

- Dual TLC2933 by Multichip Module (MCM) Technology
- Voltage-Controlled Oscillators (VCO) Section
  - Complete Oscillator Using Only One External Bias Resistor (RBIAS)
  - Recommended Lock Frequency Range
    - 37 MHz to 60 MHz (V<sub>DD</sub> = 3.3 V ± 0.15 V, T<sub>A</sub> = –20°C to 75°C)
    - 43 MHz to 100 MHz (V<sub>DD</sub> = 5 V ± 0.25 V, T<sub>A</sub> = –20°C to 75°C)
- Includes a High Speed Edge-Triggered Phase Frequency Detector (PFD) With Internal Charge Pump
- Independent VCO, PFD Power-Down Mode

#### description

The TLC2943 is a multichip module product that uses two TLC2933 chips. The TLC2933 chip is composed of a voltage-controlled oscillator (VCO) and an edge-triggered-type phase frequency detector (PFD). The oscillation frequency range of the VCO is set by an external bias resistor (RBIAS). The high-speed PFD with internal charge pump detects the phase difference between the reference frequency input and signal frequency input from the external counter. Both the VCO and the PFD have inhibit functions that can be used as a power-down mode. The high-speed and stable VCO characteristics of the TLC2933 make the TLC2943 suitable for use in dual high-performance phase-locked loop (PLL) systems.

DB PACKAGE (TOP VIEW)	
LOGIC_1 V <sub>DD</sub>	1
TEST_1	2
VCO_1 OUT	3
F <sub>IN</sub> -A_1	4
F <sub>IN</sub> -B_1	5
PFD_1 OUT	6
LOGIC_1 GND	7
GND	8
NC	9
NC	10
NC	11
GND	12
LOGIC_2 V <sub>DD</sub>	13
TEST_2	14
VCO_2 OUT	15
F <sub>IN</sub> -A_2	16
F <sub>IN</sub> -B_2	17
PFD_2 OUT	18
LOGIC_2 GND	19
VCO_1 V <sub>DD</sub>	38
R <sub>BIAS</sub> _1	37
VCOIN_1	36
VCO_1 GND	35
VCO_1 INHIBIT	34
PFD_1 INHIBIT	33
NC	32
GND	31
NC	30
NC	29
NC	28
GND	27
VCO_2 V <sub>DD</sub>	26
R <sub>BIAS</sub> _2	25
VCOIN_2	24
VCO_2 GND	23
VCO_2 INHIBIT	22
PFD_2 INHIBIT	21
NC	20

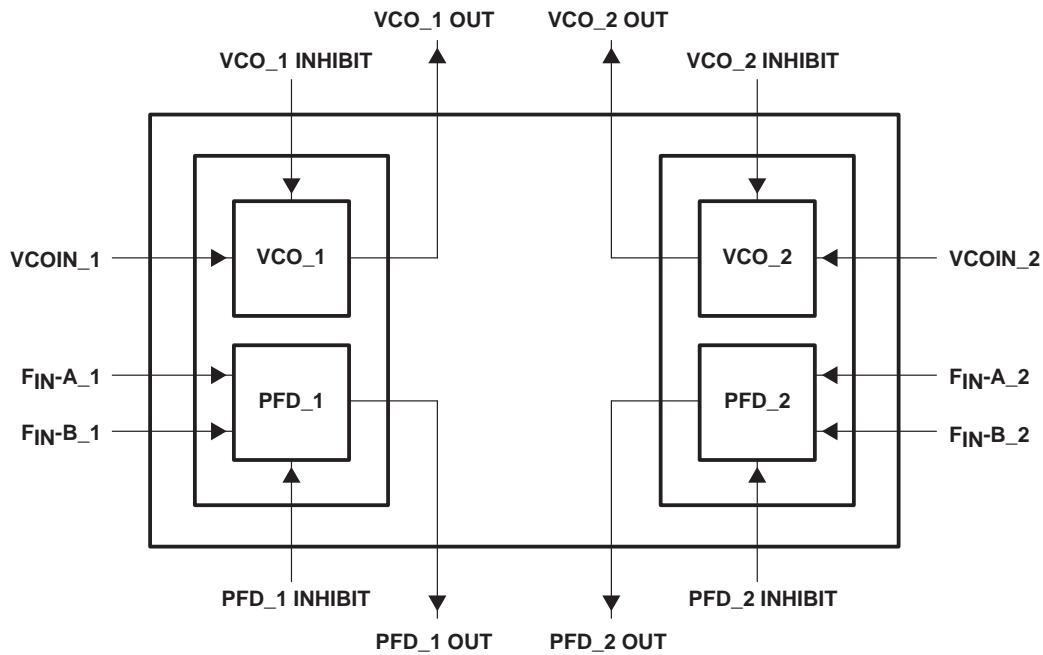
#### AVAILABLE OPTIONS

T <sub>A</sub>	PACKAGE	
	SMALL OUTLINE (DB)	
–20°C to 75°C	TLC2943IDB	TLC2943IDBR (Tape and Reel)



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## functional block diagram



### Terminal Functions

TERMINAL NAME	NO.	I/O	DESCRIPTION
GND	8, 31		Common GND for chip 1
	12, 27		Common GND for chip 2
F <sub>IN</sub> -A_1, F <sub>IN</sub> -B_1	4 5	I	Reference frequency signal input and comparison frequency signal input for PFD_1. fREF-IN_1 inputs to F <sub>IN</sub> -A_1, and comparison frequency input from external counter logic to F <sub>IN</sub> -B_1, for a lag-lead filter use as LPF.
F <sub>IN</sub> -A_2, F <sub>IN</sub> -B_2	16 17	I	Reference frequency signal input and comparison frequency signal input for PFD_2. fREF-IN_2 inputs to F <sub>IN</sub> -A_2, and comparison frequency input from external counter logic to F <sub>IN</sub> -B_2, for a lag-lead filter use as LPF.
LOGIC_1 GND	7		Ground for the internal logic of chip 1
LOGIC_2 GND	19		Ground for the internal logic of chip 2
LOGIC_1 V <sub>DD</sub>	1		Power supply for the internal logic of chip 1. This power supply should be separate from VCO V <sub>DD</sub> to reduce cross-coupling between supplies.
LOGIC_2 V <sub>DD</sub>	13		Power supply for the internal logic of chip 2. This power supply should be separate from VCO V <sub>DD</sub> to reduce cross-coupling between supplies.
NC	9, 10, 11, 20, 28, 29, 30, 32		No internal connection
PFD_1 INHIBIT	33	I	PFD inhibit control for chip 1. When PFD_1 INHIBIT is high, PFD_1 OUT is in the high-impedance state, see Table 2.
PFD_2 INHIBIT	21	I	PFD inhibit control for chip 2. When PFD_2 INHIBIT is high, PFD_2 OUT is in the high-impedance state, see Table 2.
PFD_1 OUT	6	O	PFD output of chip 1. When the PFD_1 INHIBIT is high, PFD_1 OUT is in the high-impedance state.
PFD_2 OUT	18	O	PFD output of chip 2. When the PFD_2 INHIBIT is high, PFD_2 OUT is in the high-impedance state.
R <sub>BIAS</sub> _1	37	I	Bias supply for VCO_1. An external resistor (R <sub>BIAS</sub> ) between VCO_1 V <sub>DD</sub> and BIAS_1 supplies bias for adjusting the oscillation frequency range of VCO_1.
R <sub>BIAS</sub> _2	25	I	Bias supply for VCO_2. An external resistor (R <sub>BIAS</sub> ) between VCO_2 V <sub>DD</sub> and BIAS_2 supplies bias for adjusting the oscillation frequency range of VCO_2.
TEST_1	2		Test terminal. TEST connects to LOGIC_1 GND for normal operation.
TEST_2	14		Test terminal. TEST connects to LOGIC_2 GND for normal operation.
VCO_1 GND	35		GND for VCO_1
VCO_2 GND	23		GND for VCO_2
VCO_1 INHIBIT	34	I	VCO inhibit control for chip 1. When VCO_1 INHIBIT is high, VCO_1 OUT is low (see Table 1).
VCO_2 INHIBIT	22	I	VCO inhibit control for chip 2. When VCO_2 INHIBIT is high, VCO_2 OUT is low (see Table 1).
VCO_1 OUT	3	O	VCO output of chip 1. When VCO_1 INHIBIT is high, VCO_1 OUT is low.
VCO_2 OUT	15	O	VCO output of chip 2. When VCO_2 INHIBIT is high, VCO_2 OUT is low.
VCO_1 V <sub>DD</sub>	38		Power supply for VCO_1. This power supply should be separate from LOGIC V <sub>DD</sub> to reduce cross-coupling between supplies.
VCO_2 V <sub>DD</sub>	26		Power supply for VCO_2. This power supply should be separate from LOGIC V <sub>DD</sub> to reduce cross-coupling between supplies.
VCOIN_1	36	I	VCO_1 control voltage input. Nominally the external loop filter output connects to VCO IN to control VCO oscillation frequency.
VCOIN_2	24	I	VCO_2 control voltage input. Nominally the external loop filter output connects to VCO IN to control VCO oscillation frequency.

## detailed description

### MCM (multichip module) technology for TLC2943

The TLC2943 is a multichip module (MCM) product that uses two TLC2933 chips. Inside the package, two chips are completely isolated by a special formed lead-frame. Therefore, when using the TLC2943 in two asynchronous PLL circuits, there is no performance degradation by electrical interference between chips inside the package. So, the same performance as TLC2933 can be easily expected by using TLC2943.

The NC terminals in the middle on both sides of the package are to achieve complete isolation inside the package. To get the best performance from this MCM technology, it is better to make a careful board layout of the external power supply, ground, and signal lines.

### voltage controlled oscillator (VCO)

VCO\_1 and VCO\_2 have the same typical characteristics. Each VCO oscillation frequency is determined by an external resistor ( $R_{BIAS}$ ) connected between the VCO  $V_{DD}$  and the BIAS terminals. The oscillation frequency and range depend on this resistor value. The bias resistor value for the minimum temperature coefficient is nominally 2.2 k $\Omega$  with  $V_{DD} = 3.3$  V and nominally 2.4 k $\Omega$  with  $V_{DD} = 5$  V. For the lock frequency range, refer to the recommended operating conditions. Figure 1 shows the typical frequency variation and VCO control voltage.

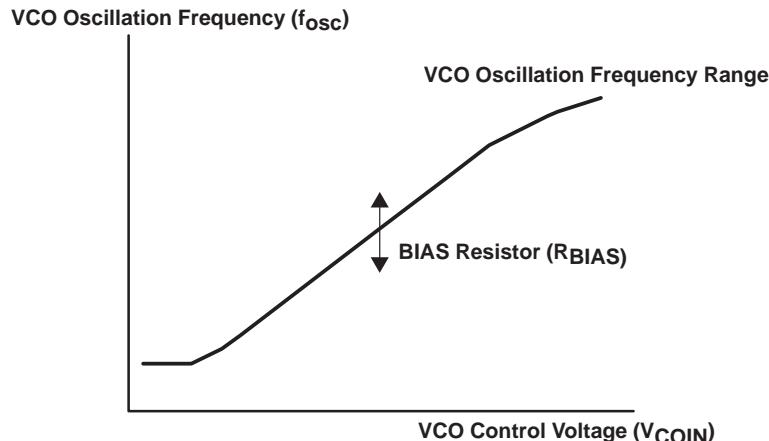


Figure 1. VCO\_1 and VCO\_2 Oscillation Frequency

### VCO inhibit function

Each VCO has an externally controlled inhibit function that inhibits the VCO output. The VCO oscillation is stopped during a high level on VCOINHIBIT, so the high level can also be used as the power-down mode. The VCO output maintains a low level during the power-down mode (see Table 1 and Table 2).

Table 1. VCO\_1 Inhibit Function

VCO_1 INHIBIT	VCO_1 OSCILLATOR	VCO_1 OUT	VCO_1 IDD
Low	Active	Active	Normal
High	Stop	Low	Power down

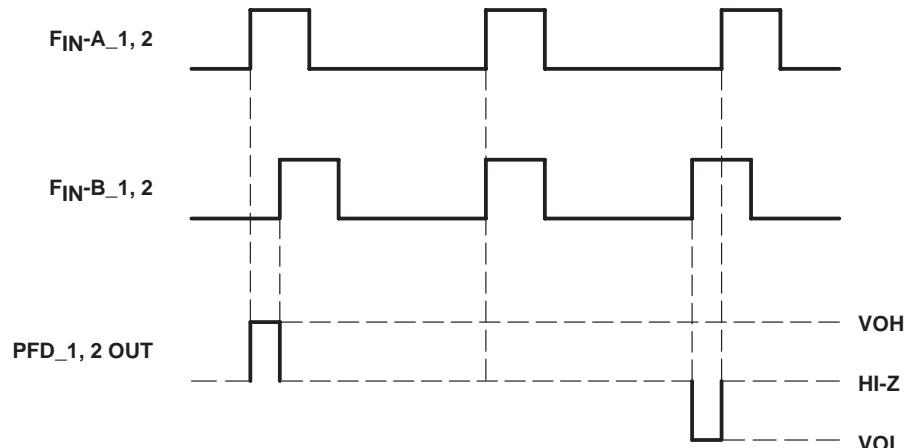
Table 2. VCO\_2 Inhibit Function

VCO_2 INHIBIT	VCO_2 OSCILLATOR	VCO_2 OUT	VCO_2 IDD
Low	Active	Active	Normal
High	Stop	Low	Power down

## detailed description (continued)

### phase frequency detector (PFD)

The PFD is a high-speed, edge-triggered detector with an internal charge pump. The PFD detects the phase difference between two frequency inputs supplied to  $F_{IN\text{-}A}$  and  $F_{IN\text{-}B}$  as shown in Figure 2. Nominally the reference is supplied to  $F_{IN\text{-}A}$ , and the frequency from the external counter output is fed to  $F_{IN\text{-}B}$ . For clock recovery PLL systems, other types of phase detectors should be used.



**Figure 2. PFD Function Timing Chart**

### PFD output control

A high level on PFD INHIBIT places the PFD OUT in the high impedance state and the PFD stops phase detection as shown in Table 3 and Table 4. A high level on PFD inhibit also can be used as the power-down mode for the PFD.

**Table 3. PFD\_1 Inhibit Function**

PFD_1 INHIBIT	PFD_1	PFD_1 OUT	PFD_1 $I_{DD}$
Low	Active	Active	Normal
High	Stop	Hi-Z	Power down

**Table 4. PFD\_2 Inhibit Function**

PFD_2 INHIBIT	PFD_2	PFD_2 OUT	PFD_2 $I_{DD}$
Low	Active	Active	Normal
High	Stop	Hi-Z	Power down

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### internal function block diagram

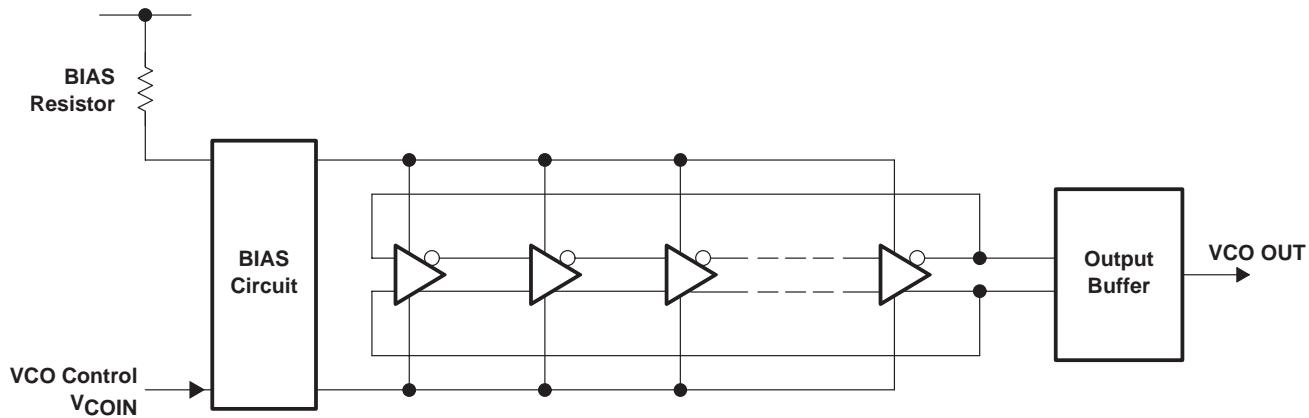


Figure 3. VCO Block Schematic (VCO\_1, VCO\_2)

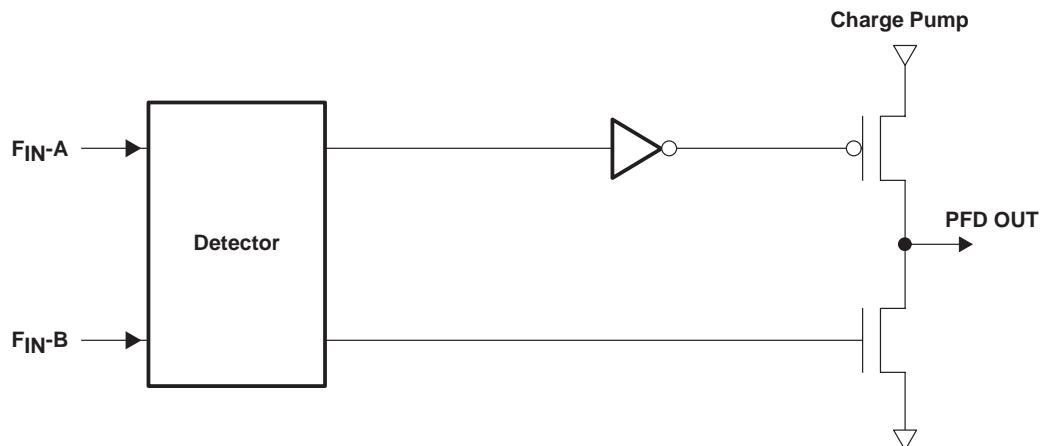


Figure 4. PFD Block Schematic (PFD\_1, PFD\_2)

**absolute maximum ratings over operating free-air temperature (unless otherwise noted)†**

Supply voltage (each supply), $V_{DD}$ (see Note 1)	.....	7 V
Input voltage range (each input), $V_I$ (see Note 1)	.....	−0.5 to $V_{DD} + 0.5$ V
Input current (each input), $I_I$	.....	±20 mA
Output current (each output), $I_O$	.....	±20 mA
Continuous total power dissipation at (or below) $T_A = 25^\circ\text{C}$ (see Note 2)	.....	1160 mW
Operating free-air temperature range, $T_A$	.....	−20°C to 75°C
Storage temperature range, $T_{stg}$	.....	−65°C to 150°C
Lead temperature 1.6 mm (1/16 in) from case for 10 seconds	.....	260°C

† Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

NOTES: 1. All voltage values are with respect to network ground terminal.  
2. For operation above 25°C free-air temperature, derate linearly at the rate of 9.3 mW/°C.

**recommended operating conditions**

		MIN	NOM	MAX	UNIT
Supply voltage (each supply, see Notes 3 and 4 ), $V_{DD}$	$V_{DD} = 3$ V	2.85	3	3.15	V
	$V_{DD} = 3.3$ V	3.15	3.3	3.45	
	$V_{DD} = 5$ V	4.75	5	5.25	
Input voltage range (input except for VCOIN_1, 2), $V_I$		0	$V_{DD}$		V
Output current (each output), $I_O$		0	±2		mA
Control voltage, VCOIN		1	$V_{DD}$		V
Clock frequency, $f$	$V_{DD} = 3$ V	37	55		MHz
	$V_{DD} = 3.3$ V	37	60		
	$V_{DD} = 5$ V	43	100		
Oscillation frequency range set resistor (each RBIAS), RBIAS VCO	$V_{DD} = 3$ V	1.8	2.7		kΩ
	$V_{DD} = 3.3$ V	1.8	3.0		
	$V_{DD} = 5$ V	2.2	3.0		
Top operating temperature range		−20	75		°C

NOTES: 3. It is recommended that the logic supply terminal (LOGIC  $V_{DD}$ ) and the VCO supply terminal (VCO  $V_{DD}$ ) be at the same voltage and separated from each other.  
4. Insert bypass capacitors locating the nearest point to each power supply terminal.

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**electrical characteristics over recommended operating free-air temperature range,  $V_{DD} = 3$  V (unless otherwise noted)**

### VCO section

PARAMETER	TEST CONDITIONS	MIN	NOM	MAX	UNIT	
$V_{OH}$	High-level output voltage	$I_{OH} = -2$ mA	2.4		V	
$V_{OL}$	Low-level output voltage	$I_{OL} = 2$ mA		0.3	V	
$V_{(TH+)}$	Positive input threshold voltage		0.9	1.5	2.1	V
$I_I$	Input current	$V_I = V_{DD}$ or GND		$\pm 1$	$\mu A$	
$Z_{(VCOIN)}$	VCOIN input impedance	$V_{COIN} = 1/2V_{DD}$	10		$M\Omega$	
$I_{DD(INH)}$	VCO supply current (inhibit) (for one chip)	See Note 5	0.01	1	$\mu A$	
$I_{DD(VCO)}$	VCO supply current (for one chip)	See Note 6	5.1	15	mA	

NOTES: 5. The current into VCO  $V_{DD}$  and LOGIC  $V_{DD}$  when VCO INHIBIT =  $V_{DD}$  and PFD INHIBIT is high.  
6. The current into VCO  $V_{DD}$  and LOGIC  $V_{DD}$  when VCO IN =  $1/2 V_{DD}$ ,  $R_{BIAS} = 2.4$  k $\Omega$ , VCO INHIBIT = ground, and PFD INHIBIT is high.

### PFD section

PARAMETER	TEST CONDITIONS	MIN	NOM	MAX	UNIT
$V_{OH}$	$I_{OH} = -2$ mA	2.7			V
$V_{OL}$	$I_{OL} = 2$ mA		0.2		V
$I_{OZ}$	PFD INHIBIT = high, $V_O = V_{DD}$ or GND		$\pm 1$		$\mu A$
$V_{IH}$	High-level input voltage at $F_{IN-A}$ , $F_{IN-B}$		2.1		V
$V_{IL}$	Low-level input voltage at $F_{IN-A}$ , $F_{IN-B}$		0.9		V
$V_{(TH+)}$	Positive input threshold voltage at PFD INHIBIT	0.9	1.5	2.1	V
$C_I$	Input capacitance at $F_{IN-A}$ , $F_{IN-B}$		5		pF
$Z_I$	Input impedance at $F_{IN-A}$ , $F_{IN-B}$		10		$M\Omega$
$I_{DD(PFD)}$	PFD supply current	See Note 7	0.7	4	mA

NOTE 7: The current into LOGIC  $V_{DD}$  when  $F_{IN-A}$  and  $F_{IN-B} = 30$  MHz ( $V_I(PP) = 3$  V, rectangular wave), PFD INHIBIT = GND, PFD OUT open, and VCO OUT is inhibited.

**electrical characteristics over recommended operating free-air temperature range,  $V_{DD} = 3.3$  V (unless otherwise noted) (continued)**

**VCO section**

PARAMETER	TEST CONDITIONS	MIN	NOM	MAX	UNIT
$V_{OH}$ High-level output voltage	$I_{OH} = -2$ mA		2.7		V
$V_{OL}$ Low-level output voltage	$I_{OL} = 2$ mA		0.4		V
$V_{(TH+)}$ Positive input threshold voltage		1	1.65	2.3	V
$I_I$ Input current	$V_I = V_{DD}$ or GND			$\pm 1$	$\mu$ A
$Z_{(VCOIN)}$ VCOIN input impedance	$V_{COIN} = 1/2V_{DD}$		10		$M\Omega$
$I_{DD(INH)}$ VCO supply current (inhibit) (for one chip)	See Note 5		0.01	1	$\mu$ A
$I_{DD(VCO)}$ VCO supply current (for one chip)	See Note 6		6.2	16	mA

NOTES: 5. The current into VCO  $V_{DD}$  and LOGIC  $V_{DD}$  when VCO INHIBIT =  $V_{DD}$  and PFD INHIBIT is high.  
 6. The current into VCO  $V_{DD}$  and LOGIC  $V_{DD}$  when VCO IN =  $1/2 V_{DD}$ ,  $R_{BIAS} = 2.4$  k $\Omega$ , VCO INHIBIT = ground, and PFD INHIBIT is high.

**PFD section**

PARAMETER	TEST CONDITIONS	MIN	NOM	MAX	UNIT
$V_{OH}$ High-level output voltage	$I_{OH} = -2$ mA	3			V
$V_{OL}$ Low-level output voltage	$I_{OL} = 2$ mA		0.2		V
$I_{OZ}$ High-impedance state output current	PFD INHIBIT = high, $V_O = V_{DD}$ or GND			$\pm 1$	$\mu$ A
$V_{IH}$ High-level input voltage at $F_{IN-A}$ , $F_{IN-B}$			2.3		V
$V_{IL}$ Low-level input voltage at $F_{IN-A}$ , $F_{IN-B}$			1		V
$V_{(TH+)}$ Positive input threshold voltage at PFD INHIBIT		1	1.65	2.3	V
$C_I$ Input capacitance at $F_{IN-A}$ , $F_{IN-B}$			5		pF
$Z_I$ Input impedance at $F_{IN-A}$ , $F_{IN-B}$			10		$M\Omega$
$I_{DD(PFD)}$ PFD supply current	See Note 8		0.8	5	mA

NOTE 8: The current into LOGIC  $V_{DD}$  when  $F_{IN-A}$  and  $F_{IN-B} = 30$  MHz ( $V_I(PP) = 3.3$  V, rectangular wave), PFD INHIBIT = GND, PFD OUT open, and VCO OUT is inhibited.

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**electrical characteristics over recommended operating free-air temperature range,  $V_{DD} = 5$  V (unless otherwise noted) (continued)**

### VCO section

PARAMETER	TEST CONDITIONS	MIN	NOM	MAX	UNIT	
$V_{OH}$	High-level output voltage	$I_{OH} = -2$ mA	4.5		V	
$V_{OL}$	Low-level output voltage	$I_{OL} = 2$ mA		0.5	V	
$V_{(TH+)}$	Positive input threshold voltage		1.5	2.5	3.5	V
$I_I$	Input current	$V_I = V_{DD}$ or GND		$\pm 1$	$\mu A$	
$Z_{(VCOIN)}$	VCOIN input impedance	$V_{COIN} = 1/2V_{DD}$	10		$M\Omega$	
$I_{DD(INH)}$	VCO supply current (inhibit) (for one chip)	See Note 5	0.01	1	$\mu A$	
$I_{DD(VCO)}$	VCO supply current (for one chip)	See Note 6	14	35	mA	

NOTES: 5. The current into VCO  $V_{DD}$  and LOGIC  $V_{DD}$  when VCO INHIBIT =  $V_{DD}$  and PFD INHIBIT is high.  
6. The current into VCO  $V_{DD}$  and LOGIC  $V_{DD}$  when VCO IN =  $1/2 V_{DD}$ ,  $R_{BIAS} = 2.4$  k $\Omega$ , VCO INHIBIT = ground, and PFD INHIBIT is high.

### PFD section

PARAMETER	TEST CONDITIONS	MIN	NOM	MAX	UNIT
$V_{OH}$	$I_{OH} = -2$ mA	4.5			V
$V_{OL}$	$I_{OL} = 2$ mA		0.2		V
$I_{OZ}$	PFD INHIBIT = high, $V_O = V_{DD}$ or GND		$\pm 1$		$\mu A$
$V_{IH}$	High-level input voltage at $F_{IN-A}$ , $F_{IN-B}$		3.5		V
$V_{IL}$	Low-level input voltage at $F_{IN-A}$ , $F_{IN-B}$			1.5	V
$V_{(TH+)}$	Positive input threshold voltage at PFD INHIBIT	1.5	2.5	3.5	V
$C_I$	Input capacitance at $F_{IN-A}$ , $F_{IN-B}$		7		pF
$Z_I$	Input impedance at $F_{IN-A}$ , $F_{IN-B}$		10		$M\Omega$
$I_{DD(PFD)}$	PFD supply current	See Note 9	2.6	8	mA

NOTE 9: The current into LOGIC  $V_{DD}$  when  $F_{IN-A}$  and  $F_{IN-B} = 50$  MHz ( $V_I(PP) = 5$  V, rectangular wave), PFD INHIBIT = GND, PFD OUT open, and VCO OUT is inhibited.

**operating characteristics at  $V_{DD} = 3$  V,  $T_A = 25^\circ\text{C}$  (unless otherwise noted)**

**VCO section**

PARAMETER	TEST CONDITIONS	MIN	NOM	MAX	UNIT
$f_{(\text{OSC})}$ Oscillation frequency	$R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $V_{\text{COIN}} = 1/2V_{DD}$	38	48	58	MHz
$t_{(\text{STB})}$ Time to stable oscillation	See Note 10			10	$\mu\text{s}$
$t_r$ Output rise time	$C_L = 15 \text{ pF}$ , See Figure 5		3.3	10	ns
$t_f$ Output fall time	$C_L = 15 \text{ pF}$ , See Figure 5		2	8	ns
$f_{(\text{DUTY})}$ Duty cycle	$R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $V_{\text{COIN}} = 1/2V_{DD}$	45%	50%	55%	
$f_{(\text{TA})}$ Temperature coefficient of oscillation frequency	$R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $V_{\text{COIN}} = 1/2V_{DD}$ , $T_{\text{op}} = -20^\circ\text{C}$ to $75^\circ\text{C}$		0.03		$^\circ\text{C}$
$f_{(\text{VDD})}$ Supply voltage coefficient of oscillation frequency supply	$R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $V_{\text{COIN}} = 1.5 \text{ V}$ , $V_{DD} = 2.85 \text{ V}$ to $3.15 \text{ V}$		0.04		%/mV

NOTE 10: The time period to the stable VCO oscillation frequency after the VCO INHIBIT terminal is changed to a low level.

**PFD section**

PARAMETER	TEST CONDITIONS	MIN	NOM	MAX	UNIT
$f_{\text{MAX}}$ Maximum operating frequency		30			MHz
$t_{PLZ}$ PFD output disable time from low level	See Figure 6 and Figure 7, and Table 5		20	40	ns
$t_{PHZ}$ PFD output disable time from high level			18	40	
$t_{PZL}$ PFD output enable time to low level			4.1	18	ns
$t_{PZH}$ PFD output enable time to high level			4.8	18	
$t_r$ Rise time	$C_L = 15 \text{ pF}$ , See Figure 6		3.1	9	ns
$t_f$ Fall time			1.5	9	

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**operating characteristics at  $V_{DD} = 3.3$  V,  $T_A = 25^\circ\text{C}$  (unless otherwise noted)**

### VCO section

PARAMETER	TEST CONDITIONS	MIN	NOM	MAX	UNIT
$f_{(\text{OSC})}$	Oscillation frequency $R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $V_{\text{COIN}} = 1/2V_{DD}$	42	52	62	MHz
$t_{(\text{STB})}$	Time to stable oscillation See Note 10			10	$\mu\text{s}$
$t_r$	Output rise time $C_L = 15 \text{ pF}$ , See Figure 5		3	8	ns
$t_f$	Output fall time $C_L = 15 \text{ pF}$ , See Figure 5		1.9	7	ns
$f_{(\text{DUTY})}$	Duty cycle $R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $V_{\text{COIN}} = 1/2V_{DD}$	45%	50%	55%	
$f_{(\text{TA})}$	Temperature coefficient of oscillation frequency $R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $T_{\text{op}} = -20^\circ\text{C}$ to $75^\circ\text{C}$ $V_{\text{COIN}} = 1/2V_{DD}$		0.03		$^\circ\text{C}$
$f_{(\text{VDD})}$	Supply voltage coefficient of oscillation frequency supply $R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $V_{DD} = 3.15 \text{ V}$ to $3.45 \text{ V}$ $V_{\text{COIN}} = 1.65 \text{ V}$		0.04		$%/m\text{V}$

NOTE 10: The time period to the stable VCO oscillation frequency after the VCO INHIBIT terminal is changed to a low level.

### PFD section

PARAMETER	TEST CONDITIONS	MIN	NOM	MAX	UNIT
$f_{\text{MAX}}$	Maximum operating frequency	30			MHz
$t_{PLZ}$	PFD output disable time from low level	20	40		ns
$t_{PHZ}$	PFD output disable time from high level	18	40		
$t_{PZL}$	PFD output enable time to low level		16		ns
$t_{PZH}$	PFD output enable time to high level		16		
$t_r$	Rise time		8		ns
$t_f$	Fall time		8		

**operating characteristics at  $V_{DD} = 5$  V,  $T_A = 25^\circ\text{C}$  (unless otherwise noted)**

**VCO section**

PARAMETER		TEST CONDITIONS	MIN	NOM	MAX	UNIT
$f_{(\text{OSC})}$	Oscillation frequency	$R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $V_{\text{COIN}} = 1/2V_{DD}$	64	80	96	MHz
$t_{(\text{STB})}$	Time to stable oscillation	See Note 10			10	$\mu\text{s}$
$t_r$	Output rise time	$C_L = 15 \text{ pF}$ , See Figure 5		2.1	5	ns
$t_f$	Output fall time	$C_L = 15 \text{ pF}$ , See Figure 5		1.5	4	ns
$f_{(\text{DUTY})}$	Duty cycle	$R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $V_{\text{COIN}} = 1/2V_{DD}$	45%	50%	55%	
$f_{(\text{TA})}$	Temperature coefficient of oscillation frequency	$R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $T_{\text{op}} = -20^\circ\text{C}$ to $75^\circ\text{C}$		0.03		$^\circ\text{C}$
$f_{(\text{VDD})}$	Supply voltage coefficient of oscillation frequency supply	$R_{\text{BIAS}} = 2.4 \text{ k}\Omega$ , $V_{DD} = 4.75 \text{ V}$ to $5.25 \text{ V}$		0.02		%/mV

**PFD section**

PARAMETER		TEST CONDITIONS	MIN	NOM	MAX	UNIT
$f_{\text{MAX}}$	Maximum operating frequency		50			MHz
$t_{PLZ}$	PFD output disable time from low level			20	40	ns
$t_{PHZ}$	PFD output disable time from high level			17	40	
$t_{PZL}$	PFD output enable time to low level	See Figure 6 and Figure 7, and Table 5		3.7	10	ns
$t_{PZH}$	PFD output enable time to high level		3.5	10		
$t_r$	Rise time	$C_L = 15 \text{ pF}$ , See Figure 6		1.7	5	ns
$t_f$	Fall time			1.3	5	

## PARAMETER MEASUREMENT INFORMATION

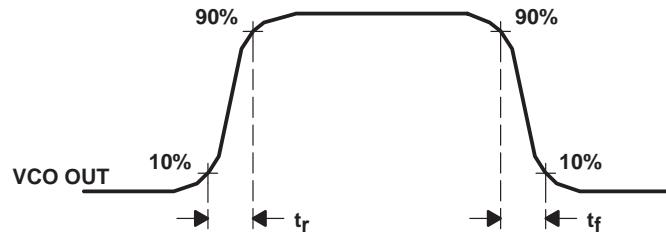


Figure 5. VCO Output Voltage Waveform (Each VCO)

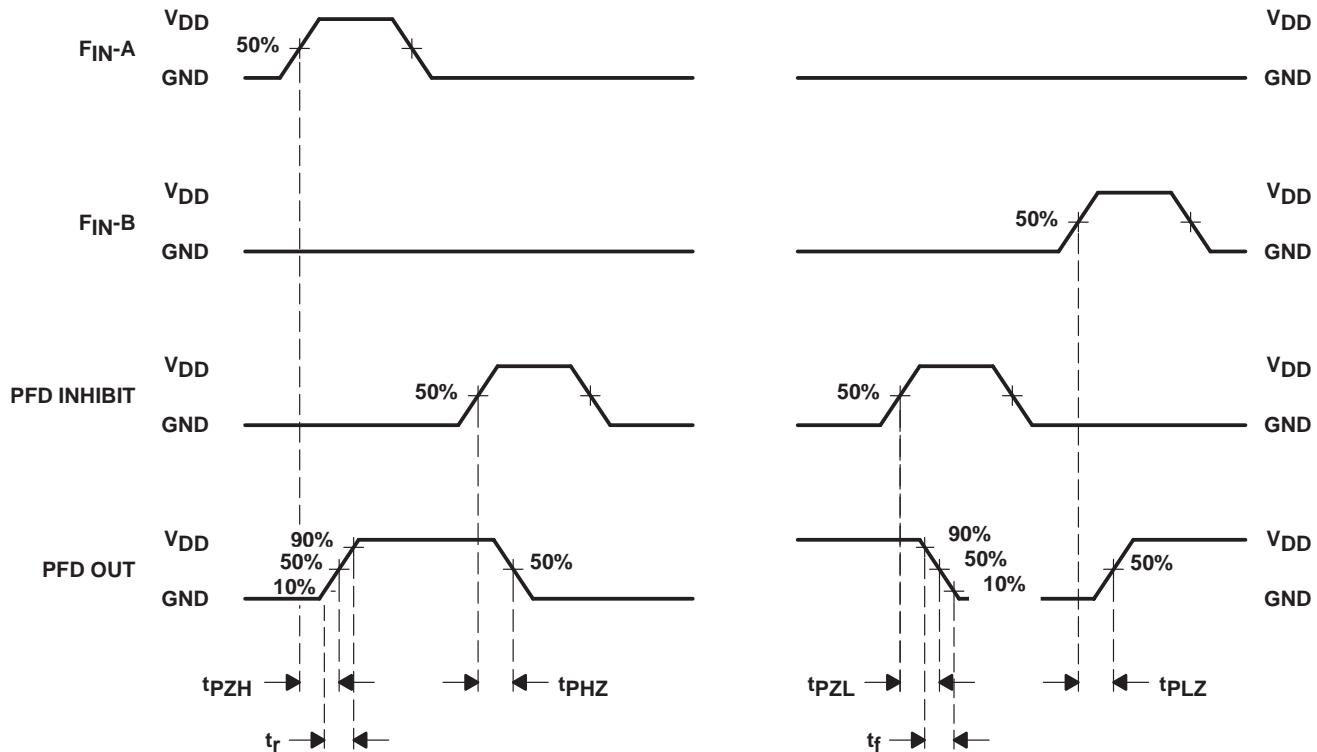


Figure 6. PFD Output Voltage Waveform

### PARAMETER MEASUREMENT INFORMATION

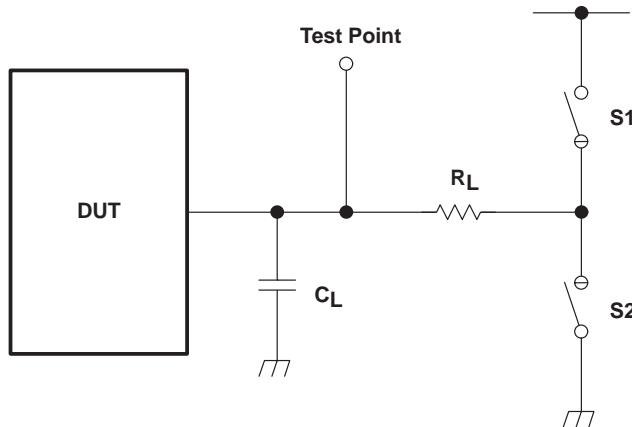


Figure 7. PFD Output Test Conditions

Table 5. PFD Output Test Conditions

PARAMETER	R <sub>L</sub>	C <sub>L</sub>	S1	S2
t <sub>PZH</sub>				
t <sub>PHZ</sub>			OPEN	CLOSE
t <sub>r</sub>	1 kΩ	15 pF		
t <sub>PZL</sub>				
t <sub>PLZ</sub>			CLOSE	OPEN
t <sub>f</sub>				

## TYPICAL CHARACTERISTICS

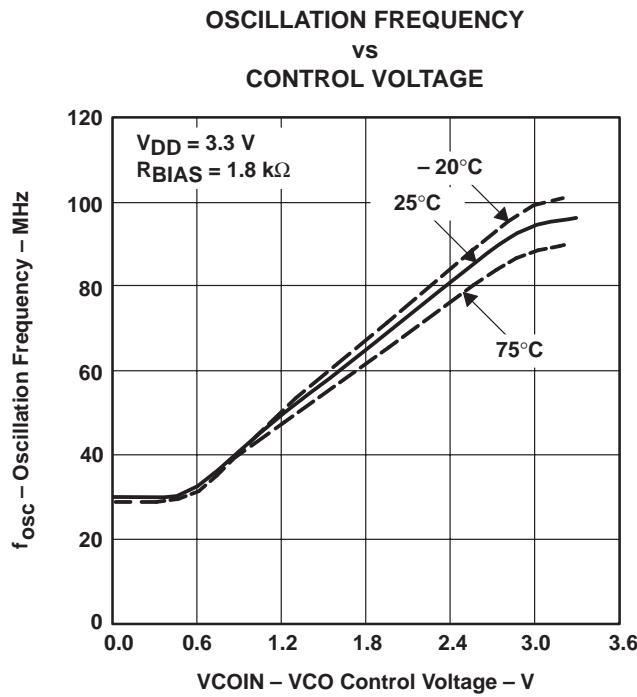


Figure 8

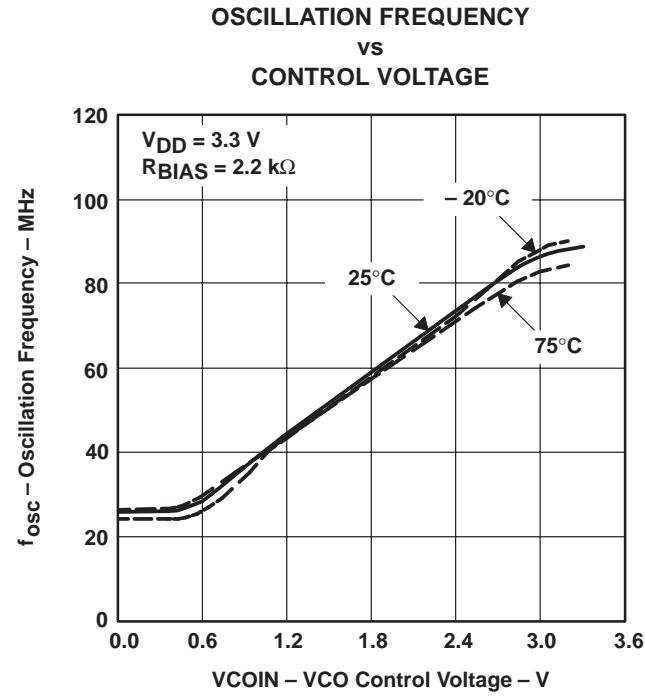


Figure 9

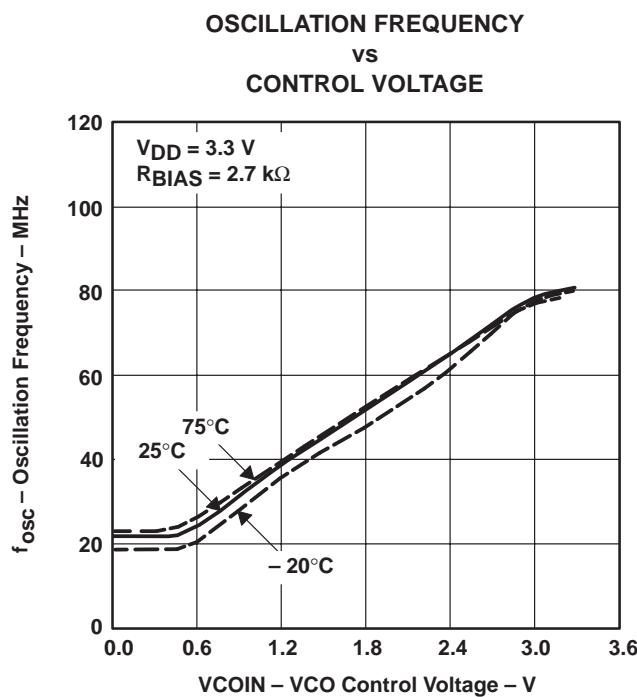


Figure 10

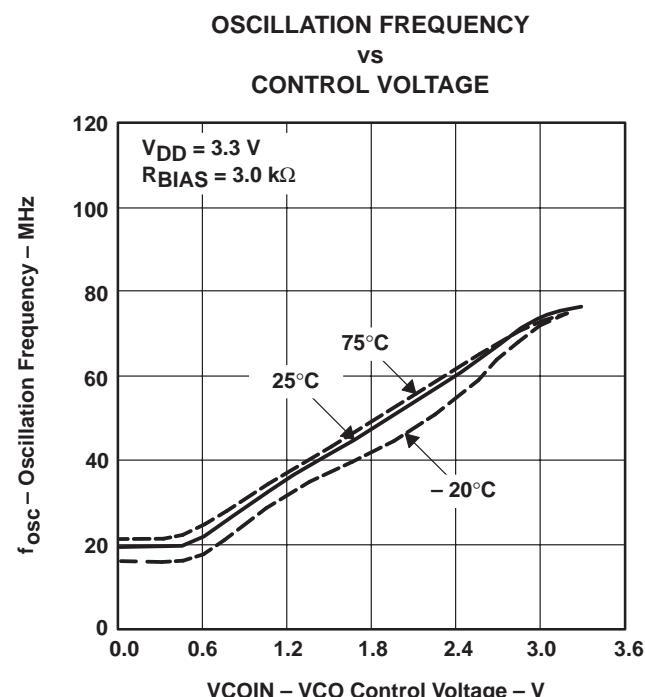
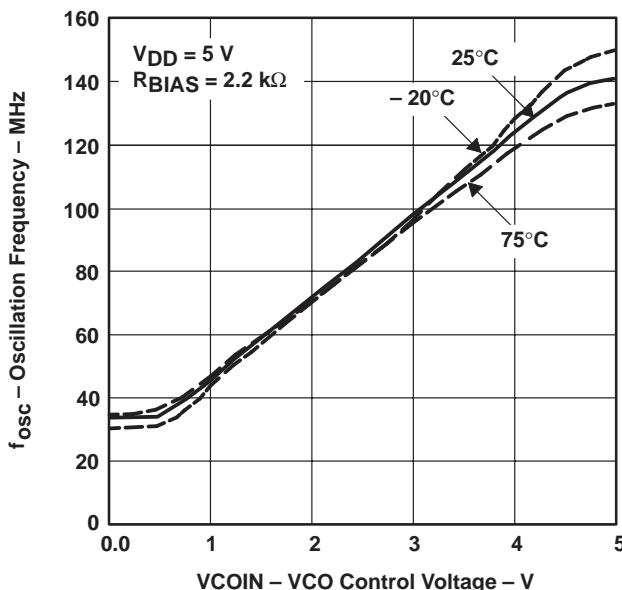


Figure 11

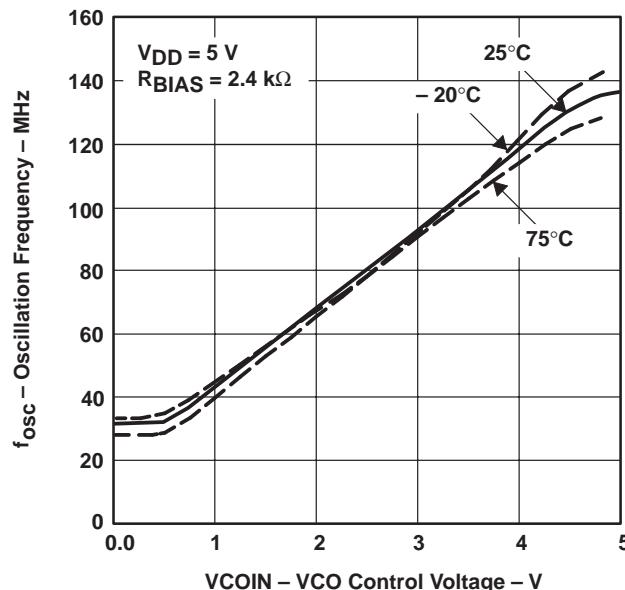
**TYPICAL CHARACTERISTICS**

**OSCILLATION FREQUENCY  
vs  
CONTROL VOLTAGE**



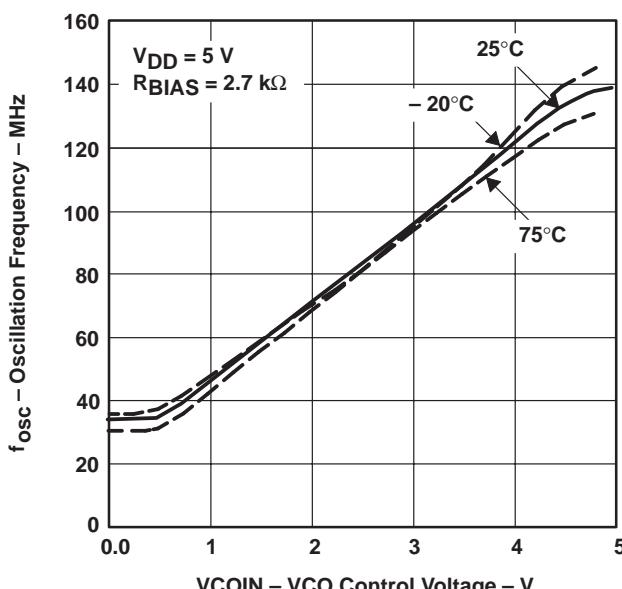
**Figure 12**

**OSCILLATION FREQUENCY  
vs  
CONTROL VOLTAGE**



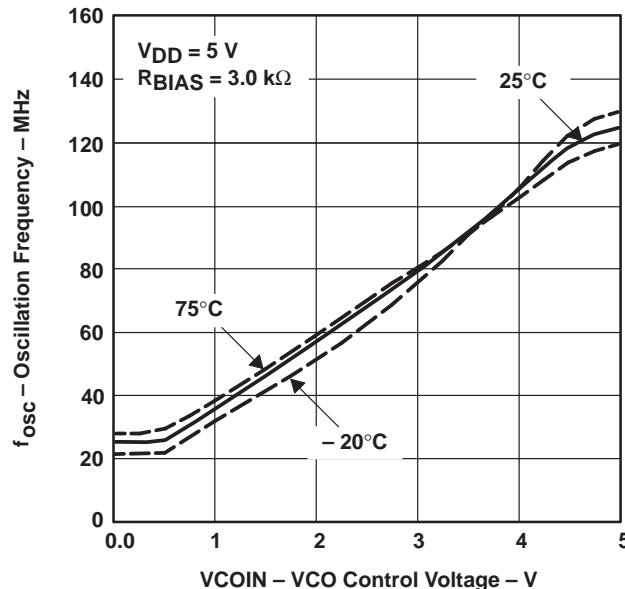
**Figure 13**

**OSCILLATION FREQUENCY  
vs  
CONTROL VOLTAGE**



**Figure 14**

**OSCILLATION FREQUENCY  
vs  
CONTROL VOLTAGE**



**Figure 15**

## TYPICAL CHARACTERISTICS

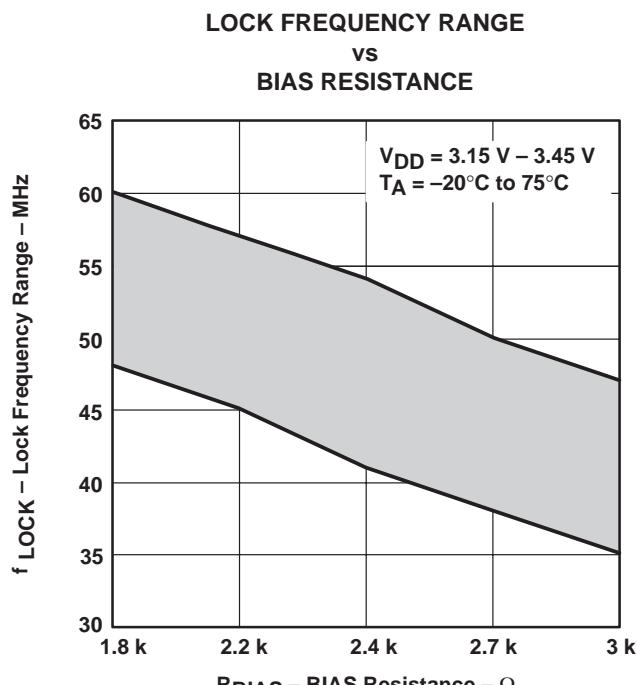


Figure 16

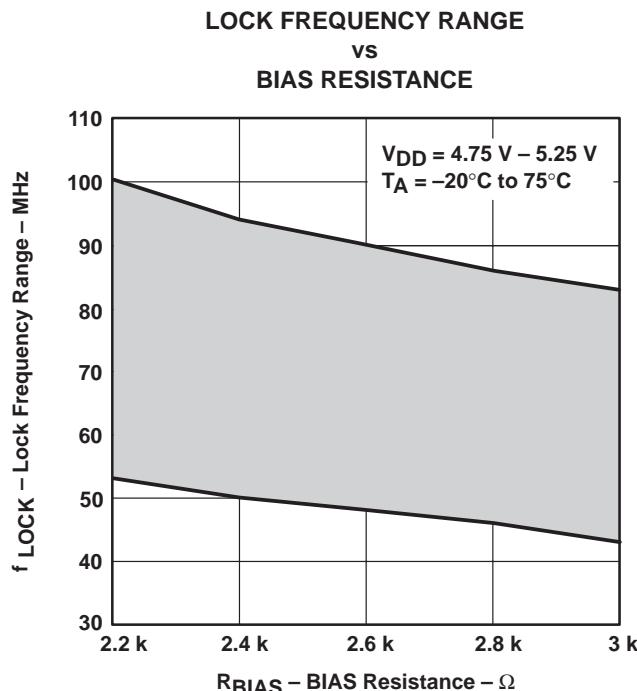


Figure 17

## APPLICATION INFORMATION

### gain of VCO and PFD

Figure 18 is a block diagram of the PLL. The divider N value depends on the input frequency and the desired VCO output frequency according to the system application requirements. The  $K_p$  and  $K_V$  values are obtained from the operating characteristics of the device as shown in Figure 18.  $K_p$  is defined from the phase detector  $V_{OL}$  and  $V_{OH}$  specifications and the equation shown in Figure 18(b).  $K_V$  is defined from Figures 8, 9, 10, and 11 as shown in Figure 18(c).

The parameters for the block diagram with the units are as follows:

$K_V$  : VCO gain (rad/s/V)  
 $K_p$  : PFD gain (V/rad)  
 $K_f$  : LPF gain (V/V)  
 $K_N$  : countdown divider gain (1/N)

### external counter

When a large N counter is required by the application, there is a possibility that the PLL response becomes slow due to the counter response delay time. In the case of a high frequency application, the counter delay time should be accounted for in the overall PLL design.

### $R_{BIAS}$

The external bias resistor sets the VCO center frequency with  $1/2 V_{DD}$  applied to the VCO IN terminal. For the most accurate results, a metal-film resistor is the better choice, but a carbon-composition resistor can also be used with excellent results. A  $0.22 \mu F$  capacitor should be connected from the BIAS terminal to ground as close to the device terminals as possible.

### hold-in range

From the technical literature, the maximum hold-in range for an input frequency step for the three types of filter configurations shown in Figure 17 is as follows:

$$\Delta\omega_H \approx 0.8 (K_p) (K_V) (K_f(\infty)) \quad (1)$$

Where

$K_f(\infty)$  = the filter transfer function value at  $\omega = \infty$

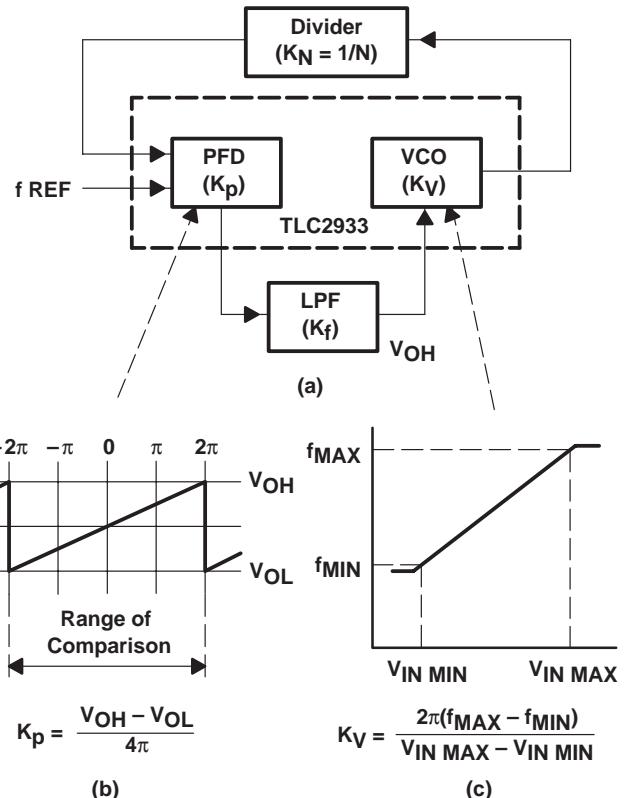


Figure 18. Example of a PLL Block Diagram

## APPLICATION INFORMATION

## low-pass-filter (LPF) configurations

References that include detailed design information about LPFs should be consulted for additional information. Lag-lead filters or active filters are often used. Examples of LPFs are shown in Figure 19. When the active filter of Figure 19(c) is used, the reference should be applied to  $F_{IN\text{-}B}$  because of the amplifier inversion. Also, in practical filter implementations,  $C_2$  is used as additional filtering at the VCO input. The value of  $C_2$  should be equal to or less than one tenth the value of  $C_1$ .

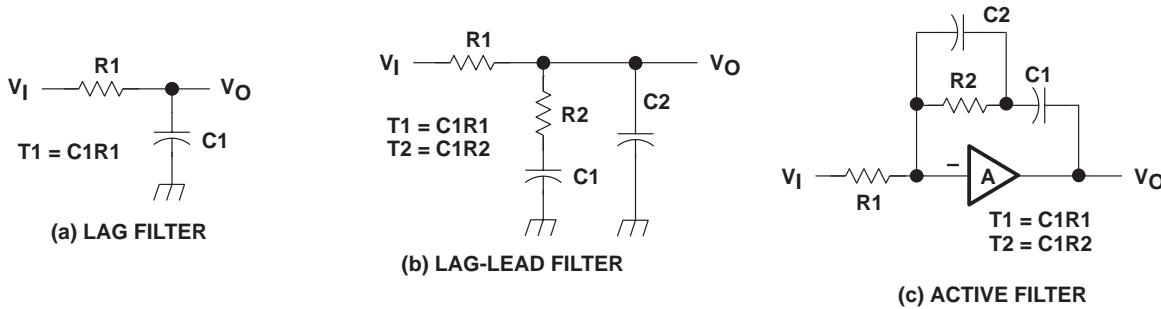


Figure 19. LPF Examples for PLL

## passive filter

The transfer function for the low-pass filter shown in Figure 17(b) is;

$$\frac{V_O}{V_{IN}} = \frac{1 + s \times T_2}{1 + s \times (T_1 + T_2)} \quad (2)$$

Where

$$T_1 = R_1 \times C_1 \text{ and } T_2 = R_2 \times C_1$$

Using this filter makes the closed-loop PLL system a type 1 second-order system. The response curves of this system to a unit step are shown in Figure 20.

## active filter

When using the active filter shown in Figure 19(c), the phase detector inputs must be reversed, since the filter adds an additional inversion. Therefore, the input reference frequency should be applied to the  $F_{IN\text{-}B}$  terminal and the output of the VCO divider should be applied to the input reference terminal,  $F_{IN\text{-}A}$ .

The transfer function for the active filter shown in Figure 19(c) is:

$$F(s) = \frac{1 + s \times R_2 \times C_1}{s \times R_1 \times C_1} \quad (3)$$

Using this filter makes the closed-loop PLL system a type 2 second-order system. The response curves of this system to a unit step are shown in Figure 21.

## APPLICATION INFORMATION

Using the lag-lead filter in Figure 19(b) and divider N value, the transfer function for phase and frequency are shown in equations 4 and 5. Note that the transfer function for phase differs from the transfer function for frequency by only the divider N value. The difference arises from the fact that the feedback for phase is unity, while the feedback for frequency is 1/N.

Hence, the transfer function of Figure 19(a) for phase is

$$\frac{\Phi_2(s)}{\Phi_1(s)} = \frac{K_p \times K_V}{N \times (T_1 + T_2)} \left[ \frac{1 + s \times T_2}{s^2 + s \times \left[ 1 + \frac{K_p \times K_V \times T_2}{N \times (T_1 + T_2)} \right] + \frac{K_p \times K_V}{N \times (T_1 + T_2)}} \right] \quad (4)$$

and the transfer function for frequency is

$$\frac{F_{OUT}(s)}{F_{REF}(s)} = \frac{K_p \times K_V}{(T_1 + T_2)} \left[ \frac{1 + s \times T_2}{s^2 + s \times \left[ 1 + \frac{K_p \times K_V \times T_2}{N \times (T_1 + T_2)} \right] + \frac{K_p \times K_V}{N \times (T_1 + T_2)}} \right] \quad (5)$$

The standard 2-pole denominator is  $D = s^2 + 2\zeta\omega_n s + \omega_n^2$  and comparing the coefficients of the denominator of equation (4) and (5) with the standard 2-pole denominator gives the following results.

$$\omega_n = \sqrt{\frac{K_p \times K_V}{N \times (T_1 + T_2)}} \quad (6)$$

Solving for  $T_1 + T_2$

$$T_1 + T_2 = \frac{K_p \times K_V}{N \times \omega_n^2}$$

and by using this value for  $T_1 + T_2$  in equation (6) the damping factor is

$$\zeta = \frac{\omega_n}{2} \times \left( T_2 + \frac{N}{K_p \times K_V} \right) \quad (7)$$

solving for  $T_2$

$$T_2 = \frac{2\zeta}{\omega} - \frac{N}{K_p \times K_V} \quad (8)$$

then by substituting for  $T_2$  in equation (6)

$$T_1 = \frac{K_V \times K_p}{N \times \omega_n^2} - \frac{2\zeta}{\omega_n} + \frac{N}{K_p \times K_V} \quad (9)$$

**APPLICATION INFORMATION**

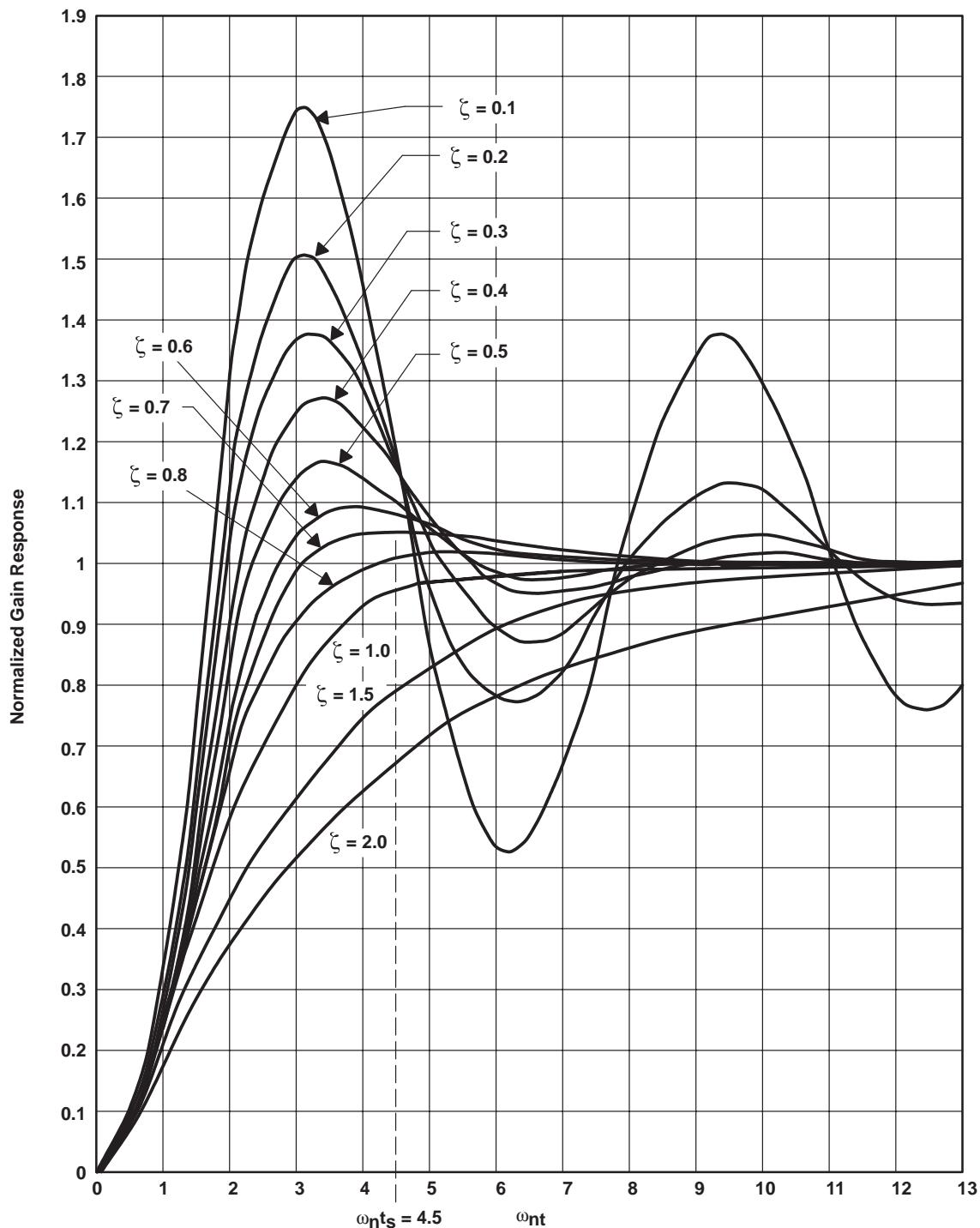
From the circuit constants and the initial design parameters then

$$R2 = \left[ \frac{2 \zeta}{\omega_n} - \frac{N}{K_p \times K_V} \right] \frac{1}{C1} \quad (10)$$

$$R1 = \left[ \frac{K_p \times K_V}{\omega_n^2 \times N} - \frac{2 \zeta}{\omega_n} + \frac{N}{K_p \times K_V} \right] \frac{1}{C1} \quad (11)$$

The capacitor, C1, is usually chosen between 1  $\mu$ F and 0.1  $\mu$ F to allow for reasonable resistor values and physical capacitor size.

**APPLICATION INFORMATION**



**Figure 20. Type 1 Second-Order Step Response**

## APPLICATION INFORMATION

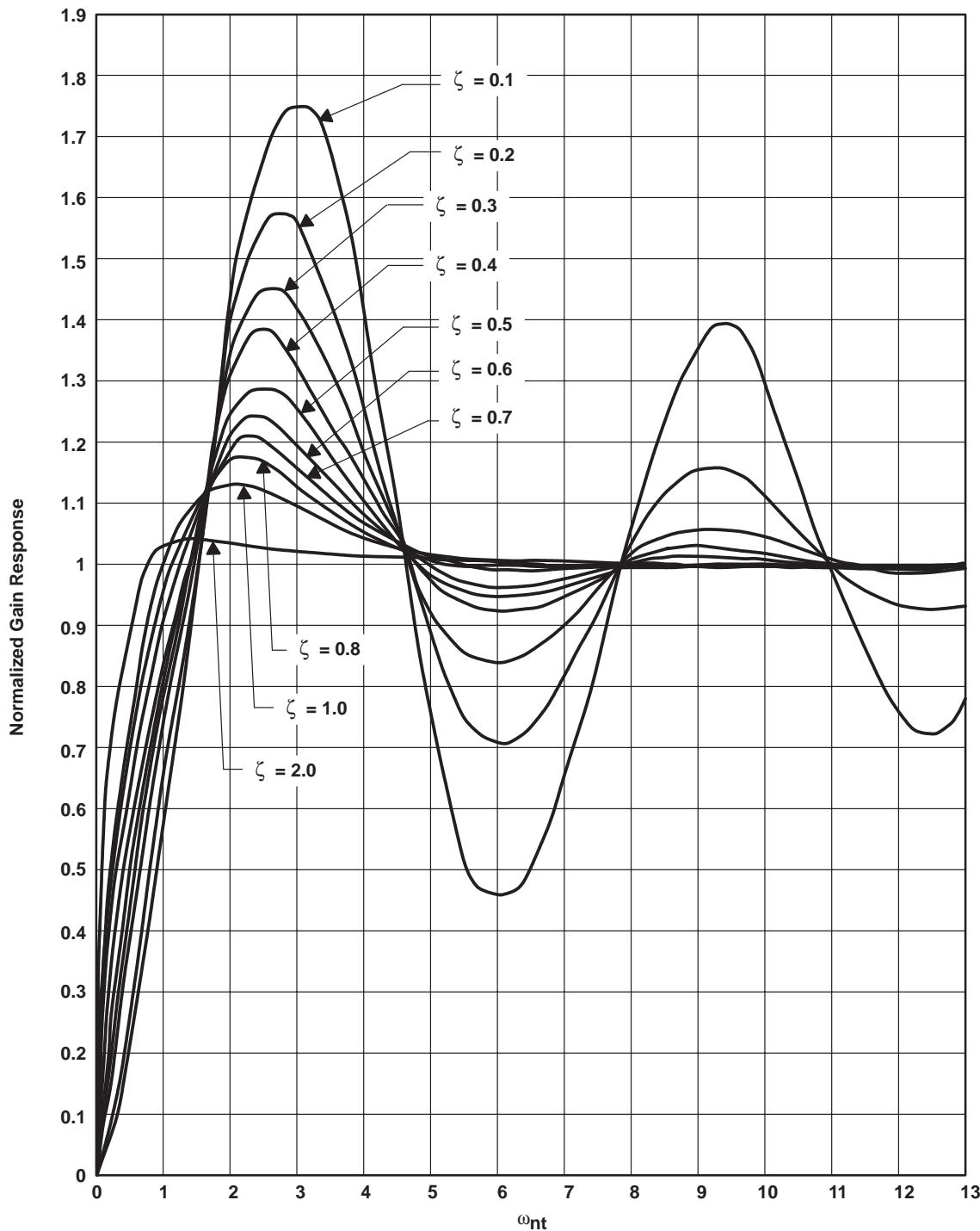


Figure 21. Type 2 Second-Order Step Response

## APPLICATION INFORMATION

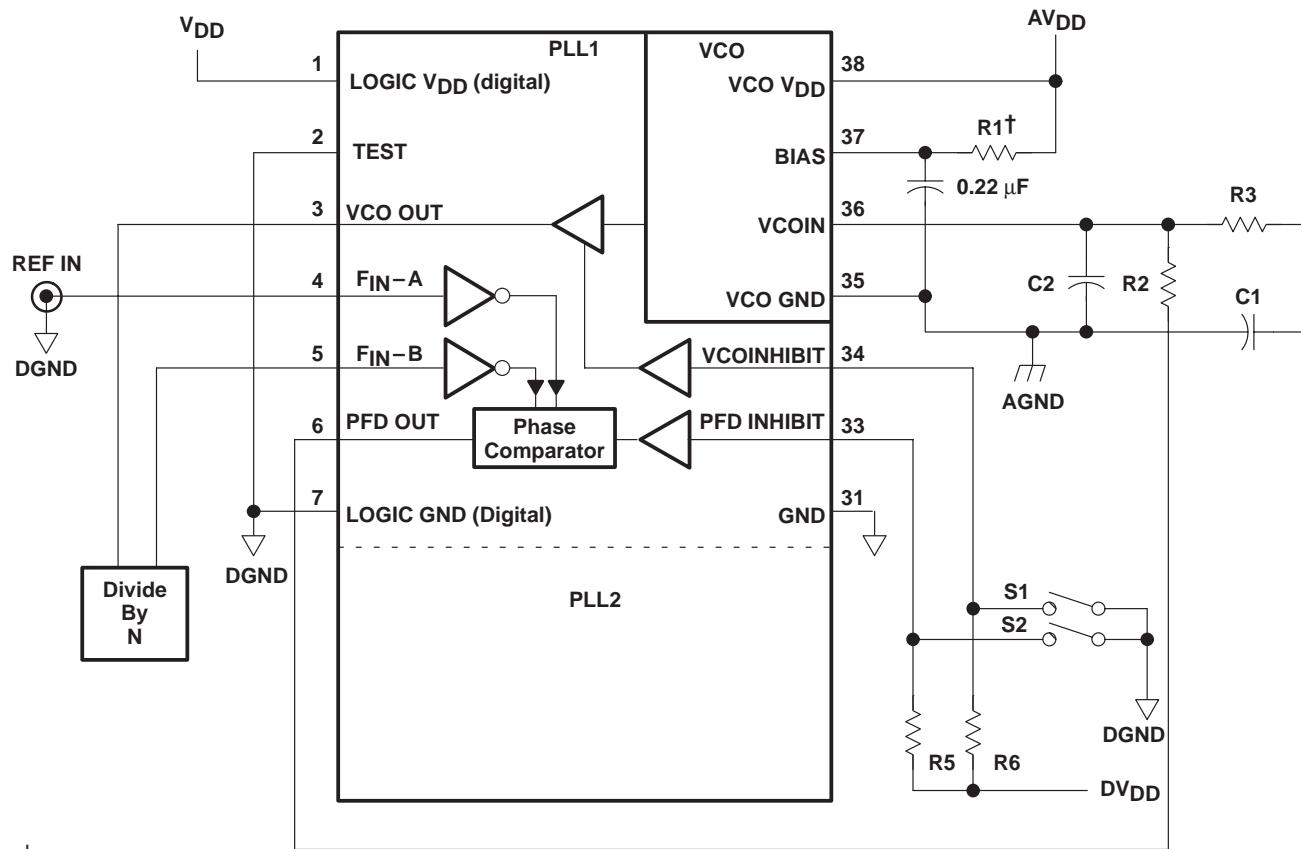
### PCB layout considerations

The TLC2943 contains high frequency analog oscillators; therefore, very careful breadboarding and printed-circuit-board (PCB) layout is required for evaluation.

The following design recommendations benefit the TLC2943 user:

- External analog and digital circuitry should be physically separated and shielded as much as possible to reduce system noise.
- RF breadboarding or RF PCB techniques should be used throughout the evaluation and production process.
- Wide ground leads or a ground plane should be used on the PCB layouts to minimize parasitic inductance and resistance. The ground plane is the better choice for noise reduction.
- LOGIC V<sub>DD</sub> and VCO V<sub>DD</sub> should be separate PCB traces and connected to the best filtered supply point available in the system to minimize supply cross-coupling.
- VCO V<sub>DD</sub> to GND and LOGIC V<sub>DD</sub> to GND should be decoupled with a 0.1- $\mu$ F capacitor placed as close as possible to the appropriate device terminals.
- The no-connection (NC) terminal on the package should be connected to GND.

The evaluation and operation schematic for the TLC2943 is shown in Figure 22.



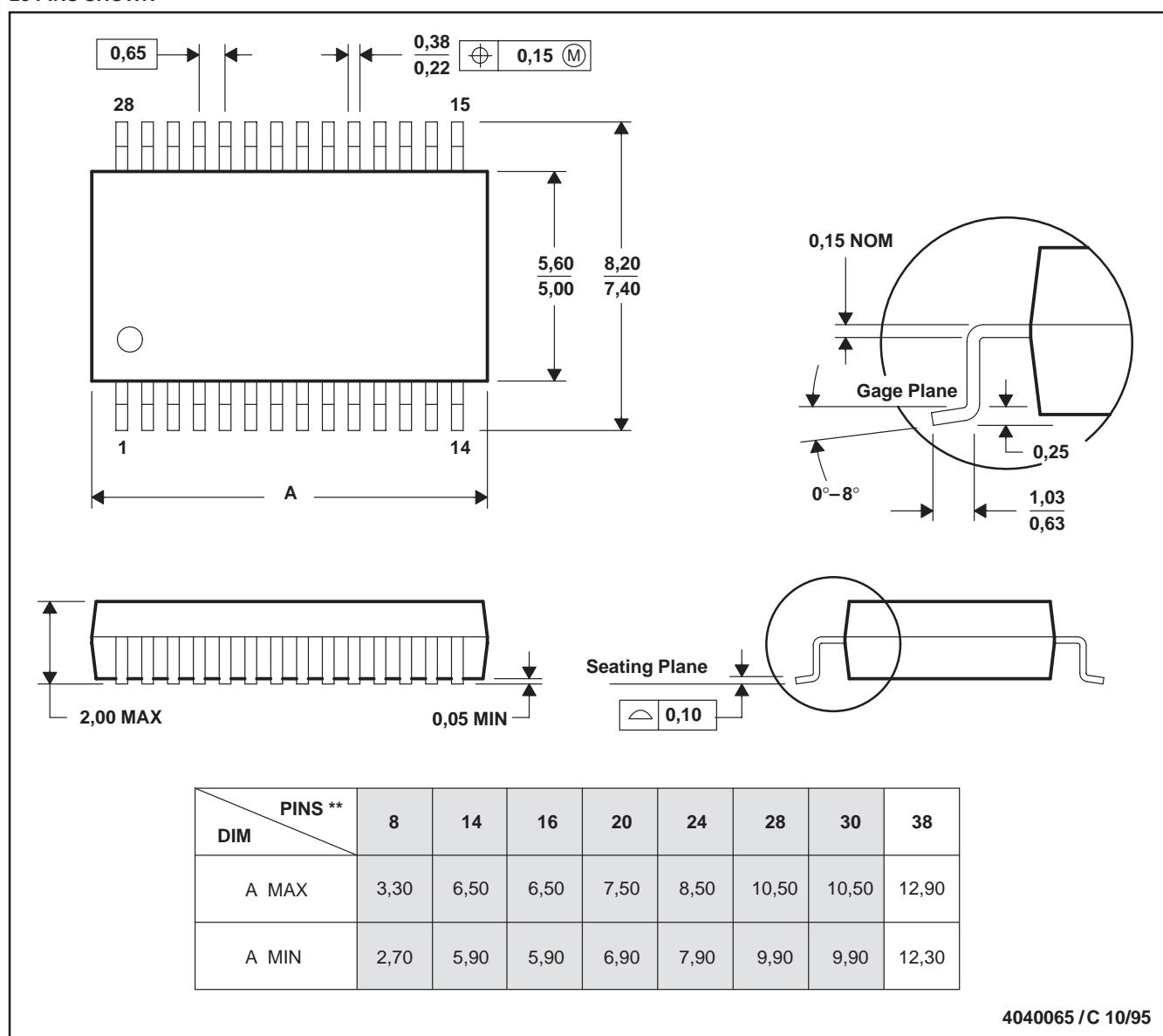
† R<sub>BIAS</sub> resistor

**Figure 22. Evaluation and Operation Schematic**

## MECHANICAL DATA

DB (R-PDSO-G\*\*) 28 PINS SHOWN

PLASTIC SMALL-OUTLINE PACKAGE



NOTES: A. All linear dimensions are in millimeters.  
 B. This drawing is subject to change without notice.  
 C. Body dimensions do not include mold flash or protrusion not to exceed 0,15.  
 D. Falls within JEDEC MO-150

**PACKAGING INFORMATION**

Orderable Device	Status <sup>(1)</sup>	Package Type	Package Drawing	Pins	Package Qty	Eco Plan <sup>(2)</sup>	Lead/Ball Finish	MSL Peak Temp <sup>(3)</sup>
TLC2943IDB	OBsolete	SSOP	DB	38		TBD	Call TI	Call TI
TLC2943IDBR	OBsolete	SSOP	DB	38		TBD	Call TI	Call TI

<sup>(1)</sup> The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBsolete:** TI has discontinued the production of the device.

<sup>(2)</sup> Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

<sup>(3)</sup> MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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Low Power Wireless	<a href="http://www.ti.com/lpw">www.ti.com/lpw</a>	Telephony	<a href="http://www.ti.com/telephony">www.ti.com/telephony</a>
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