Current: 3.3A**

## Application Section

Usually the converter has an EMI filter upstream of it, and the source voltage is connected to the input of this EMI filter. When, during compliance testing, the source voltage goes low during an under-voltage transient, the input to the converter will go even lower. This is because the inductance of the EMI filter (as well as the parasitic source inductance) will cause an oscillatory ring with the bulk capacitor. With the bulk capacitor that is present in an MQME-28 filter, the peak of this under-voltage ring may be approximately 2 volts if the source voltage drops to 6 V (it will be smaller than this at a higher transient source voltage due to the lower current drawn by the converter). As a result, it is necessary to add extra bulk capacitor across the converter's input pins if the source voltage is going to drop to 6 V, as it does for MIL-STD-704(A) or MIL-STD-1275D. It is recommended that a 100  $\mu\text{F}$ /0.25 W ESR capacitor be connected across the input pins of the converter be used as a starting point. For MIL-STD-704(B-F), where the source voltage drops to only 7 V, a 47  $\mu\text{F}$  hold-up capacitor would be a good starting point. The exact amount of capacitance required depends on the application (source inductance, load power, rate of fall of the source voltage, etc). Please consult the factory if further assistance is required.

Because input system stability is harder to maintain as the input voltage gets lower, the MQFL-28VE series converters are designed to give external access to the voltage node between the boost-converter and the pre-regulator stages. This access, at the "STABILITY" pin (pin 3), permits the user to add a stabilizing bulk capacitor with series resistance to this node. Since the voltage at this node stays above 16 V, the amount of capacitance required is much less than would be required on the converter's input pins where the voltage might drop as low as 5.5 V. It is recommended that a 22  $\mu\text{F}$  capacitor with an ESR of about 1 W be connected between the STABILITY pin and the INPUT RETURN pin (pin 2). Without this special connection to the internal node of the converter, a 300  $\mu\text{F}$  stabilizing bulk capacitor would have been required across the converter's input pins.

Another advantage of the STABILITY pin is that it provides a voltage source that stays above 16 V when the under-voltage transient occurs. This voltage source might be useful for other circuitry in the system.

## CONTROL FEATURES

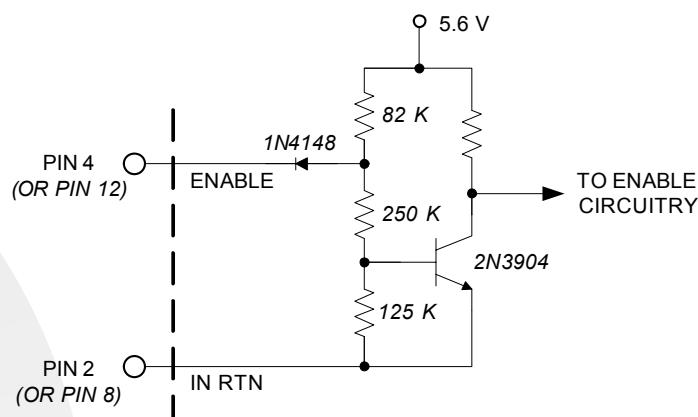
**ENABLE:** The MQFL converter has two enable pins. Both must have a logic high level for the converter to be enabled. A logic low on either pin will inhibit the converter.

The ENA1 pin (pin 4) is referenced with respect to the converter's input return (pin 2). The ENA2 pin (pin 12) is referenced with respect to the converter's output return (pin 8). This permits the converter to be inhibited from either the input or the output side.

Regardless of which pin is used to inhibit the converter, the regulation and the isolation stages are turned off. However, when the converter is inhibited through the ENA1 pin, the bias

supply is also turned off, whereas this supply remains on when the converter is inhibited through the ENA2 pin. A higher input standby current therefore results in the latter case.

Both enable pins are internally pulled high so that an open connection on both pins will enable the converter. Figure A shows the equivalent circuit looking into either enable pins. It is TTL compatible.



**Figure A:** Circuit diagram shown for reference only, actual circuit components may differ from values shown for equivalent circuit.

**SHUT DOWN:** The MQFL converter will shut down in response to only four conditions: ENA1 input low, ENA2 input low, VIN input below under-voltage lockout threshold, or VIN input above over-voltage shutdown threshold. Following a shutdown event, there is a startup inhibit delay which will prevent the converter from restarting for approximately 300 ms. After the 300 ms delay elapses, if the enable inputs are high and the input voltage is within the operating range, the converter will restart. If the VIN input is brought down to nearly 0 V and back into the operating range, there is no startup inhibit, and the output voltage will rise according to the "Turn-On Delay, Rising Vin" specification.

**REMOTE SENSE:** The purpose of the remote sense pins is to correct for the voltage drop along the conductors that connect the converter's output to the load. To achieve this goal, a separate conductor should be used to connect the +SENSE pin (pin 10) directly to the positive terminal of the load, as shown in the connection diagram on Page 2. Similarly, the -SENSE pin (pin 9) should be connected through a separate conductor to the return terminal of the load.

**NOTE:** Even if remote sensing of the load voltage is not desired, the +SENSE and the -SENSE pins must be connected to +Vout (pin 7) and OUTPUT RETURN (pin 8), respectively, to get proper regulation of the converter's output. If they are left open, the converter will have an output voltage that is approximately 200 mV higher than its specified value. If only the +SENSE pin is left open, the output voltage will be approximately 25 mV too high.





**MQFL-28VE-28S**

**Output: 28V**

**Current: 3.3A**

## Application Section

Inside the converter, +SENSE is connected to +Vout with a resistor value from 100 W to 301 W, depending on output voltage, and -SENSE is connected to OUTPUT RETURN with a 10 W resistor.

It is also important to note that when remote sense is used, the voltage across the converter's output terminals (pins 7 and 8) will be higher than the converter's nominal output voltage due to resistive drops along the connecting wires. This higher voltage at the terminals produces a greater voltage stress on the converter's internal components and may cause the converter to fail to deliver the desired output voltage at the low end of the input voltage range at the higher end of the load current and temperature range. Please consult the factory for details.

**SYNCHRONIZATION:** The MQFL converter's regulation and isolation stage switching frequencies can be synchronized to an external frequency source that is in the 500 kHz to 600 kHz range. The boost-converter stage is free-running at about 670 kHz while it is operational, and is not affected by synchronization signals. A pulse train at the desired frequency should be applied to the SYNC IN pin (pin 6) with respect to the INPUT RETURN (pin 2). This pulse train should have a duty cycle in the 20% to 80% range. Its low value should be below 0.8 V to be guaranteed to be interpreted as a logic low, and its high value should be above 2.0 V to be guaranteed to be interpreted as a logic high. The transition time between the two states should be less than 300ns.

If the MQFL converter is not to be synchronized, the SYNC IN pin should be left open circuit. The converter will then operate in its free-running mode at a frequency of approximately 550 kHz.

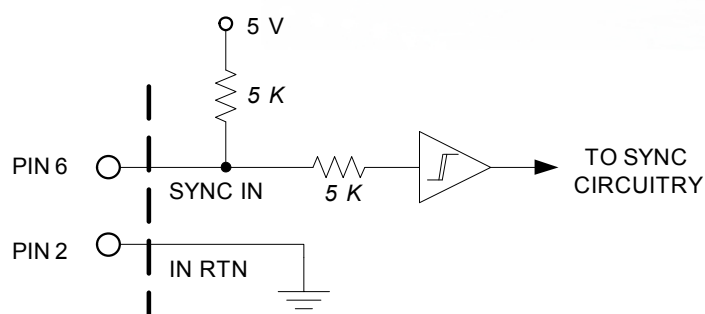
If, due to a fault, the SYNC IN pin is held in either a logic low or logic high state continuously, the MQFL converter will revert to its free-running frequency.

The MQFL converter also has a SYNC OUT pin (pin 5). This output can be used to drive the SYNC IN pins of as many as ten (10) other MQFL converters. The pulse train coming out of SYNC OUT has a duty cycle of 50% and a frequency that matches the switching frequency of the converter with which it is associated. This frequency is either the free-running frequency if there is no synchronization signal at the SYNC IN pin, or the synchronization frequency if there is.

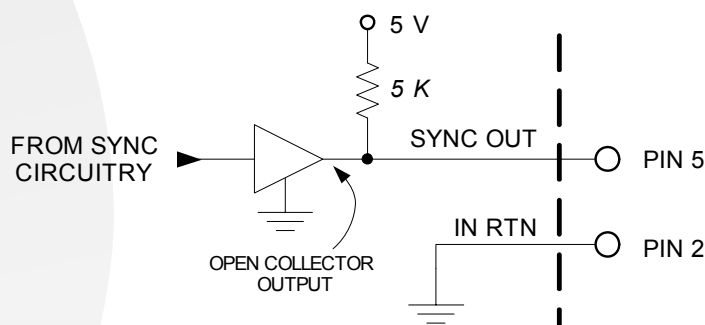
The SYNC OUT signal is available only when the voltage at the STABILITY pin (pin 3) is above approximately 12 V and when the converter is not inhibited through the ENA1 pin. An inhibit through the ENA2 pin will not turn the SYNC OUT signal off.

**NOTE:** An MQFL converter that has its SYNC IN pin driven by the SYNC OUT pin of a second MQFL converter will have its start of its switching cycle delayed approximately 180 degrees relative to that of the second converter.

Figure B shows the equivalent circuit looking into the SYNC IN pin. Figure C shows the equivalent circuit looking into the SYNC OUT pin.



**Figure B:** Equivalent circuit looking into the SYNC IN pin with respect to the IN RTN (input return) pin.



**Figure C:** Equivalent circuit looking into SYNC OUT pin with respect to the IN RTN (input return) pin.

**CURRENT SHARE:** When several MQFL converters are placed in parallel to achieve either a higher total load power or N+1 redundancy, their SHARE pins (pin 11) should be connected together. The voltage on this common SHARE node represents the average current delivered by all of the paralleled converters. Each converter monitors this average value and adjusts itself so that its output current closely matches that of the average.

Since the SHARE pin is monitored with respect to the OUTPUT RETURN (pin 8) by each converter, it is important to connect all of the converters' OUTPUT RETURN pins together through a low DC and AC impedance. When this is done correctly, the converters will deliver their appropriate fraction of the total load current to within +/- 10% at full rated load.

Whether or not converters are paralleled, the voltage at the SHARE pin could be used to monitor the approximate average current delivered by the converter(s). A nominal voltage of 1.0 V represents zero current and a nominal voltage of 2.2 V represents the maximum rated current, with a linear relationship



in between. The internal source resistance of a converter's SHARE pin signal is 2.5 kΩ. During an input voltage fault or primary disable event, the SHARE pin outputs a power failure warning pulse. The SHARE pin will go to 3 V for approximately 14 ms as the output voltage falls.

**NOTE:** Converters operating from separate input filters with reverse polarity protection (such as the MQME-28-T filter) with their outputs connected in parallel may exhibit hiccup operation at light loads. Consult factory for details.

**OUTPUT VOLTAGE TRIM:** If desired, it is possible to increase the MQFL converter's output voltage above its nominal value. To do this, use the +SENSE pin (pin 10) for this trim function instead of for its normal remote sense function, as shown in Figure D. In this case, a resistor connects the +SENSE pin to the -SENSE pin (which should still be connected to the output return, either remotely or locally). The value of the trim resistor should be chosen according to the following equation or from Figure E:

$$R_{trim} = 100 \times \frac{V_{nom}}{V_{out} - V_{nom} - 0.025}$$

where:

$V_{nom}$  = the converter's nominal output voltage,  
 $V_{out}$  = the desired output voltage (greater than  $V_{nom}$ ), and  
 $R_{trim}$  is in Ohms.

As the output voltage is trimmed up, it produces a greater voltage stress on the converter's internal components and may cause the converter to fail to deliver the desired output voltage at the low end of the input voltage range at the higher end of the load current and temperature range. Please consult the factory for details.

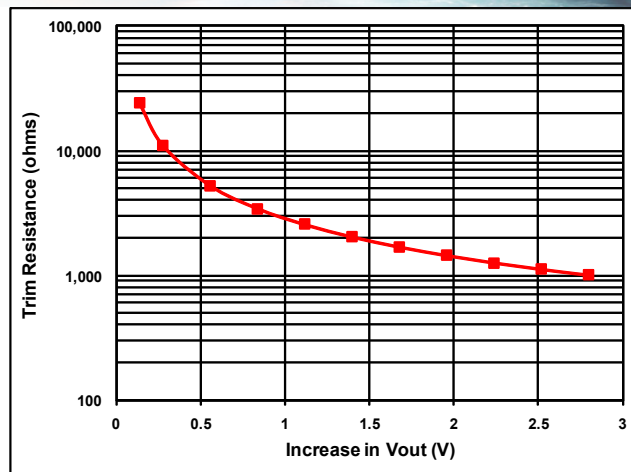


Figure E: Output Voltage Trim Graph

**INPUT UNDER-VOLTAGE LOCKOUT:** The MQFL converter has an under-voltage lockout feature that ensures the converter will be off if the input voltage is too low. This lockout only appears when the boost-converter is not operating. The threshold of input voltage at which the converter will turn on is higher than the threshold at which it will turn off. In addition, the MQFL converter will not respond to a state of the input voltage unless it has remained in that state for more than about 200 μs. This hysteresis and the delay ensure proper operation when the source impedance is high or in a noisy environment.

**INPUT OVER-VOLTAGE SHUTDOWN:** The MQFL converter also has an over-voltage feature that ensures the converter will be off if the input voltage is too high. It also has a hysteresis and time delay to ensure proper operation.

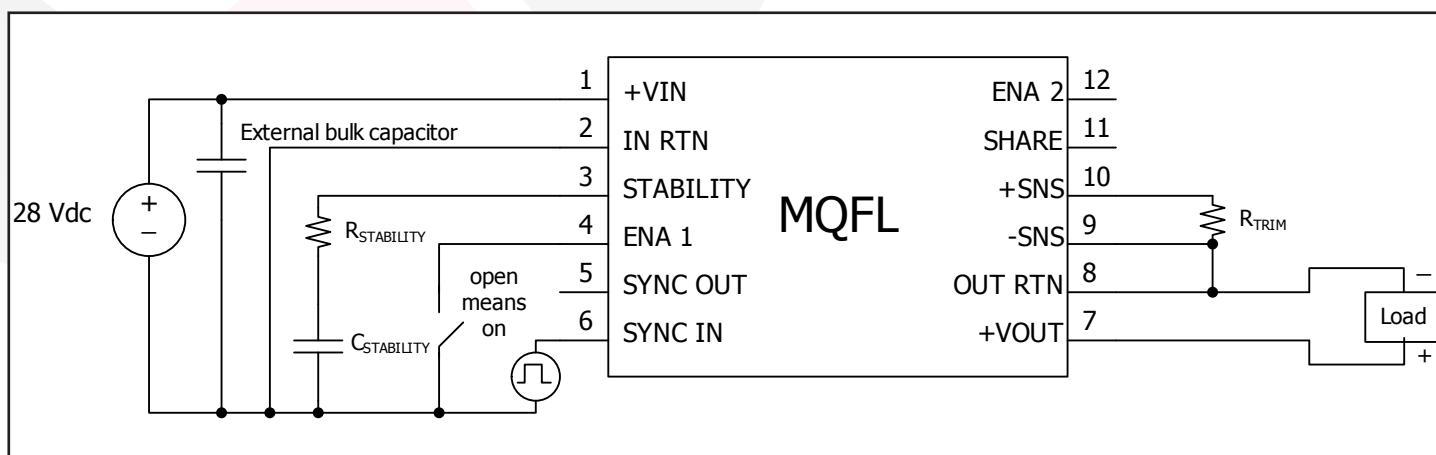


Figure D: Typical connection for output voltage trimming.



## Application Section

**BACK-DRIVE CURRENT LIMIT:** Converters that use MOSFETs as synchronous rectifiers are capable of drawing a negative current from the load if the load is a source of short- or long-term energy. This negative current is referred to as a "back-drive current".

Conditions where back-drive current might occur include paralleled converters that do not employ current sharing, or where the current share feature does not adequately ensure sharing during the startup or shutdown transitions. It can also occur when converters having different output voltages are connected together through either explicit or parasitic diodes that, while normally off, become conductive during startup or shutdown. Finally, some loads, such as motors, can return energy to their power rail. Even a load capacitor is a source of back-drive energy for some period of time during a shutdown transient.

To avoid any problems that might arise due to back-drive current, the MQFL converters limit the negative current that the converter can draw from its output terminals. The threshold for this back-drive current limit is placed sufficiently below zero so that the converter may operate properly down to zero load, but its absolute value (see the Electrical Characteristics page) is small compared to the converter's rated output current.

**THERMAL CONSIDERATIONS:** Figure 5 shows the suggested Power Derating Curves for this converter as a function of the case temperature, input voltage and the maximum desired power MOSFET junction temperature. All other components within the converter are cooler than its hottest MOSFET.

The Mil-HDBK-1547A component derating guideline calls for a maximum component temperature of 105 °C. Figure 5 therefore has one power derating curve that ensures this limit is maintained. It has been SynQor's extensive experience that reliable long-term converter operation can be achieved with a maximum component temperature of 125 °C. In extreme cases, a maximum temperature of 145 °C is permissible, but not recommended for long-term operation where high reliability is required. Derating curves for these higher temperature limits are also included in Figure 5. The maximum case temperature at which the converter should be operated is 135 °C.

When the converter is mounted on a metal plate, the plate will help to make the converter's case bottom a uniform temperature. How well it does so depends on the thickness of the plate and on the thermal conductance of the interface layer (e.g. thermal grease, thermal pad, etc.) between the case and the plate. Unless this is done very well, it is important not to mistake the plate's temperature for the maximum case temperature. It is easy for them to be as much as 5-10 °C different at full power and at high temperatures. It is suggested that a thermocouple be attached directly to the converter's case through a small hole in the plate when investigating how hot the converter is getting. Care must also be made to ensure that there is not a large thermal resistance between the thermocouple and the case due to whatever adhesive might be used to hold the thermocouple in place.

**INPUT SYSTEM INSTABILITY:** This condition can occur because any DC-DC converter appears incrementally as a negative resistance load. A detailed application note titled "Input System Instability" is available on the SynQor website which provides an understanding of why this instability arises, and shows the preferred solution for correcting it.





## CONSTRUCTION AND ENVIRONMENTAL STRESS SCREENING OPTIONS

Screening	Consistent with MIL-STD-883F	C-Grade ( specified from 0 °C to +70 °C )	ES-Grade ( specified from -45 °C to +100 °C )	HB-Grade ( specified from -55 °C to +125 °C )
Element Evaluation		No	Yes	Yes
Internal Visual	IPC-A-610 Class 3	Yes	Yes	Yes
Temperature Cycle	Method 1010	No	Condition B (-55 °C to +125 °C)	Condition C (-65 °C to +150 °C)
Constant Acceleration	Method 2001 (Y1 Direction)	No	500 g	Condition A (5000 g)
Burn-in	Method 1015	24 Hrs @ +125 °C	96 Hrs @ +125 °C	160 Hrs @ +125 °C
Final Electrical Test	Method 5005 (Group A)	+25 °C	-45, +25, +100 °C	-55, +25, +125 °C
Mechanical Seal, Thermal, and Coating Process			Full QorSeal	Full QorSeal
External Visual	Method 2009	Yes	Yes	Yes
Construction Process			QorSeal	QorSeal

MilQor® Hi-Rel converters and filters are offered in three variations of environmental stress screening options. All ES-Grade and HB-Grade MilQor Hi-Rel converters use SynQor's proprietary QorSeal® Hi-Rel assembly process that includes a Parylene-C coating of the circuit, a high performance thermal compound filler, and a nickel barrier gold plated aluminum case. Each successively higher grade has more stringent mechanical and electrical testing, as well as a longer burn-in cycle. The ES- and HB-Grades are also constructed of components that have been procured through an element evaluation process that pre-qualifies each new batch of devices.



### MIL-STD-810F Qualification Testing

MIL-STD-810F Test	Method	Description
Fungus	508.5	Table 508.5-I
Altitude	500.4 - Procedure I	Storage: 70,000 ft / 2 hr duration
	500.4 - Procedure II	Operating: 70,000 ft / 2 hr duration; Ambient Temperature
Rapid Decompression	500.4 - Procedure III	Storage: 8,000 ft to 40,000 ft
Acceleration	513.5 - Procedure II	Operating: 15 g
Salt Fog	509.4	Storage
High Temperature	501.4 - Procedure I	Storage: 135 °C / 3 hrs
	501.4 - Procedure II	Operating: 100 °C / 3 hrs
Low Temperature	502.4 - Procedure I	Storage: -65 °C / 4 hrs
	502.4 - Procedure II	Operating: -55 °C / 3 hrs
Temperature Shock	503.4 - Procedure I - C	Storage: -65 °C to 135 °C; 12 cycles
Rain	506.4 - Procedure I	Wind Blown Rain
Immersion	512.4 - Procedure I	Non-Operating
Humidity	507.4 - Procedure II	Aggravated cycle @ 95% RH (Figure 507.5-7 aggravated temp - humidity cycle, 15 cycles)
Random Vibration	514.5 - Procedure I	10 - 2000 Hz, PSD level of 1.5 g <sup>2</sup> /Hz (54.6 g <sub>rms</sub> ), duration = 1 hr/axis
Shock	516.5 - Procedure I	20 g peak, 11 ms, Functional Shock (Operating no load) (saw tooth)
	516.5 - Procedure VI	Bench Handling Shock
Sinusoidal vibration	514.5 - Category 14	Rotary wing aircraft - helicopter, 4 hrs/axis, 20 g (sine sweep from 10 - 500 Hz)
Sand and Dust	510.4 - Procedure I	Blowing Dust
	510.4 - Procedure II	Blowing Sand



# SynQor®

## Technical Specifications

**MQFL-28VE-28S**

**Output: 28V**

**Current: 3.3A**

### First Article Testing consistent with MIL-STD-883F

MIL-STD-883F Test	Method	Description
Electrical Tests	5005	
Physical Dimensions test	2016	
Resistance to Solvents test	2015.13	
Solderability test	2003.8	
Lead Integrity test	2004.5	
Salt Atmosphere test	1009.8	Condition "A"
Adhesion of Lead Finish test	2025.4	
Altitude Operation test	1001	Condition "C"
ESD Sensitivity	3015.7	Class 2
Stabilization Bake test	1008.2	Condition "C"
Vibration Fatigue test	2005.2	Condition "A"
Random Vibration test	2026	Condition "II K"
Sequential Test Group #1		
Life Test – Steady State test	1005.8	
Life Test – Intermittent Duty test	1006	
Sequential Test Group #2		
Temperature Cycle test	1010.8	Condition "C"
Constant Acceleration test	2001.2	Condition "A"
Sequential Test Group #3		
Thermal Shock test	1011.9	Condition "B"
Temperature Cycle test	1010.8	Condition "C"
Moisture Resistance test	1004.7	With Sub cycle
Sequential Test Group #4		
Mechanical Shock test	2002.4	Condition "B"
Variable Frequency Vibration test	2007.3	Condition "A"



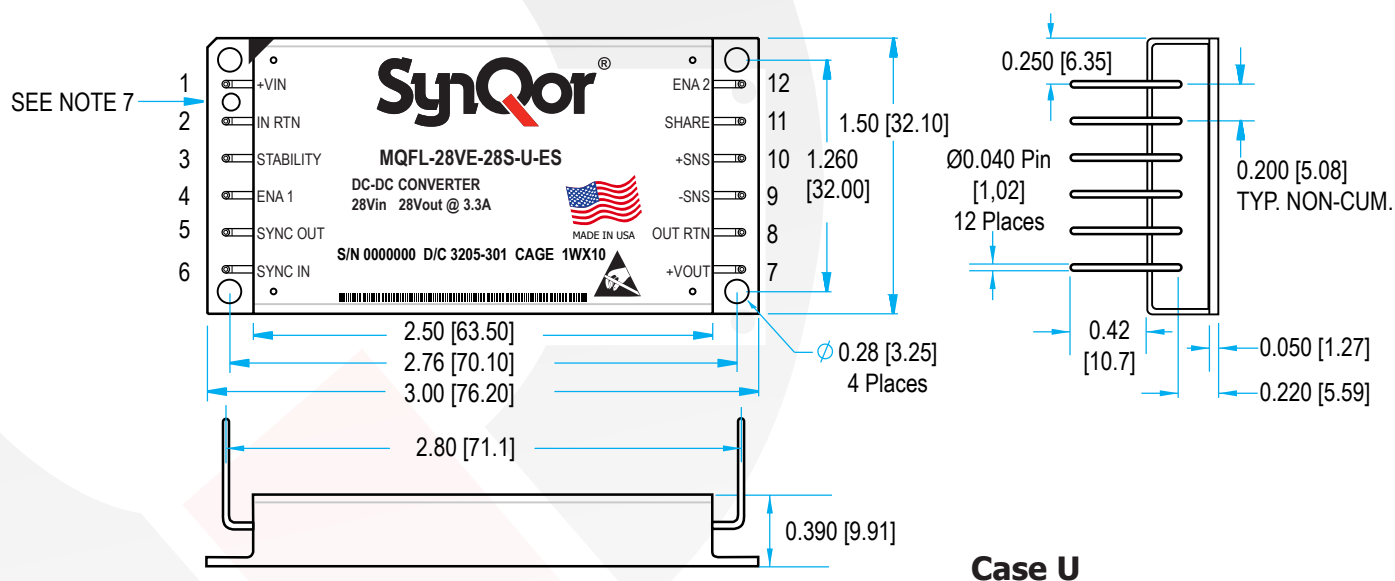
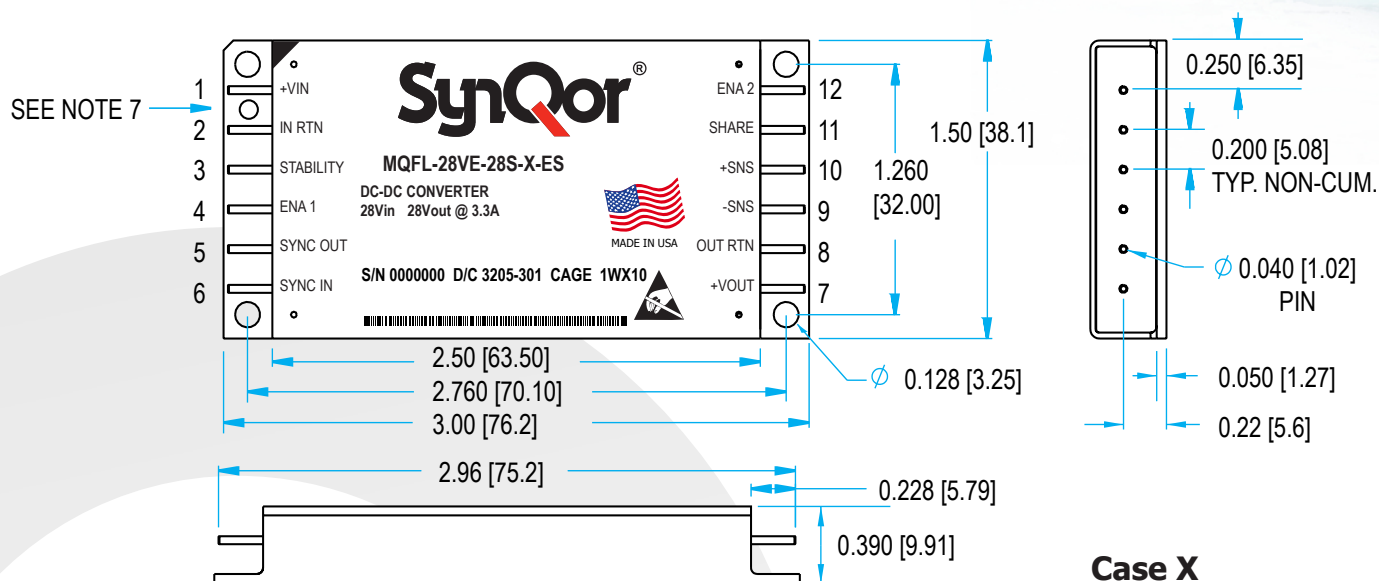


**MQFL-28VE-28S**

**Output: 28V**

**Current: 3.3A**

## Mechanical Diagrams



### NOTES

- 1) Pins 0.040" (1.02 mm) diameter
- 2) Pin Material: Copper Alloy  
Finish: Gold over Nickel plating, followed by Sn/Pb solder dip
- 3) All dimensions in inches (mm) Tolerances: x.xxx +/-0.02 in. (x.x +/-0.5 mm)  
x.xxx +/-0.010 in. (x.xx +/-0.25 mm)
- 4) Weight: 2.8 oz (78.5 g) typical
- 5) Workmanship: Meets or exceeds IPC-A-610 Class III
- 6) Print Labeling on Top Surface per Product Label Format Drawing
- 7) Pin 1 identification hole, not intended for mounting (case X and U)
- 8) Baseplate flatness tolerance is 0.004" (.10 mm) TIR for surface.

### PIN DESIGNATIONS

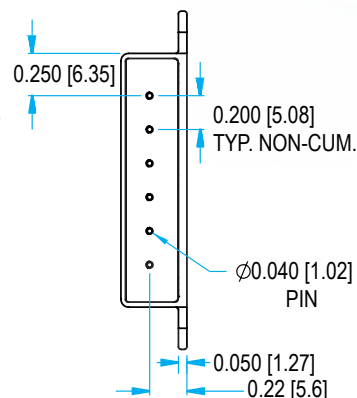
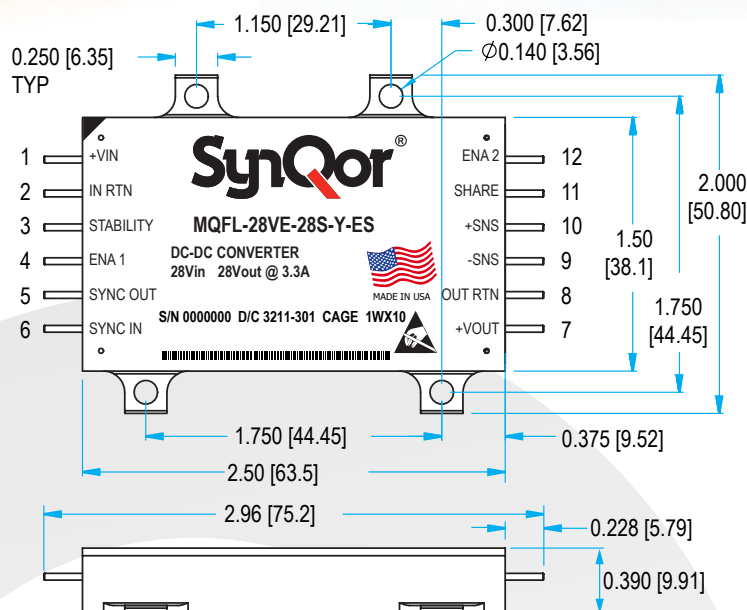
Pin #	Function	Pin #	Function
1	Positive input	7	Positive output
2	Input return	8	Output return
3	Stability	9	- Sense
4	Enable 1	10	+ Sense
5	Sync output	11	Share
6	Sync input	12	Enable 2



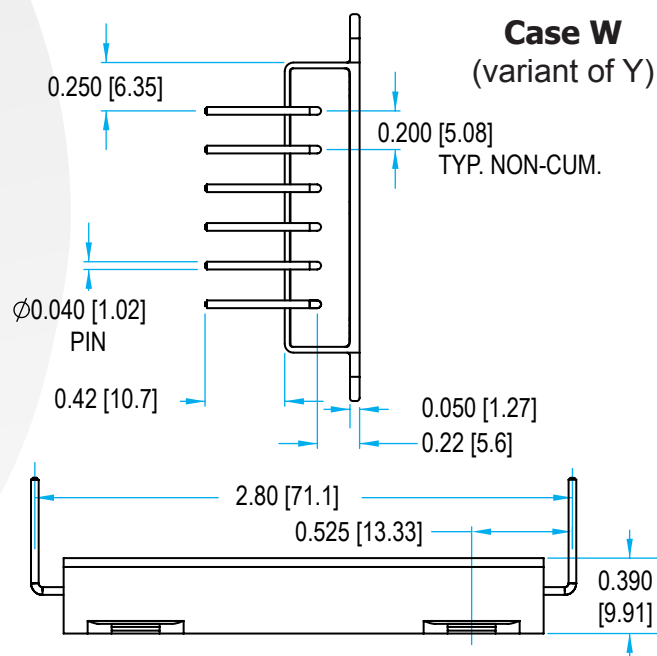
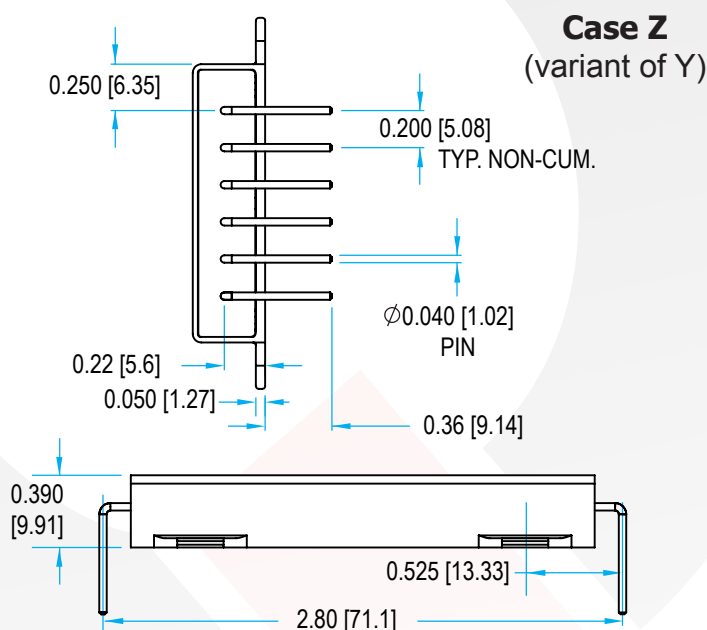
**MQFL-28VE-28S**

**Output: 28V**

**Current: 3.3A**



**Case Y**



### NOTES

- 1) Pins 0.040" (1.02 mm) diameter
- 2) Pin Material: Copper Alloy  
Finish: Gold over Nickel plating, followed by Sn/Pb solder dip
- 3) All dimensions in inches (mm) Tolerances: x.xx +/-0.02 in. (x.x +/-0.5 mm)  
x.xxx +/-0.010 in. (x.xx +/-0.25 mm)
- 4) Weight: 2.8 oz (78.5 g) typical
- 5) Workmanship: Meets or exceeds IPC-A-610 Class III
- 6) Print Labeling on Top Surface per Product Label Format Drawing
- 7) Pin 1 identification hole, not intended for mounting (case X and U)
- 8) Baseplate flatness tolerance is 0.004" (.10 mm) TIR for surface.

### PIN DESIGNATIONS

Pin #	Function	Pin #	Function
1	Positive input	7	Positive output
2	Input return	8	Output return
3	Stability	9	- Sense
4	Enable 1	10	+ Sense
5	Sync output	11	Share
6	Sync input	12	Enable 2



**MQFL-28VE-28S**

**Output: 28V**

**Current: 3.3A**

## Ordering Information

### MilQor Converter FAMILY MATRIX

The tables below show the array of MilQor converters available. When ordering SynQor converters, please ensure that you use the complete part number according to the table in the last page. Contact the factory for other requirements.

Full Size	Single Output											Dual Output <sup>†</sup>		
	1.5 V (1R5S)	1.8 V (1R8S)	2.5 V (2R5S)	3.3 V (3R3S)	5 V (05S)	6 V (06S)	7.5 V (7R5S)	9 V (09S)	12 V (12S)	15 V (15S)	28 V (28S)	5 V (05D)	12 V (12D)	15 V (15D)
<b>MQFL-28</b> 16-40 Vin Cont. 16-50 Vin 1 s Trans.* Absolute Max Vin = 60 V	40 A	40 A	40 A	30 A	24 A	20 A	16 A	13 A	10 A	8 A	4 A	24 A Total	10 A Total	8 A Total
<b>MQFL-28E</b> 16-70 Vin Cont. 16-80 Vin 1 s Trans.* Absolute Max Vin = 100 V	40 A	40 A	40 A	30 A	24 A	20 A	16 A	13 A	10 A	8 A	4 A	24 A Total	10 A Total	8 A Total
<b>MQFL-28 V</b> 16-40 Vin Cont. 5.5-50 Vin 1 s Trans.* Absolute Max Vin = 60 V	40 A	40 A	40 A	30 A	20 A	17 A	13 A	11 A	8 A	6.5 A	3.3 A			
<b>MQFL-28 VE</b> 16-70 Vin Cont. 5.5-80 Vin 1 s Trans.* Absolute Max Vin = 100 V	40 A	40 A	40 A	30 A	20 A	17 A	13 A	11 A	8A	6.5A	3.3A			
<b>MQFL-270</b> 155-400 Vin Cont. 155-475 Vin 1 s Trans.* Absolute Max Vin = 550 V	40A	40A	40A	30A	24A	20A	16A	13 A	10A	8 A	4 A	24 A Total	10 A Total	8 A Total
<b>MQFL-270L</b> 65-350 Vin Cont. 65-475 Vin 1 s Trans.* Absolute Max Vin = 550 V	40 A	40 A	30 A	22 A	15 A	12 A	10 A	8 A	6 A	5 A	2.7 A	15 A Total	6 A Total	5 A Total
Half Size	Single Output											Dual Output <sup>†</sup>		
	1.5 V (1R5S)	1.8 V (1R8S)	2.5 V (2R5S)	3.3 V (3R3S)	5 V (05S)	6 V (06S)	7.5 V (7R5S)	9 V (09S)	12 V (12S)	15 V (15S)	28 V (28S)	5 V (05D)	12 V (12D)	15 V (15D)
<b>MQHL-28</b> 16-40 Vin Cont. 16-50 Vin 1 s Trans.* Absolute Max Vin = 60 V	20 A	20 A	20 A	15 A	10 A	8 A	6.6 A	5.5 A	4 A	3.3 A	1.8 A	10 A Total	4 A Total	3.3 A Total
<b>MQHL-28E</b> 16-70 Vin Cont. 16-80 Vin 1 s Trans.* Absolute Max Vin = 100 V	20 A	20 A	20 A	15 A	10 A	8 A	6.6 A	5.5 A	4 A	3.3 A	1.8 A	10 A Total	4 A Total	3.3 A Total
<b>MQHR-28</b> 16-40 Vin Cont. 16-50 Vin 1 s Trans.* Absolute Max Vin = 60 V	10 A	10 A	10 A	7.5 A	5 A	4 A	3.3 A	2.75 A	2 A	1.65 A	0.9 A	5 A Total	2 A Total	1.65 A Total
<b>MQHR-28E</b> 16-70 Vin Cont. 16-80 Vin 1 s Trans.* Absolute Max Vin = 100 V	10 A	10 A	10 A	7.5 A	5 A	4 A	3.3 A	2.75 A	2 A	1.65 A	0.9 A	5 A Total	2 A Total	1.65 A Total

Check with factory for availability.

<sup>†</sup>80% of total output current available on any one output.

\*Converters may be operated at the highest transient input voltage, but some component electrical and thermal stresses would be beyond MIL-HDBK-1547A guidelines.





**MQFL-28VE-28S**  
**Output: 28V**  
**Current: 3.3A**

## Ordering Information

### PART NUMBERING SYSTEM

The part numbering system for SynQor's MilQor DC-DC converters follows the format shown in the table below.

Not all combinations make valid part numbers, please contact SynQor for availability. See the Product Summary web page for more options.

**Example: MQFL-28VE-28S-Y-ES**

Model Name	Input Voltage Range	Output Voltage(s)		Package Outline/ Pin Configuration	Screening Grade
		Single Output	Dual Output		
MQFL MQHL MQHR	28 28E 28V 28VE  270 270L	1R5S	05D 6R5D 12D 15D	U X Y W Z	C ES HB
		1R8S			
		2R5S			
		3R3S			
		05S			
		06S			
		6R5S			
		7R5S			
		08S			
		09S			
		12S			
		15S			
		28S			

### APPLICATION NOTES

A variety of application notes and technical white papers can be downloaded in pdf format from the SynQor website.

#### Contact SynQor for further information and to order:

**Phone:** 978-849-0600  
**Toll Free:** 1-888-567-9596  
**Fax:** 978-849-0602  
**E-mail:** [mqnbofae@synqor.com](mailto:mqnbofae@synqor.com)  
**Web:** [www.synqor.com](http://www.synqor.com)  
**Address:** 155 Swanson Road  
 Boxborough, MA 01719  
 USA

#### PATENTS

SynQor holds numerous U.S. patents, one or more of which apply to most of its power conversion products. Any that apply to the product(s) listed in this document are identified by markings on the product(s) or on internal components of the product(s) in accordance with U.S. patent laws. SynQor's patents include the following:

5,999,417 6,222,742 6,545,890 6,594,159 6,894,468 6,896,526  
 6,927,987 7,050,309 7,072,190 7,085,146 7,119,524 7,269,034  
 7,272,021 7,272,023 7,558,083 7,564,702 7,765,687 7,787,261  
 8,023,290 8,149,597 8,493,751 8,644,027 9,143,042

#### Warranty

SynQor offers a two (2) year limited warranty. Complete warranty information is listed on our website or is available upon request from SynQor.