

# Digital DC/DC PMBus 17A Module

## ZL9117M

The ZL9117M is a 17A, variable output, step-down PMBus-compliant digital power supply. Included in the module is a high-performance digital PWM controller, power MOSFETs, an inductor, and all the passive components required for a highly integrated DC/DC power solution. This power module has built-in auto-compensation algorithms, which eliminates the need for manual compensation design work. The ZL9117M operates over a wide input voltage range and supports an output voltage range of 0.6V to 3.6V, which can be set by external resistors or via PMBus. This high-efficiency power module is capable of delivering 17A. Only bulk input and output capacitors are needed to finish the design. The output voltage can be precisely regulated to as low as 0.6V with  $\pm 1\%$  output voltage regulation over line, load, and temperature variations.

**The ZL9117M features auto-compensation, internal soft-start, auto-recovery overcurrent protection, an enable option, and pre-biased output start-up capabilities.**

The ZL9117M is packaged in a thermally enhanced, compact (15mmx15mm) and low profile (3.5mm) over-molded QFN package module suitable for automated assembly by standard surface mount equipment. The ZL9117M is Pb-free and RoHS compliant.

**Figure 1 represents a typical implementation of the ZL9117M. For PMBus operation, it is recommended to tie the Enable pin (EN) to SGND.**

## Features

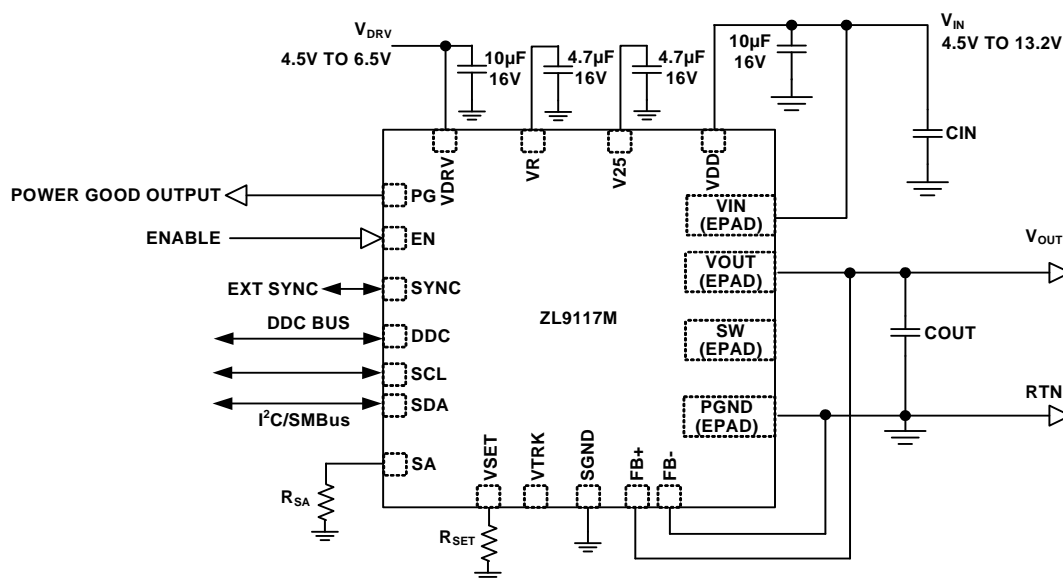
- Complete digital switch mode power supply
- Fast transient response
- Auto compensating PID filter
- External synchronization
- Output voltage tracking
- Current sharing
- Programmable soft-start delay and ramp
- Overcurrent/undercurrent protection
- PMBus compliant

## Applications

- Server, telecom, and datacom
- Industrial and medical equipment
- General purpose point of load

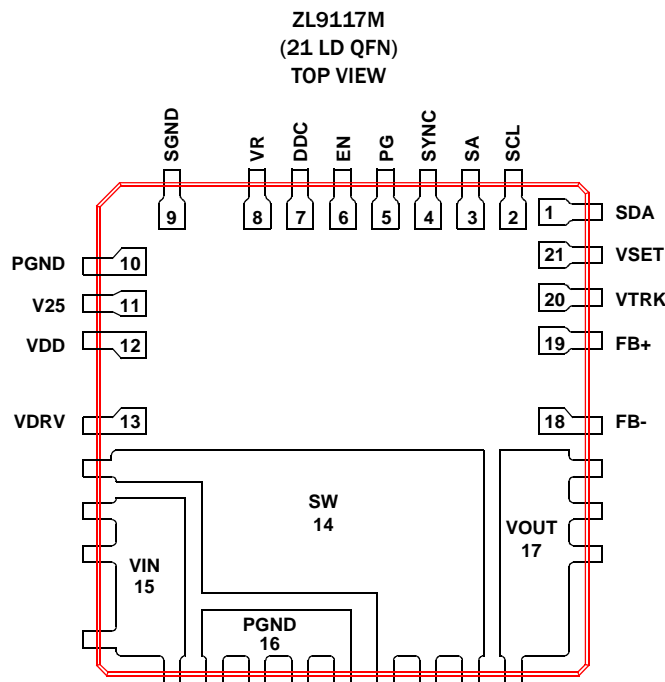
## Related Literature

- See [AN2033](#), “Zilker Labs PMBus Command Set for DDC Products”
- See [AN2034](#), “Configuring Current Sharing on the ZL2004 and ZL2006”



**FIGURE 1. A COMPLETE DIGITAL SWITCH MODE POWER SUPPLY, ONLY BULK INPUT AND OUTPUT CAPACITORS ARE REQUIRED TO FINISH THE DESIGN**

## Pin Configuration



## Pin Descriptions

PIN	LABEL	TYPE	DESCRIPTION
1	SDA	I/O	Serial data. A pull-up resistor is required for this application.
2	SCL	I/O	Serial clock. A pull-up resistor is required for this application.
3	SA	I	Serial address select pin. Used to assign unique SMBus address to each module.
4	SYNC	I/O	Clock synchronization. Used for synchronization to external frequency reference.
5	PG	O	Power-good output.
6	EN	I	Enable input (factory setting active high). Pull-up to enable PWM switching and pull-down to disable PWM switching.
7	DDC	I/O	Digital-DC bus (open drain). Interoperability between Zilker Labs modules. A pull-up resistor is required for this application.
8	VR	PWR	Internal 5V reference used to power internal drivers. Connect 4.7μF bypass capacitor to this pin.
9	SGND	PWR	Signal ground. Connect to low impedance ground plane.
10	PGND	PWR	Power ground. Connect to low impedance ground plane.
11	V25	PWR	Internal 2.5V reference used to power internal circuitry. Connect 4.7μF bypass capacitor to this pin.
12	VDD	PWR	Input supply voltage for controller. Connect 4.7μF bypass capacitor to this pin.
13	VDRV	PWR	Power supply for internal FET drivers. Connect 10μF bypass capacitor to this pin.
14 (epad)	SW	PWR	Drive train switch node.
15 (epad)	VIN	PWR	Power supply input FET voltage.
16 (epad)	PGND	PWR	Power ground. Connect to low impedance ground plane.
17 (epad)	VOUT	PWR	Power supply output voltage. Output voltage from PWM.
18	FB-	I	Output voltage feedback. Connect to load return of ground regulation point.
19	FB+	I	Output voltage feedback. Connect to output regulation point.
20	VTRK	I	Tracking sense input. Used to track an external voltage source.
21	VSET	I	Output voltage selection pin. Used to set V <sub>OUT</sub> set point and V <sub>OUT</sub> max.

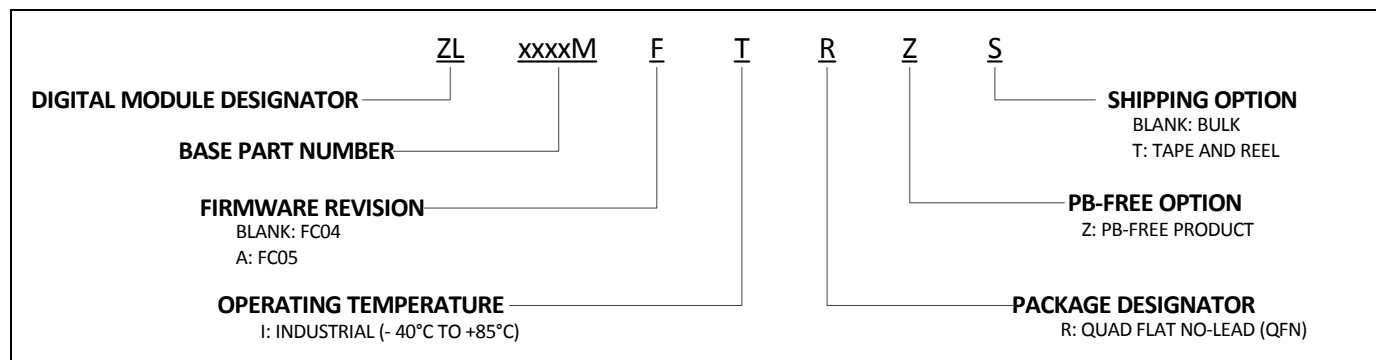
# ZL9117M

## Ordering Information

PART NUMBER (Notes 1, 2, 3)	PART MARKING	TEMP RANGE (°C)	PACKAGE (Pb-Free)	PKG. DWG. #
ZL9117MIRZ	ZL9117M	-40 to +85	21 Ld 15x15 QFN	L21.15x15
ZL9117MAIRZ	ZL9117MA	-40 to +85	21 Ld 15x15 QFN	L21.15x15

### NOTES:

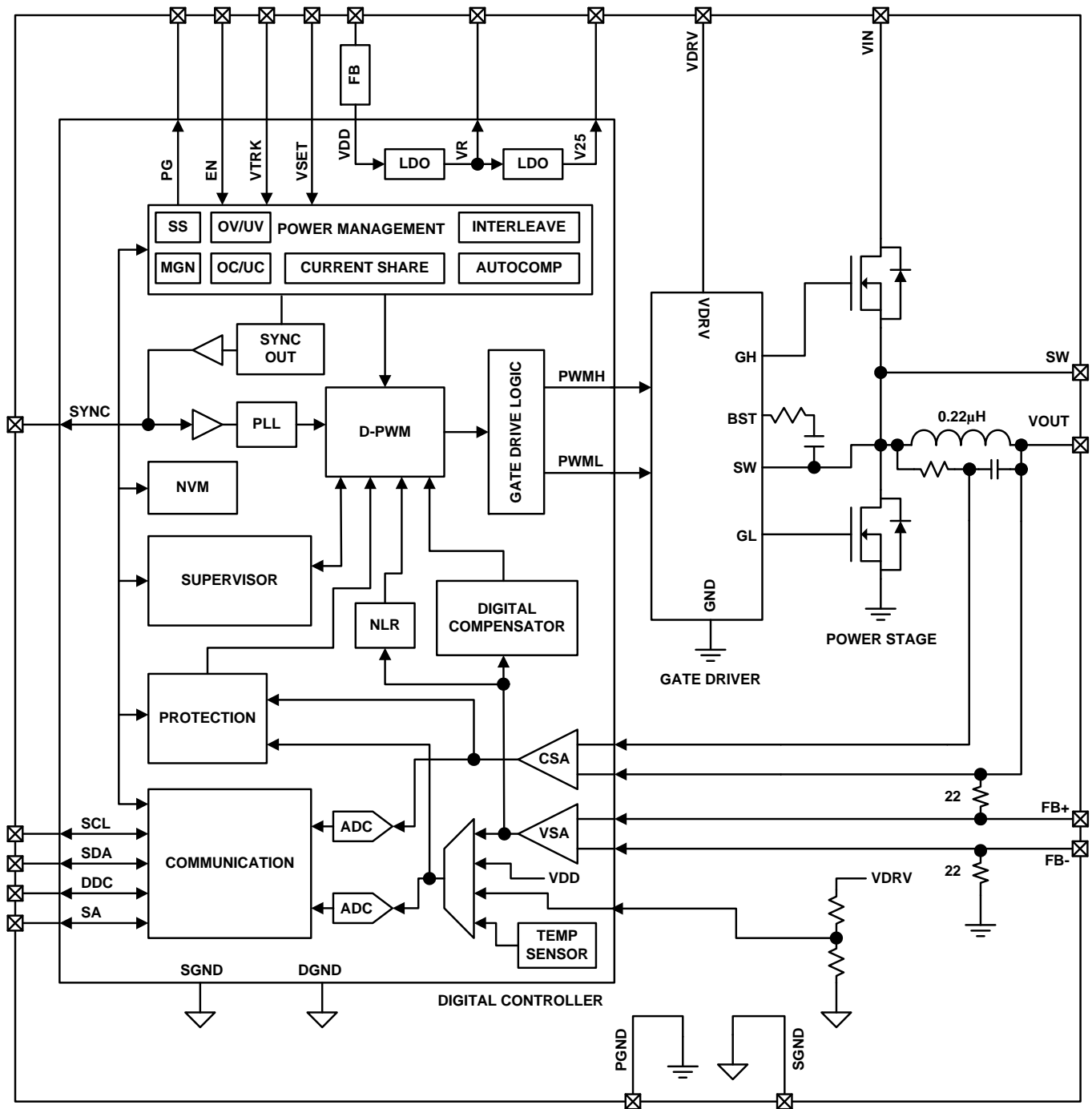
1. Add "-T\*" suffix for tape and reel. Please refer to [TB347](#) for details on reel specifications.
2. These Intersil Pb-free plastic packaged products employ special Pb-free material sets, molding compounds/die attach materials, and 100% matte tin plate plus anneal (e3 termination finish, which is RoHS compliant and compatible with both SnPb and Pb-free soldering operations). Intersil Pb-free products are MSL classified at Pb-free peak reflow temperatures that meet or exceed the Pb-free requirements of IPC/JEDEC J STD-020.
3. For Moisture Sensitivity Level (MSL), please see device information page for [ZL9117M](#). For more information on MSL please see Tech Brief [TB363](#).



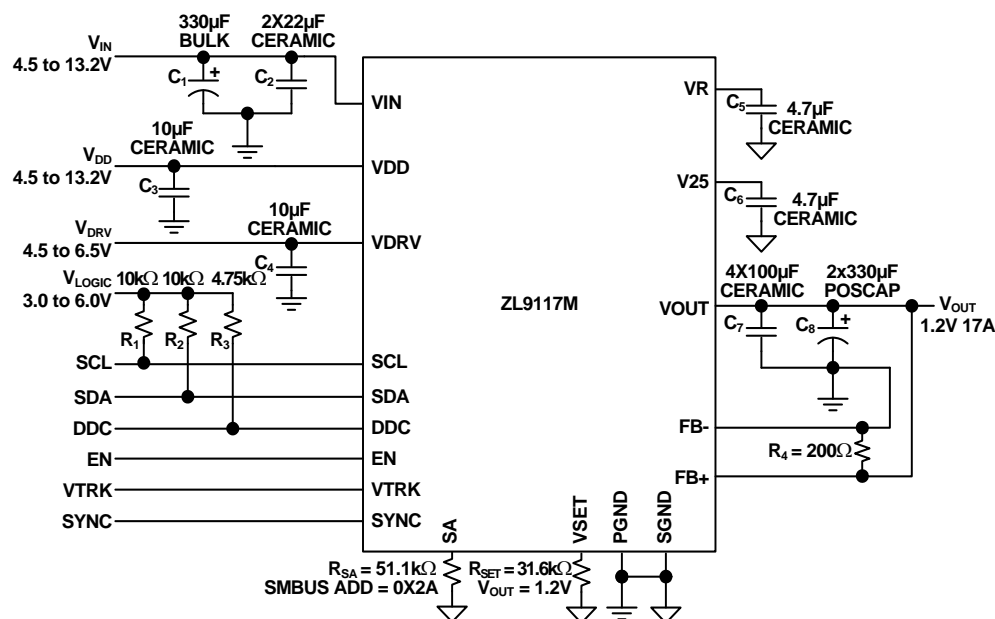
## Firmware Revision History

Firmware Revision Code	Change Description	Note
FC04		Not recommended for a new design.
FC05	<ol style="list-style-type: none"><li>1. Bug fixed to clear VMON_UV_WARNING when VMON (VDRV) voltage is ramped up with a delayed of &gt;50ms from VIN.</li><li>2. Make OVUV_CONFIG = 0x00 a factory default.</li><li>3. Make DEADTIME = 1410 Freeze a factory default.</li></ol>	Recommended for a new design.

## ZL9117M Internal Block Diagram



## Typical Application - Single Module



### NOTES:

4.  $R_1$  and  $R_2$  are not required if the PMBus host already has I<sup>2</sup>C pull-up resistors.
5. Only one  $R_3$  per DDC bus is required when DDC bus is shared with other modules.
6. The VR, V25, VDRV, and VDD capacitors should be placed no farther than 0.5cm from the pin.
7.  $R_4$  is optional but recommended to sink possible ~100 $\mu$ A backflow current from the FB+ pin. Backflow current is present only when the module is in a disabled state with power still available at the V<sub>DD</sub> pin.
8. When Low-Side power FET is selected to be enabled as a response to an OV fault, it is recommended to place a Schottky diode close to the VOUT and PGND pins in order to prevent voltage at the FB+ pin dropping below absolute minimum of -0.3V, which may be caused by negative current build up on the internal power inductor.

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## Absolute Maximum Ratings (Note 9)

DC Supply Voltage for VDD Pin	-0.3V to 15.7V
Input Voltage for VIN Pin	-0.3V to 15.7V
MOSFET Drive Reference for VR Pin	-0.3V to 6.5V
2.5V Logic Reference for V25 Pin	-0.3V to 3V
MOSFET Driver Power for VDRV Pin	-0.3V to 7.5V
Logic I/O Voltage for DDC, EN, FB+, FB-, PG, SA, SCL, SDA, SYNC, VSET Pins	-0.3V to 6V
ESD Rating	
Human Body Model (Tested per JESD22-A114F)	2000V
Machine Model (Tested per JESD22-A115C)	200V
Charged Device Model (Tested per JESD22-C110D)	1000V
Latch Up (Tested per JESD78C; Class 2, Level A)	100mA

## Thermal Information

Thermal Resistance (Typical)	$\theta_{JA}$ (°C/W)	$\theta_{JC}$ (°C/W)
QFN Package (Notes 12, 13)	11.5	2.2
Junction Temperature	-55°C to +150°C	
Storage Temperature	-55°C to +150°C	
Pb-Free Reflow Profile	see link below <a href="http://www.intersil.com/pbfree/Pb-FreeReflow.asp">http://www.intersil.com/pbfree/Pb-FreeReflow.asp</a>	

## Recommended Operating Conditions

Input Supply Voltage Range, $V_{IN}$	4.5V to 13.2V
Input Supply For Controller, $V_{DD}$ (Note 10)	4.5V to 13.2V
Driver Supply Voltage, $V_{DRV}$	4.5V to 6.5V
Output Voltage Range, $V_{OUT}$ (Note 11)	0.54V to 3.6V
Output Current Range, $I_{OUT(DC)}$ (Note 24)	0A to 17A
Operating Junction Temperature Range, $T_J$	-40°C to +125°C

CAUTION: Do not operate at or near the maximum ratings listed for extended periods of time. Exposure to such conditions may adversely impact product reliability and result in failures not covered by warranty.

### NOTES:

- Voltage measured with respect to SGND.
- $V_{IN}$  supplies the power FETs.  $V_{DD}$  supplies the controller.  $V_{IN}$  can be tied to  $V_{DD}$ . For  $V_{DD} \leq 5.5V$ ,  $V_{DD}$  should be tied to VR.
- Includes  $\pm 10\%$  margin limits.
- $\theta_{JA}$  is simulated in free air with device mounted on a four-layer FR-4 test board (76.2 x 114.3 x 1.6mm) with 80% coverage, 2oz Cu on top and bottom layers, plus two, buried, one-ounce Cu layers with coverage across the entire test board area. Multiple vias were used, with via diameter = 0.3mm on 1.2mm pitch.
- For  $\theta_{JC}$ , the "case" temperature is measured at the center of the package underside.

**Electrical Specifications**  $V_{DD} = 12V$ ,  $T_A = -40^\circ C$  to  $+85^\circ C$  unless otherwise noted. Typical values are at  $T_A = +25^\circ C$ . **Boldface limits apply over the operating temperature range,  $-40^\circ C$  to  $+85^\circ C$ .**

PARAMETER	CONDITIONS	MIN (Note 14)	TYP (Note 15)	MAX (Note 14)	UNIT
<b>INPUT AND SUPPLY CHARACTERISTICS</b>					
Input Bias Supply Current, $I_{DD}$	$V_{IN} = V_{DD} = 13.2V$ , $f_{SW} = 571kHz$ , No load	-	20	<b>40</b>	mA
Input Bias Shutdown Current, $I_{DDs}$	EN = 0V, No $I^2C$ /SMBus activity	-	15.5	<b>20</b>	mA
Input Supply Current, $I_{VIN}$	$V_{IN} = 12V$ , $I_{OUT} = 17A$ , $V_{OUT} = 1.0V$	-	1.78	-	A
Driver Supply Current, $I_{VDRV}$	$V_{DRV} = 6V$ , $V_{OUT} = 1.0V$ , $f_{SW} = 571Hz$ , NO Load	-	25	-	mA
VR Reference Output Voltage (Note 16)	$V_{DD} > 6V$ , $I_{VR} < 20mA$	<b>4.5</b>	5.2	<b>5.7</b>	V
V25 Reference Output Voltage (Note 16)	$V_R > 3V$ , $I_{V25} < 20mA$	<b>2.25</b>	2.5	<b>2.75</b>	V
<b>OUTPUT CHARACTERISTICS</b>					
Output Load Current (Notes 23, 24)	$V_{IN} = 12V$ , $V_{OUT} = 1.0V$	-	-	17	A
Output Voltage Accuracy (Note 16, 17)	Include Line, Load, Temp	<b>-1</b>	-	<b>+1</b>	%
Peak-to-peak Output Ripple Voltage, $\Delta V_{OUT}$ (Note 17)	$I_{OUT} = 17A$ , $V_{OUT} = 1.0V$ , $C_{OUT} = 3000\mu F$	-	6	-	mV
Soft-start Delay Duration Range (Notes 16, 18)	Set using $I^2C$ /SMBus	<b>2</b>	-	<b>200</b>	ms
Soft-start Delay Duration Accuracy (Note 16)	Turn-on delay (precise mode) (Notes 18, 19)	-	$\pm 0.25$	-	ms
	Turn-on delay (normal mode) (Note 20)	-	-0.25/+4	-	ms
	Turn-off delay (Note 20)	-	-0.25/+4	-	ms
Soft-start Ramp Duration Range (Note 16)	Set using $I^2C$	<b>0</b>	-	<b>200</b>	ms
Soft-start Ramp Duration Accuracy (Note 16)		-	100	-	$\mu s$
<b>DYNAMIC CHARACTERISTICS</b>					
Voltage Change for Positive Load Step	$\Delta I_{OUT} = 6A$ , slew rate = $2.5A/\mu s$ , $V_{OUT} = 1.0V$ , $C_{OUT} = 3000\mu F$	-	3	-	%
Voltage Change for Negative Load Step	$\Delta I_{OUT} = 6A$ , slew rate = $2.5A/\mu s$ , $V_{OUT} = 1.0V$ , $C_{OUT} = 3000\mu F$	-	3	-	%

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**Electrical Specifications**  $V_{DD} = 12V$ ,  $T_A = -40^{\circ}C$  to  $+85^{\circ}C$  unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ . **Boldface limits apply over the operating temperature range,  $-40^{\circ}C$  to  $+85^{\circ}C$ .** (Continued)

PARAMETER	CONDITIONS	MIN (Note 14)	TYP (Note 15)	MAX (Note 14)	UNIT
<b>OSCILLATOR AND SWITCHING CHARACTERISTICS (Note 16)</b>					
Switching Frequency Range		<b>500</b>	571	<b>1000</b>	kHz
Maximum PWM Duty Cycle	Factory setting	<b>95</b>	–	–	%
Minimum SYNC Pulse Width		<b>150</b>	–	–	ns
Input Clock Frequency Drift Tolerance	External clock source	<b>-13</b>	–	<b>13</b>	%
<b>LOGIC INPUT/OUTPUT CHARACTERISTICS (Note 16)</b>					
Logic Input Bias Current	EN, PG, SCL, SDA pins	<b>-10</b>	–	<b>10</b>	$\mu A$
Logic Input Low, $V_{IL}$		–	–	<b>0.8</b>	V
Logic Input High, $V_{IH}$		<b>2.0</b>	–	–	V
Logic Output Low, $V_{OL}$	$I_{OL} \leq 4mA$ (Note 22)	–	–	<b>0.4</b>	V
Logic Output High, $V_{OH}$	$I_{OH} \geq -2mA$ (Note 22)	<b>2.25</b>	–	–	V
<b>FAULT PROTECTION CHARACTERISTICS (Note 16)</b>					
UVLO Threshold Range	Configurable via I <sup>2</sup> C/SMBus	<b>2.85</b>	–	<b>16</b>	V
UVLO Set-point Accuracy		<b>-150</b>	–	<b>150</b>	mV
UVLO Hysteresis	Factory setting	–	3	–	%
	Configurable via I <sup>2</sup> C/SMBus	<b>0</b>	–	<b>100</b>	%
UVLO Delay		–	–	<b>2.5</b>	$\mu s$
Power-Good $V_{OUT}$ Threshold	Factory setting	–	90	–	% $V_{OUT}$
Power-Good $V_{OUT}$ Hysteresis	Factory setting	–	5	–	%
Power-Good Delay (Note 21)	Configurable via I <sup>2</sup> C/SMBus	<b>0</b>	–	<b>200</b>	ms
VSEN Undervoltage Threshold	Factory setting	–	85	–	% $V_{OUT}$
	Configurable via I <sup>2</sup> C/SMBus	<b>0</b>	–	<b>110</b>	% $V_{OUT}$
VSEN Overvoltage Threshold	Factory setting	–	<b>115</b>	–	% $V_{OUT}$
	Configurable via I <sup>2</sup> C/SMBus	<b>0</b>	–	<b>115</b>	% $V_{OUT}$
VSEN Undervoltage Hysteresis		–	5	–	% $V_{OUT}$
VSEN Undervoltage/Overvoltage Fault Response Time	Factory setting	–	<b>16</b>	–	$\mu s$
	Configurable via I <sup>2</sup> C/SMBus	<b>5</b>	–	<b>60</b>	$\mu s$
Thermal Protection Threshold (Controller Junction Temperature)	Factory setting	–	<b>125</b>	–	$^{\circ}C$
	Configurable via I <sup>2</sup> C/SMBus	<b>-40</b>	–	<b>125</b>	$^{\circ}C$
Thermal Protection Hysteresis		–	<b>15</b>	–	$^{\circ}C$

## NOTES:

- Compliance to datasheet limits is assured by one or more methods: production test, characterization and/or design.
- Parameters with TYP limits are not production tested unless otherwise specified.
- Parameters are 100% tested for internal controller prior to module assembly.
- $V_{OUT}$  measured at the termination of the FB+ and FB- sense points.
- The device requires a delay period following an enable signal and prior to ramping its output. Precise timing mode limits this delay period to approximately 2ms, where in normal mode it may vary up to 4ms.
- Precise ramp timing mode is only valid when using the EN pin to enable the device rather than PMBus enable.
- The devices may require up to a 4ms delay following the assertion of the enable signal (normal mode) or following the de-assertion of the enable signal.
- Factory setting for Power-Good delay is set to the same value as the soft-start ramp time.
- Nominal capacitance of logic pins is 5pF.
- This condition is tested on the Intersil 3-module evaluation board at  $+50^{\circ}C$  ambient temperature and 400LFM air flow.
- The load current is related to the thermal derating curves. The maximum allowed current is derated while the output voltage goes higher than 2.5V.

## Typical Performance Curves

Operating condition:  $T_A = +25^\circ\text{C}$ , No air flow,  $F_{SW} = 571\text{kHz}$ ,  $V_{DRV} = 5\text{V}$ ,  $C_{OUT} = 3000\mu\text{F}$ .

Typical values are used unless otherwise noted.

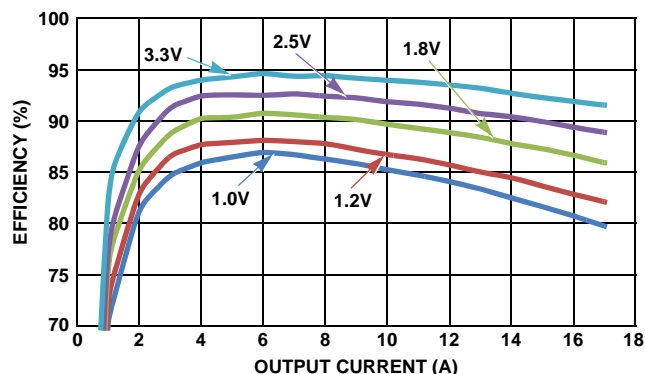


FIGURE 2. EFFICIENCY,  $V_{IN} = 5\text{V}$ , FOR VARIOUS OUTPUT VOLTAGES LISTED

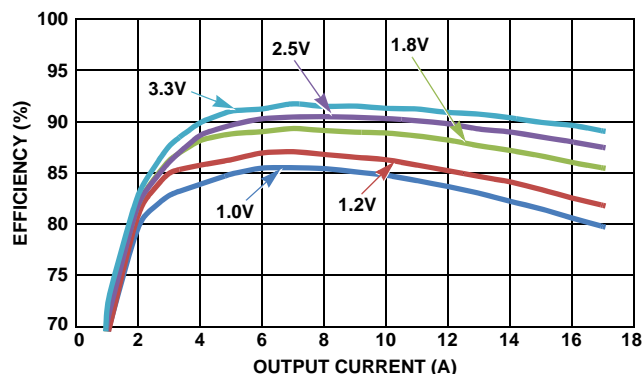


FIGURE 3. EFFICIENCY,  $V_{IN} = 9\text{V}$ , FOR VARIOUS OUTPUT VOLTAGES LISTED

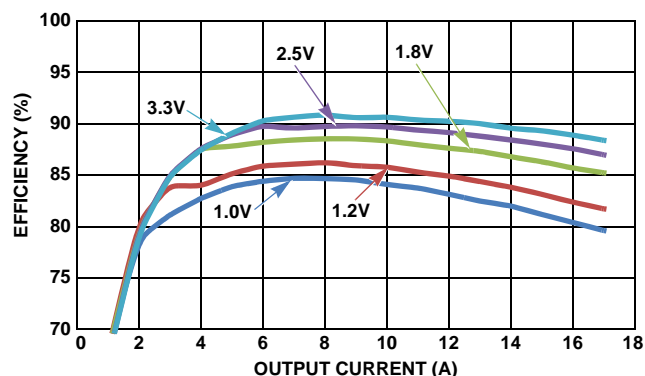


FIGURE 4. EFFICIENCY,  $V_{IN} = 12\text{V}$ , FOR VARIOUS OUTPUT VOLTAGES LISTED

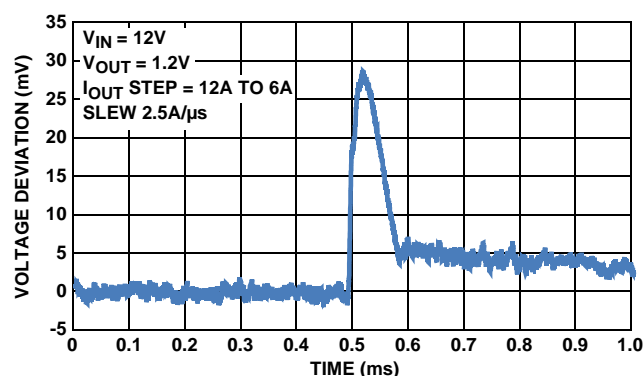


FIGURE 5. DYNAMIC RESPONSE, UNLOAD

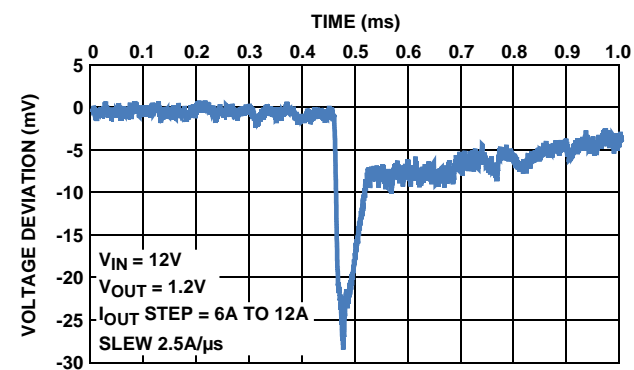


FIGURE 6. DYNAMIC RESPONSE, LOAD

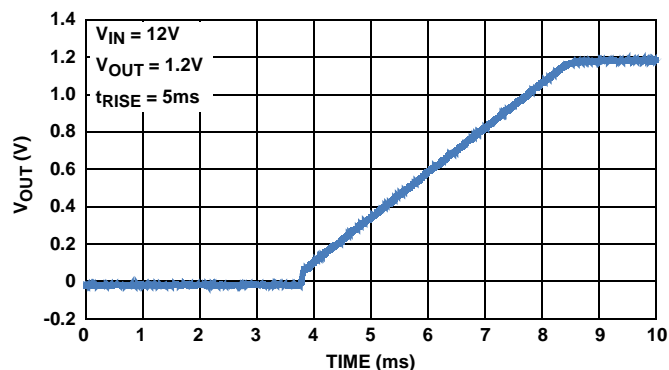


FIGURE 7. SOFT-START RAMP-UP



## Typical Performance Curves

Operating condition:  $T_A = +25^\circ\text{C}$ , No air flow,  $F_{SW} = 571\text{kHz}$ ,  $V_{DRV} = 5\text{V}$ ,  $C_{OUT} = 3000\mu\text{F}$ .

Typical values are used unless otherwise noted. (Continued)

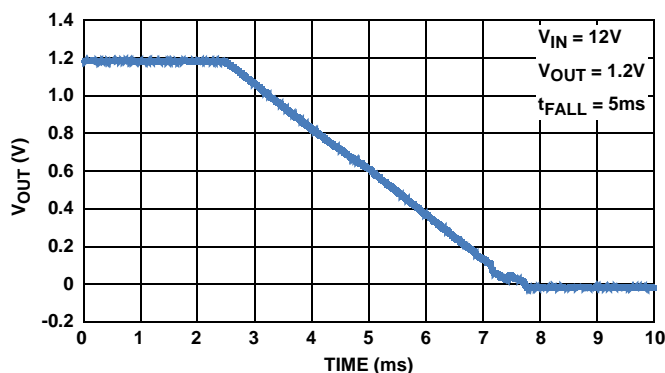


FIGURE 8. RAMP-DOWN

## Derating Curves

Operating conditions:  $T_A = +25^\circ\text{C}$ ,  $F_{SW} = 571\text{kHz}$ ,  $V_{DRV} = 5\text{V}$ ,  $C_{OUT} = 3000\mu\text{F}$ .

Typical values are used unless otherwise noted.

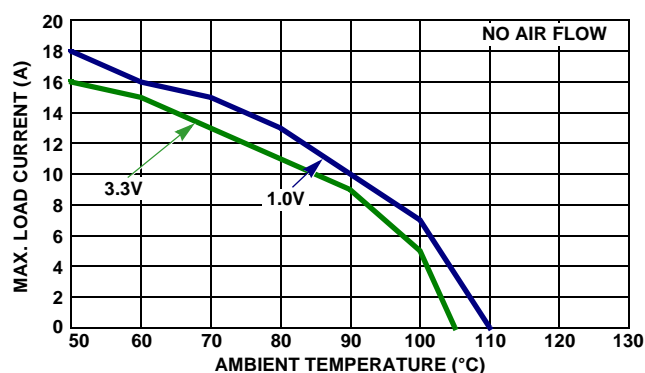


FIGURE 9. DERATING CURVE,  $5V_{IN}$ , FOR VARIOUS OUTPUT VOLTAGES LISTED

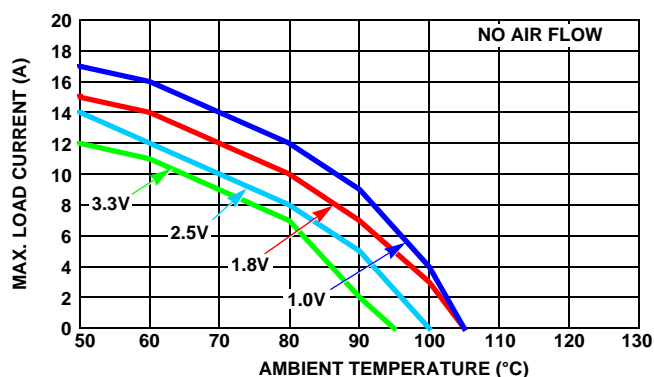


FIGURE 10. DERATING CURVE,  $12V_{IN}$ , FOR VARIOUS OUTPUT VOLTAGES LISTED

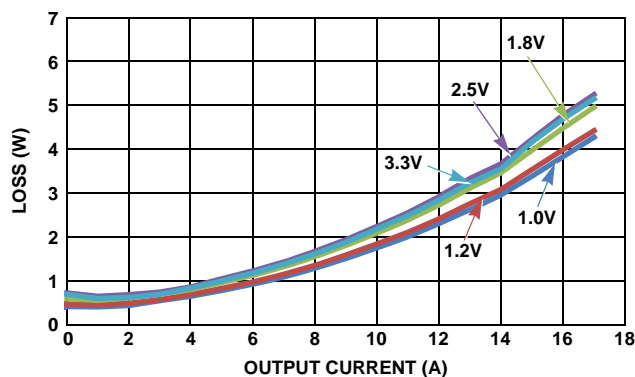


FIGURE 11. POWER LOSS CURVE,  $5V_{IN}$ , FOR VARIOUS OUTPUT VOLTAGES LISTED

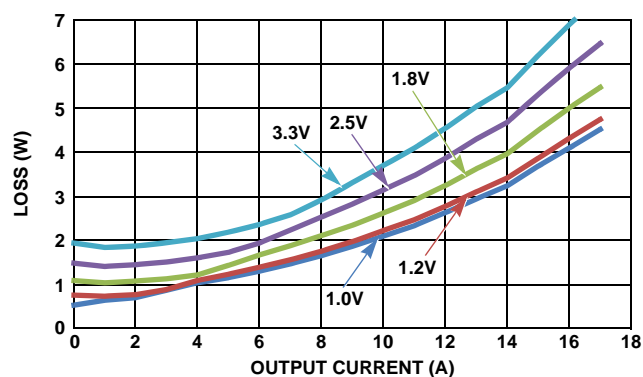


FIGURE 12. POWER LOSS CURVE,  $12V_{IN}$ , FOR VARIOUS OUTPUT VOLTAGES LISTED

## Functional Description

### I<sup>2</sup>C/SMBus Communications

The ZL9117M provides an I<sup>2</sup>C/SMBus digital interface that enables the user to configure all aspects of the module operation as well as monitor the input and output parameters. The ZL9117M can be used with any I<sup>2</sup>C host device. In addition, the module is compatible with SMBus version 2.0. Pull-up resistors are required on the I<sup>2</sup>C/SMBus as specified in the SMBus 2.0 specification. The ZL9117M accepts most standard PMBus commands. When controlling the device with PMBus commands, it is recommended that the enable pin is tied to SGND.

The SMBus device address and VOUT\_MAX are the only parameters that must be set by external pins. All other device parameters can be set via the I<sup>2</sup>C/SMBus. The device address is set using the SA pin. VOUT\_MAX is determined as 10% greater than the voltage set by the VSET pin. Standard 1% resistor values are used between the respective pin and SGND.

### Output Voltage Selection

The output voltage may be set to a voltage between 0.6V and 3.6V provided that the input voltage is higher than the desired output voltage by an amount sufficient to prevent the device from exceeding its maximum duty cycle specification.

The VSET pin is used to set the output voltage to levels as shown in Table 1. The R<sub>SET</sub> resistor is placed between the VSET pin and SGND.

TABLE 1. OUTPUT VOLTAGE RESISTOR SETTINGS

V <sub>OUT</sub> (V)	R <sub>SET</sub> (kΩ)
0.60	10
0.65	11
0.70	12.1
0.75	13.3
0.80	14.7
0.85	16.2
0.90	17.8
0.95	19.6
1.00	21.5
1.05	23.7
1.10	26.1
1.15	28.7
1.20	31.6
1.25	34.8
1.30	38.3
1.40	42.2
1.50	46.4
1.60	51.1
1.70	56.2

TABLE 1. OUTPUT VOLTAGE RESISTOR SETTINGS (Continued)

V <sub>OUT</sub> (V)	R <sub>SET</sub> (kΩ)
1.80	61.9
1.90	68.1
2.00	75
2.10	82.5
2.20	90.9
2.30	100
2.50	110
2.80	121
3.00	133
3.30	147

The output voltage may also be set to any value between 0.6V and 3.6V using a PMBus command over the I<sup>2</sup>C/SMBus interface. See Application Note [AN2033](#) for details.

The RSET resistor program places an upper limit in output voltage setting through PMBUS programming to 10% above the value set by the resistor.

### Soft-start Delay and Ramp Times

It may be necessary to set a delay from when an enable signal is received until the output voltage starts to ramp to its target value. In addition, the designer may wish to precisely set the time required for V<sub>OUT</sub> to ramp to its target value after the delay period has expired. These features may be used as part of an overall in-rush current management strategy or to precisely control how fast a load IC is turned on. The ZL9117M gives the system designer several options for precisely and independently controlling both the delay and ramp time periods.

The soft-start delay period begins when the EN pin is asserted and ends when the delay time expires.

The soft-start delay and ramp times are set to custom values via the I<sup>2</sup>C/SMBus interface. When the delay time is set to 0ms, the device begins its ramp-up after the internal circuitry has initialized (approximately 2ms). When the soft-start ramp period is set to 0ms, the output ramps up as quickly as the output load capacitance and loop settings allow. It is generally recommended to set the soft-start ramp to a value greater than 500μs to prevent inadvertent fault conditions due to excessive in-rush current.

### Power-Good

The ZL9117M provides a Power-Good (PG) signal that indicates the output voltage is within a specified tolerance of its target level and no fault condition exists. By default, the PG pin asserts if the output is within 10% of the target voltage. These limits and the polarity of the pin may be changed via the I<sup>2</sup>C/SMBus interface. See Application Note [AN2033](#) for details.

A PG delay period is defined as the time from when all conditions within the ZL9117M for asserting PG are met to when the PG pin is actually asserted. This feature is commonly used instead of

using an external reset controller to control external digital logic. By default, the ZL9117M PG delay is set equal to the soft-start ramp time setting. Therefore, if the soft-start ramp time is set to 10ms, the PG delay is set to 10ms. The PG delay may be set independently of the soft-start ramp using the I<sup>2</sup>C/SMBus as described in Application Note [AN2033](#).

## Switching Frequency and PLL

The ZL9117M incorporates an internal phase-locked loop (PLL) to clock the internal circuitry. The PLL can be driven by an external clock source connected to the SYNC pin. When using the internal oscillator, the SYNC pin can be configured as a clock source.

The internal switching frequency of the ZL9117M is 571kHz.

## Loop Compensation

The ZL9117M operates as a voltage-mode synchronous buck controller with a fixed frequency PWM scheme. The module is internally compensated via the I<sup>2</sup>C/SMBus interface.

The ZL9117M has an auto compensation feature that measures the characteristics of the power train and calculates the proper tap coefficients. By default, auto compensation is configured to execute one time after ramp with 50% auto compensation Gain with Power-Good asserted immediately after the first auto compensation cycle completes.

Please refer to Application Note [AN2033](#) for further details.

## Adaptive Diode Emulation

Adaptive diode emulation mode turns off the low-side FET gate drive at low load currents to prevent the inductor current from going negative, reducing the energy losses and increasing overall efficiency. Diode emulation is available to single-phase devices only.

Note: the overall bandwidth of the device may be reduced when in diode emulation mode. Disabling the diode emulation prior to applying significant load steps is recommended.

## Input Undervoltage Lockout

The input undervoltage lockout (UVLO) prevents the ZL9117M from operating when the input falls below a preset threshold, indicating the input supply is out of its specified range. The UVLO threshold ( $V_{UVLO}$ ) can be set between 2.85V and 16V using the I<sup>2</sup>C/SMBus interface.

Once an input undervoltage fault condition occurs, the device can respond in a number of ways, as follows:

1. Continue operating without interruption.
2. Continue operating for a given delay period, followed by shutdown if the fault still exists. The device remains in shutdown until instructed to restart.
3. Initiate an immediate shutdown until the fault is cleared. The user can select a specific number of retry attempts.

The default response from a UVLO fault is an immediate shutdown of the module. The controller continuously checks for the presence of the fault condition. If the fault condition is no longer present, the ZL9117M is re-enabled.

Please refer to Application Note [AN2033](#) for details on how to configure the UVLO threshold or to select specific UVLO fault response options via the I<sup>2</sup>C/SMBus interface.

## Output Overvoltage Protection

The ZL9117M offers an internal output overvoltage protection circuit that can be used to protect sensitive load circuitry from being subjected to a voltage higher than its prescribed limits. A hardware comparator is used to compare the actual output voltage (seen at the FB+ pin) to a threshold set to 15% higher than the target output voltage (the default setting). If the FB+ voltage exceeds this threshold, the PG pin de-asserts, and the controller can then respond in a number of ways, as follows:

1. Initiate an immediate shutdown until the fault is cleared. The user can select a specific number of retry attempts.
2. Turn off the high-side MOSFET and turn on the low-side MOSFET. The low-side MOSFET remains ON until the device attempts a restart.

The default response from an overvoltage fault is to immediately shut down. The controller continuously checks for the presence of the fault condition, and when the fault condition no longer exists, the device is re-enabled.

For continuous overvoltage protection when operating from an external clock, the only allowed response is an immediate shutdown.

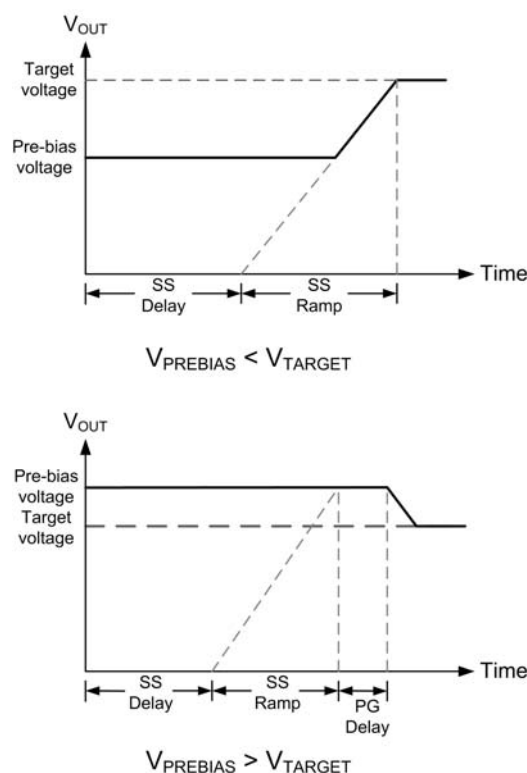
Please refer to Application Note [AN2033](#) for details on how to select specific overvoltage fault response options via I<sup>2</sup>C/SMBus.

## Output Pre-Bias Protection

An output pre-bias condition exists when an externally applied voltage is present on a power supply's output before the power supply's control IC is enabled. Certain applications require that the converter not be allowed to sink current during start-up if a pre-bias condition exists at the output. The ZL9117M provides pre-bias protection by sampling the output voltage prior to initiating an output ramp.

If a pre-bias voltage lower than the target voltage exists after the pre-configured delay period has expired, the target voltage is set to match the existing pre-bias voltage, and both drivers are enabled. The output voltage is then ramped to the final regulation value at the preconfigured ramp rate.

The actual time the output takes to ramp from the pre-bias voltage to the target voltage varies, depending on the pre-bias voltage, however, the total time elapsed from when the delay period expires and when the output reaches its target value will match the pre-configured ramp time. See Figure 13.



**FIGURE 13. OUTPUT RESPONSES TO PRE-BIAS VOLTAGES**

If a pre-bias voltage higher than the target voltage exists after the pre-configured delay period has expired, the target voltage is set to match the existing pre-bias voltage, and both drivers are enabled with a PWM duty cycle that would ideally create the pre-bias voltage.

Once the pre-configured soft-start ramp period has expired, the PG pin is asserted (assuming the pre-bias voltage is not higher than the overvoltage limit). The PWM then adjusts its duty cycle to match the original target voltage, and the output ramps down to the preconfigured output voltage.

If a pre-bias voltage higher than the overvoltage limit exists, the device does not initiate a turn-on sequence and declares an overvoltage fault condition to exist. In this case, the device responds based on the output overvoltage fault response method that has been selected. See “Output Overvoltage Protection” on page 11 for response options due to an overvoltage condition.

Note that pre-bias protection is not offered for current sharing groups that also have tracking enabled.  $V_{DD}$  must be tied to  $V_{IN}$  for proper prebias start-up in single module operation.

## Output Overcurrent Protection

The ZL9117M can protect the power supply from damage if the output is shorted to ground or if an overload condition is imposed on the output. The following overcurrent protection response options are available:

1. Initiate a shutdown and attempt to restart an infinite number of times with a preset delay period between attempts.
2. Initiate a shutdown and attempt to restart a preset number of times with a preset delay period between attempts.

3. Continue operating for a given delay period, followed by shutdown if the fault still exists.
4. Continue operating through the fault (this could result in permanent damage to the power supply).
5. Initiate an immediate shutdown.

The default response from an overcurrent fault is an immediate shutdown of the controller. The controller continuously checks for the presence of the fault condition, and if the fault condition no longer exists, the device is re-enabled.

Please refer to Application Note [AN2033](#) for details on how to select specific overcurrent fault response options via I<sup>2</sup>C/SMBus.

## Thermal Overload Protection

The ZL9117M includes a thermal sensor that continuously measures the internal temperature of the module and shuts down the controller when the temperature exceeds the preset limit. The default temperature limit is set to +125 °C in the factory, but the user may set the limit to a different value if desired. See Application Note [AN2033](#) for details. Note that setting a higher thermal limit via the I<sup>2</sup>C/SMBus interface may result in permanent damage to the controller. Once the module has been disabled due to an internal temperature fault, the user may select one of several fault response options as follows:

1. Initiate a shutdown and attempt to restart an infinite number of times with a preset delay period between attempts.
2. Initiate a shutdown and attempt to restart a preset number of times with a preset delay period between attempts.
3. Continue operating for a given delay period, followed by shutdown if the fault still exists.
4. Continue operating through the fault (this could result in permanent damage to the power supply).
5. Initiate an immediate shutdown.

If the user has configured the module to restart, the controller waits the preset delay period (if configured to do so) and then checks the module temperature. If the temperature has dropped below a threshold that is approximately +15 °C lower than the selected temperature fault limit, the controller attempts to re-start. If the temperature still exceeds the fault limit, the controller waits the preset delay period and retries again.

The default response from a temperature fault is an immediate shutdown of the module. The controller continuously checks for the fault condition, and once the fault has cleared, the ZL9117M is re-enabled.

Please refer to Application Note [AN2033](#) for details on how to select specific temperature fault response options via I<sup>2</sup>C/SMBus.

## I<sup>2</sup>C/SMBus Module Address Selection

Each module must have its own unique serial address to distinguish between other devices on the bus. The module address is set by connecting a resistor between the SA pin and SGND. Table 2 lists the available module addresses.

**TABLE 2. SMBus ADDRESS RESISTOR SELECTION**

R <sub>SA</sub> (kΩ)	SMBus ADDRESS
10	0x19
11	0x1A
12.1	0x1B
13.3	0x1C
14.7	0x1D
16.2	0x1E
17.8	0x1F
19.6	0x20
21.5	0x21
23.7	0x22
26.1, or connect to SGND	0x23
28.7, or Open	0x24
31.6, or connect to V25 or VR	0x25
34.8	0x26
38.3	0x27
42.2	0x28
46.4	0x29
51.1	0x2A
56.2	0x2B
61.9	0x2C
68.1	0x2D
75	0x2E
82.5	0x2F
90.9	0x30
100	0x31

## Digital-DC Bus

The Digital-DC Communications (DDC) bus is used to communicate between Zilker Labs Digital-DC modules and devices. This dedicated bus provides the communication channel between devices for features such as sequencing, fault spreading, and current sharing. The DDC pin on all Digital-DC devices in an application should be connected together. A pull-up resistor is required on the DDC bus in order to guarantee the rise time as shown in Equation 1:

$$\text{Rise Time} = R_{PU} \cdot C_{LOAD} \approx 1\mu\text{s} \quad (\text{EQ. 1})$$

where  $R_{PU}$  is the DDC bus pull-up resistance and  $C_{LOAD}$  is the bus loading. The pull-up resistor may be tied to an external 3.3V or 5V supply as long as this voltage is present prior to or during device power-up. As rules of thumb, each device connected to the DDC bus presents approximately 10pF of capacitive loading, and each inch of FR4 PCB trace introduces approximately 2pF. The ideal design uses a central pull-up resistor that is well-matched to the total load capacitance. The minimum pull-up resistance

should be limited to a value that enables any device to assert the bus to a voltage that ensures a logic 0 (typically 0.8V at the device monitoring point), given the pull-up voltage and the pull-down current capability of the ZL9117M (nominally 4mA).

## Phase Spreading

When multiple point-of-load converters share a common DC input supply, it is desirable to adjust the clock phase offset of each device such that not all devices start to switch simultaneously. Setting each converter to start its switching cycle at a different point in time, can dramatically reduce input capacitance requirements and efficiency losses. Since the peak current drawn from the input supply is effectively spread out over a period of time, the peak current drawn at any given moment is reduced, and the power losses proportional to the  $I_{RMS}^2$  are reduced dramatically.

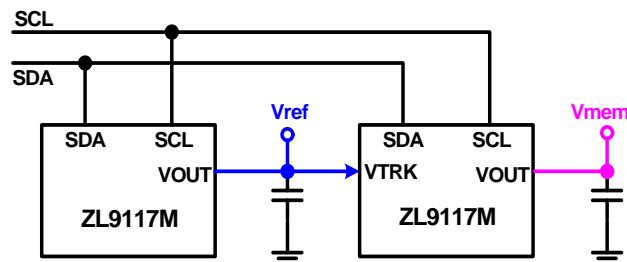
To enable phase spreading, all converters must be synchronized to the same switching clock. The phase offset of each device may also be set to any value between 0° and 360° in 22.5° increments via the I<sup>2</sup>C/SMBus interface. Refer to Application Note [AN2033](#) for further details.

## Output Voltage Tracking

High performance systems place stringent demands on the order in which the power supply voltages turn on. This is particularly true when powering FPGAs, ASICs, and other advanced processor devices that require multiple supply voltages to power a single die. In most cases, the I/O interface operates at a higher voltage than the core and therefore the core supply voltage must not exceed the I/O supply voltage according to the manufacturers' specifications. Voltage tracking protects these sensitive ICs by limiting the differential voltage among multiple power supplies during the power-up and power-down sequence.

The ZL9117M integrates a lossless tracking scheme that allows its output to track a voltage that is applied to the VTRK pin with no additional components required. The VTRK pin is an analog input that, when tracking mode is enabled, and configures the voltage applied to the VTRK pin to act as a reference for the member device's output regulation.

Voltage tracking can be configured by PMBus only. An example is shown in Figure 14.



**FIGURE 14. PMBUS TRACKING CONFIGURATION**

The ZL9117M offers two modes of tracking: coincident and ratiometric. Figures 15 and Figure 16 illustrate the output voltage waveform for the two tracking modes.

**Coincident:** This mode configures the ZL9117M to ramp its output voltage at the same rate as the voltage applied to the VTRK pin. Two options are available for this mode;

a. Track at 100% VOUT limited. Member rail tracks the reference rail and stops when the member reaches its target voltage, Figure 15A.

b. Track at 100% VTRK limited. Member rail tracks the reference at the instantaneous voltage value applied to the VTRK pin, Figure 15B.

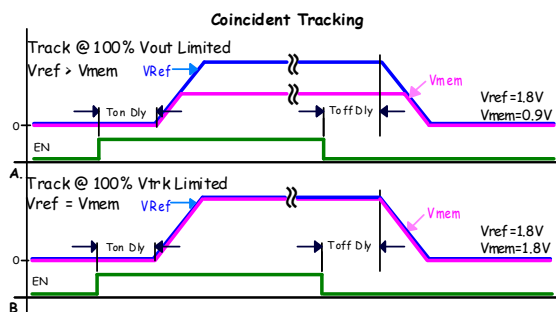


FIGURE 15. COINCIDENT TRACKING

**Ratiometric:** This mode configures the ZL9117M to ramp its output voltage as a percentage of the voltage applied to the VTRK pin. The default setting is 50%, but an external resistor or PMBus command may be used to configure a different tracking ratio.

a. Track at 50% VOUT limited. Member rail tracks the reference rail and stops when the member reaches 50% of the target voltage, Figure 16A.

b. Track at 50% VTRK limited. Member rail tracks the reference at the instantaneous voltage value applied to the VTRK pin until the member rail reaches 50% of the reference rail voltage, or if the member is configured to less than 50% of the reference the member will achieve its configured target, Figure 16B. Refer to Application Note [AN2033](#) for further details.

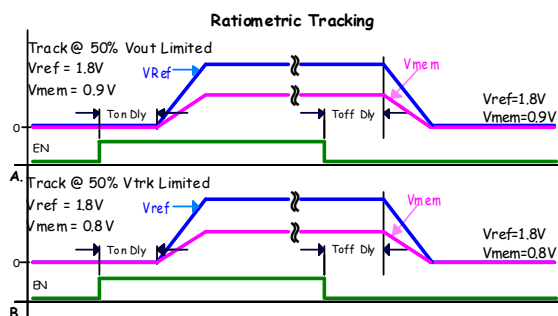


FIGURE 16. RATIOMETRIC TRACKING

## Output Sequencing

A group of Digital-DC modules or devices may be configured to power-up in a predetermined sequence. This feature is especially useful when powering advanced processors, FPGAs and ASICs that require one supply to reach its operating voltage; prior to another supply reaching its operating voltage in order to avoid

latch-up. Multi-device sequencing can be achieved by configuring each device through the I<sup>2</sup>C/SMBus interface.

Multiple device sequencing is configured by issuing PMBus commands to assign the preceding device in the sequencing chain as well as the device that follows in the sequencing chain.

The Enable pins of all devices in a sequencing group must be tied together and driven high to initiate a sequenced turn-on of the group. Enable must be driven low to initiate a sequenced turnoff of the group.

Refer to Application Note [AN2033](#) for details on sequencing via the I<sup>2</sup>C/SMBus interface.

## Fault Spreading

Digital DC modules and devices can be configured to broadcast a fault event over the DDC bus to the other devices in the group. When a non-destructive fault occurs and the device is configured to shut down on a fault, the device shuts down and broadcasts the fault event over the DDC bus. The other devices on the DDC bus shut down simultaneously, if configured to do so, and attempt to re-start in their prescribed order, if configured to do so.

## Active Current Sharing

Paralleling multiple ZL9117M modules can be used to increase the output current capability of a single power rail. By connecting the DDC pins of each module together and configuring the modules as a current sharing rail, the units share the current equally within a few percent. Figure 17 illustrates a typical connection for two modules.

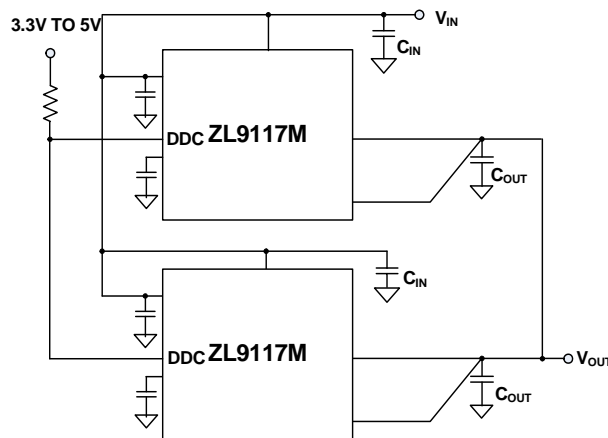


FIGURE 17. CURRENT SHARING GROUP

The ZL9117M uses a low-bandwidth, first-order digital current sharing technique to balance the unequal module output loading by aligning the load lines of member modules to a reference module.

Droop resistance is used to add artificial resistance in the output voltage path to control the slope of the load line curve, calibrating out the physical parasitic mismatches due to power train components and PCB layout.

Upon system start-up, the module with the lowest member position as selected in ISHARE\_CONFIG is defined as the



reference module. The remaining modules are members. The reference module broadcasts its current over the DDC bus. The members use the reference current information to trim their voltages ( $V_{MEMBER}$ ) to balance the current loading of each module in the system.

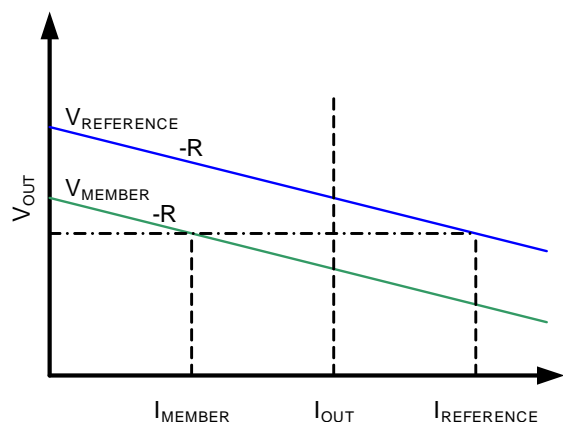


FIGURE 18. ACTIVE CURRENT SHARING

Figure 18 shows that, for load lines with identical slopes, the member voltage is increased towards the reference voltage which closes the gap between the inductor currents.

The relation between reference and member current and voltage is given by Equation 2:

$$V_{MEMBER} = V_{OUT} + R \times (I_{REFERENCE} - I_{MEMBER}) \quad (EQ. 2)$$

where  $R$  is the value of the droop resistance.

The `ISHARE_CONFIG` command is used to configure the module for active current sharing. The default setting is a stand-alone non-current sharing module. A current sharing rail can be part of a system sequencing group.

For fault configuration, the current share rail is configured in a quasi-redundant mode. In this mode, when a member module fails, the remaining members continue to operate and attempt to maintain regulation. Of the remaining modules, the module with the lowest member position becomes the reference. If fault spreading is enabled, the current share rail failure is not broadcast until the entire current share rail fails.

The phase offset of (multi-phase) current sharing modules is automatically set to a value between  $0^\circ$  and  $337.5^\circ$  in  $22.5^\circ$  increments as in Equation 3:

$$\text{Phase Offset} = \text{SMBus Address}[4:0] - \text{Current Share Position} \times 22.5^\circ \quad (EQ. 3)$$

Please refer to Application Note [AN2034](#) for additional details on current sharing.

## Phase Adding/Dropping

The ZL9117M allows multiple power converters to be connected in parallel to supply higher load currents than can be addressed using a single-phase design. In doing so, the power converter is optimized at a load current range that requires all phases to be operational. During periods of light loading, it may be beneficial

to disable one or more phases to eliminate the current drain and switching losses associated with those phases, resulting in higher efficiency.

The ZL9117M offers the ability to add and drop phases using a PMBus command in response to an observed load current change. All phases in a current share rail are considered active prior to the current sharing rail ramp to power-good.

Any member of the current sharing rail can be dropped. If the reference module is dropped, the remaining active module with the lowest member position becomes the new reference.

Additionally, any change to the number of members of a current sharing rail will precipitate autonomous phase distribution within the rail where all active phases realign their phase position based on their order within the number of active members.

If the members of a current sharing rail are forced to shut down due to an observed fault, all members of the rail attempt to re-start simultaneously after the fault has cleared.

## Monitoring via I<sup>2</sup>C/SMBus

A system controller can monitor a wide variety of different ZL9117M system parameters through the I<sup>2</sup>C/SMBus interface.

The module can monitor for any number of power conversion parameters including but not limited to the following:

- Input voltage/Output voltage
- Output current
- Internal temperature
- Switching frequency
- Duty cycle

Please refer to Application Note [AN2033](#) for details on how to monitor specific parameters via the I<sup>2</sup>C/SMBus interface.

## Snapshot Parameter Capture

The ZL9117M offers a special feature that enables the user to capture parametric data during normal operation or following a fault. The SnapShot functionality is enabled by setting bit 1 of `MISC_CONFIG` to 1.

See [AN2033](#) for details on using SnapShot in addition to the parameters supported. The SnapShot feature enables the user to read parameters via a block read transfer through the SMBus. This can be done during normal operation, although it should be noted that reading the 22 bytes occupies the SMBus for some time.

The `SNAPSHOT_CONTROL` command enables the user to store the SnapShot parameters to Flash memory in response to a pending fault, as well as to read the stored data from Flash memory after a fault has occurred. Table 3 describes the usage of this command. Automatic writes to Flash memory following a fault are triggered when any fault threshold level is exceeded, provided that the specific fault's response is to shut down (writing to Flash memory is not allowed if the device is configured to re-try following the specific fault condition). It should also be noted that the module's  $V_{DD}$  voltage must be maintained during the time when the controller is writing the data to Flash memory; a process that requires between  $700\mu s$  to  $1400\mu s$ , depending on

whether the data is set up for a block write. Undesirable results may be observed if the device's  $V_{DD}$  supply drops below 3.0V during this process.

**TABLE 3. SNAPSHOT\_CONTROL COMMAND**

DATA VALUE	DESCRIPTION
1	Copies current SNAPSHOT values from Flash memory to RAM for immediate access using SNAPSHOT command.
2	Writes current SNAPSHOT values to Flash memory. Only available when device is disabled.

If the module experiences a fault and power is lost, the user can extract the last SnapShot parameters stored during the fault by writing a 1 to SNAPSHOT\_CONTROL (transfers data from Flash memory to RAM) and then issuing a SNAPSHOT command (reads data from RAM via SMBus).

## Non-Volatile Memory and Device Security Features

The ZL9117M has internal non-volatile memory where user configurations are stored. Integrated security measures ensure that the user can only restore the module to a level that has been made available to them.

During the initialization process, the ZL9117M checks for stored values contained in its internal non-volatile memory. The ZL9117M offers two internal memory storage units that are accessible by the user as follows:

1. **Default Store:** The ZL9117M has a default configuration that is stored in the default store in the controller. The module can be restored to its default settings by issuing a **RESTORE\_DEFAULT\_ALL** command over the SMBus.
2. **User Store:** The user can modify certain power supply settings as described in this data sheet. The user stores their configuration in the user store.

Please refer to Application Note [AN2033](#) for details on how to set specific security measures via the I<sup>2</sup>C/SMBus interface.

## OUTPUT CAPACITOR SELECTION

Several trade-offs must also be considered when selecting an output capacitor. Low ESR values are needed to have a small output deviation during transient load steps ( $V_{osag}$ ) and low output voltage ripple ( $V_{orip}$ ). However, capacitors with low ESR, such as semi-stable (X5R and X7R) dielectric ceramic capacitors, also have relatively low capacitance values. Many designs can use a combination of high capacitance devices and low ESR devices in parallel.

For high ripple currents, a low capacitance value can cause a significant amount of output voltage ripple. Likewise, in high transient load steps, a relatively large amount of capacitance is needed to minimize the output voltage deviation while the inductor current ramps up or down to the new steady state output current value.

As a starting point, apportion one-half of the output ripple voltage to the capacitor ESR and the other half to capacitance, as shown in Equations 4 and 5:

$$C_{OUT} = \frac{I_{opp}}{8 \times f_{SW} \times \frac{V_{orip}}{2}} \quad (EQ. 4)$$

$$ESR = \frac{V_{orip}}{2 \times I_{opp}} \quad (EQ. 5)$$

Use these values to make an initial capacitor selection, using a single capacitor or several capacitors in parallel.

After a capacitor has been selected, the resulting output voltage ripple can be calculated using Equation 6:

$$V_{orip} = I_{opp} \times ESR + \frac{I_{opp}}{8 \times f_{SW} \times C_{out}} \quad (EQ. 6)$$

Because each part of this equation was made to be less than or equal to half of the allowed output ripple voltage, the  $V_{orip}$  should be less than the desired maximum output ripple.

Usually, at higher output voltages, inductor ripple current is very high so it is recommend to use a combination of several ceramic capacitor with low ESR bulk capacitors to ensure low output ripple voltage and loop stability. Inadequate amount of capacitance at the output can cause instability to the control loop.

## INPUT CAPACITOR

It is highly recommended that dedicated input capacitors be used in any point-of-load design, even when the supply is powered from a heavily filtered 5V or 12V "bulk" supply from an off-line power supply. This is because of the high RMS ripple current that is drawn by the buck converter topology. This ripple ( $I_{CINrms}$ ) can be determined from Equation 7:

$$I_{CINrms} = I_{OUT} \times \sqrt{D \times (1 - D)} \quad (EQ. 7)$$

Without capacitive filtering near the power supply circuit, this current would flow through the supply bus and return planes, coupling noise into other system circuitry. The input capacitors should be rated at 1.2X the ripple current calculated above to avoid overheating of the capacitors due to the high ripple current, which can cause premature failure. Ceramic capacitors with X7R or X5R dielectric with low ESR and 1.1X the maximum expected input voltage are recommended.

## Layout Guide

To achieve stable operation, low losses, and good thermal performance some layout considerations are necessary.

- Establish a separate ground plane for SGND (pin 9) and PGND (pin 10 and pin 16) and connect them at a single point as shown in the Figure 19. CV25, CVR, RSA, and RVSET are placed on the bottom layer and are connected to a single SGND plane that is connected to the PGND at a single point. This will help to block the high frequency noise from entering to the controller via SGND.
- Place a high frequency ceramic capacitor between (1) VIN and PGND (pin 16), (2) VOUT and PGND (pin 16) and (3) bypass capacitors between VDRV, VDD, V25, VR and the ground plane, as close to the module as possible to minimize high frequency noise. High frequency ceramic capacitors close to the module



- Use large copper areas for power path (VIN, PGND, VOUT) to minimize conduction loss and thermal stress. Also, use multiple vias to connect the power planes in different layers.
- Connect remote sensed traces to the regulation point to achieve a tight output voltage regulation, and keep them in parallel. Route a trace from FB- to a location near the load ground, and a trace from FB+ to the point-of-load where the tight output voltage is desired.
- Avoid routing any sensitive signal traces, such as the VOUT, FB+, FB- sensing point near the PHASE pin.



Experimental power loss curves along with  $\theta_{JA}$  from thermal modeling analysis can be used to evaluate the thermal consideration for the module. The derating curves are derived from the maximum power allowed while maintaining the temperature below the maximum junction temperature of +125 °C. In actual application, other heat sources and design margin should be considered.

The structure of the ZL9117M belongs to the Quad Flat-pack No-lead package (QFN). This kind of package has advantages, such as good thermal and electrical conductivity, low weight and small size. The QFN package is applicable for surface mounting technology and is being more readily used in the industry. The ZL9117M contains several types of devices, including resistors, capacitors, inductors and control ICs. The ZL9117M is a copper lead-frame based package with exposed copper thermal pads, which have good electrical and thermal conductivity. The copper lead frame and multi component assembly is overmolded with polymer mold compound to protect these devices.

typical reflow profile parameters. These guidelines are general design rules. Users could modify parameters according to their application.

The bottom of ZL9117M is a lead-frame footprint, which is attached to the PCB by surface mounting process. The PCB layout pattern is shown on the second page of the Package Outline Drawing L21.15x15 on Page 21. The PCB layout pattern is essentially 1:1 with the QFN exposed pad and I/O termination dimensions, except for the PCB lands being a slightly extended distance of 0.2mm (0.4mm max) longer than the QFN terminations, which allows for solder filleting around the periphery of the package. This ensures a more complete and inspectable solder joint. The thermal lands on the PCB layout should match 1:1 with the package exposed die pads.

A grid of 1.0mm to 1.2mm pitch thermal vias, which drops down and connects to buried copper plane(s), should be placed under the thermal land. The via should be about 0.3mm to 0.33mm in diameter with the barrel plated to about 1.0 ounce copper. Although adding more vias (by decreasing via pitch) will improve the thermal performance, diminishing returns will be seen as more and more vias are added. Simply use as many vias as practical for the thermal land size and your board design rules allow.

Reflowed solder joints on the perimeter I/O lands should have about a 50µm to 75µm (2mil to 3mil) standoff height. The solder paste stencil design is the first step in developing optimized, reliable solder joins. Stencil aperture size to land size ratio should typically be 1:1. The aperture width may be reduced slightly to help prevent solder bridging between adjacent I/O lands. To reduce solder paste volume on the larger thermal lands, it is recommended that an array of smaller apertures be used instead of one large aperture. It is recommended that the stencil printing area cover 50% to 80% of the PCB layout pattern. A typical solder stencil pattern is shown on the second page of the Package Outline Drawing L21.15x15 on Page 21. The gap width between pad to pad is 0.6mm. The user should consider the symmetry of the whole stencil pattern when designing its pads. A laser cut, stainless steel stencil with electropolished trapezoidal walls is recommended. Electropolishing “smooths” the aperture walls resulting in reduced surface friction and better paste release which reduces voids. Using a Trapezoidal Section Aperture (TSA) also promotes paste release and forms a “brick like” paste deposit that assists in firm component placement. A 0.1mm to 0.15mm stencil thickness is recommended for this large pitch (1.3mm) QFN.

Due to the low mount height of the QFN, "No Clean" Type 3 solder paste per ANSI/J-STD-005 is recommended. Nitrogen purge is also recommended during reflow. A system board reflow profile depends on the thermal mass of the entire populated board, so it is not practical to define a specific soldering profile just for the QFN. The profile given in Figure 20 is provided as a guideline, to be customized for varying manufacturing practices and applications.

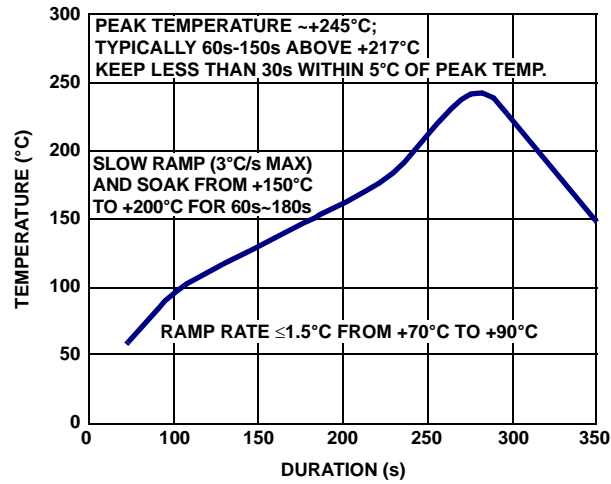


FIGURE 20. TYPICAL REFLOW PROFILE

## Revision History

The revision history provided is for informational purposes only and is believed to be accurate, but not warranted. Please go to web to make sure you have the latest revision.

DATE	REVISION	CHANGE
May 10, 2013	FN7914.3	Page 3: Added ZL9117MAIRZ to ordering information table. Page 6 - Electrical Spec Table changed in Input and Supply Characteristics section Driver Supply current, IVDRV - Conditions, Typ and Unit From: Not Switching, 190, uA To: VDRV = 6V, VOUT = 1.0V, FSW = 571kHz, No Load, 25, mA
December 4, 2012	FN7914.2	Changed CIN and COUT values in Figure 1 on Page 1. Removed Notes from Figure 1 on Page 1. Moved to pin description table (Page 2) and typical application (Page 5). Line and load regulation on output characteristic (Electrical Specifications) were combined to provide output voltage accuracy specification. Added "ZL9117M Internal Block Diagram" on page 4. Added "Typical Application - Single Module" on page 5. Added "Output Voltage Selection" on page 10. Added "Output Voltage Tracking" on page 13. Added "Output Capacitor Selection" and "Input Capacitor" on page 16. Updated first bullet in "Layout Guide" on page 16. Updated Figure 19 on Page 17.
October 12, 2011	FN7914.1	On Page 1: Changed "... required for a complete DC/DC power solution." in first paragraph to "... required for a highly integrated DC/DC power solution." Added "This power module has built-in auto-compensation algorithms, which eliminates the need for manual compensation design work." to first paragraph. Changed "The ZL9117M features internal compensation.." to "The ZL9117M features auto-compensation.." Added "Auto Compensating PID Filter" to "Features".
August 30, 2011	FN7914.0	Initial Release

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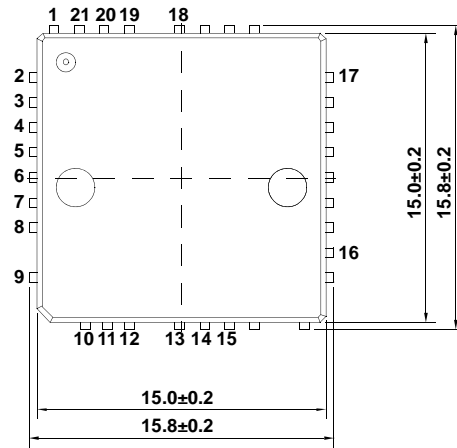
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# Package Outline Drawing

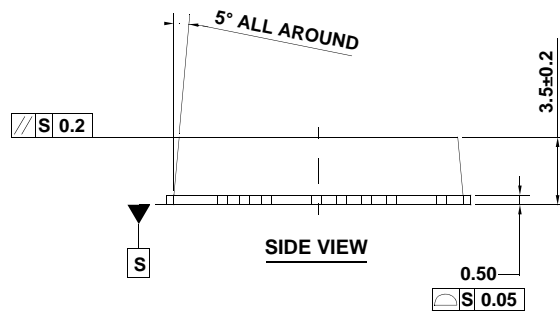
## L21.15x15

21 LEAD QUAD FLAT NO-LEAD PLASTIC PACKAGE (PUNCH QFN)

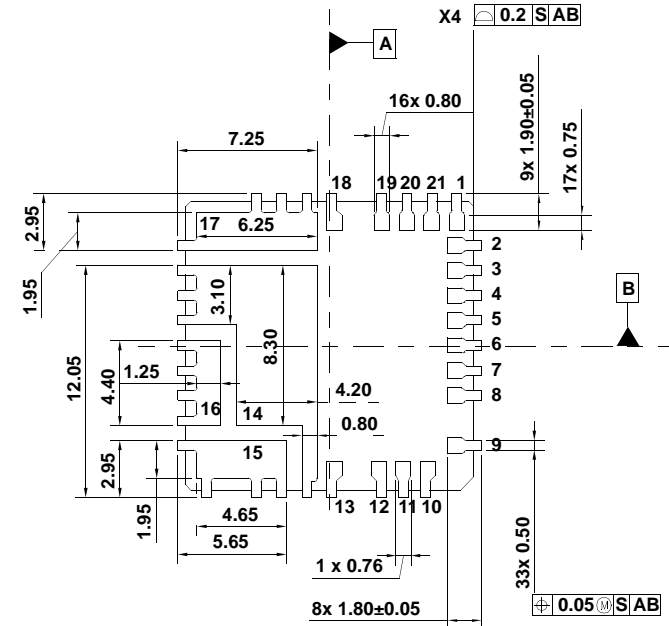
Rev 2, 8/11



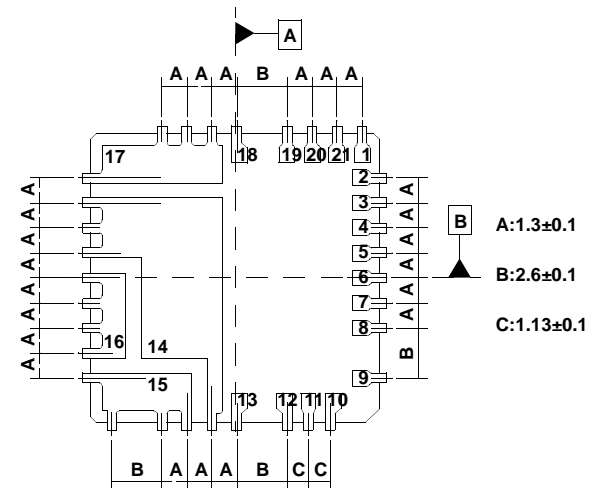
TOP VIEW



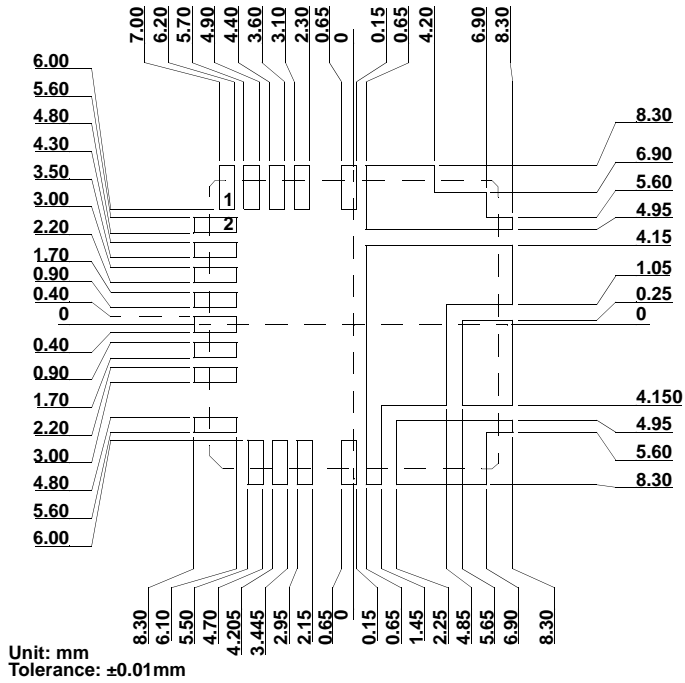
SIDE VIEW



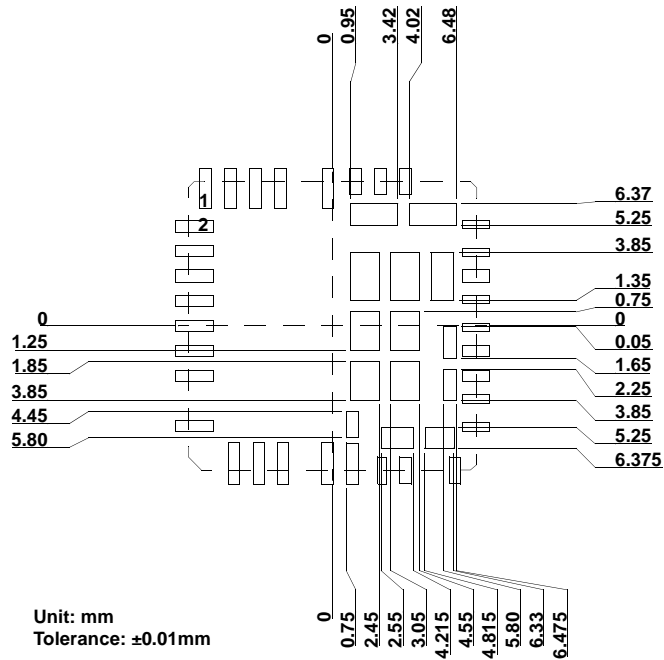
BOTTOM VIEW



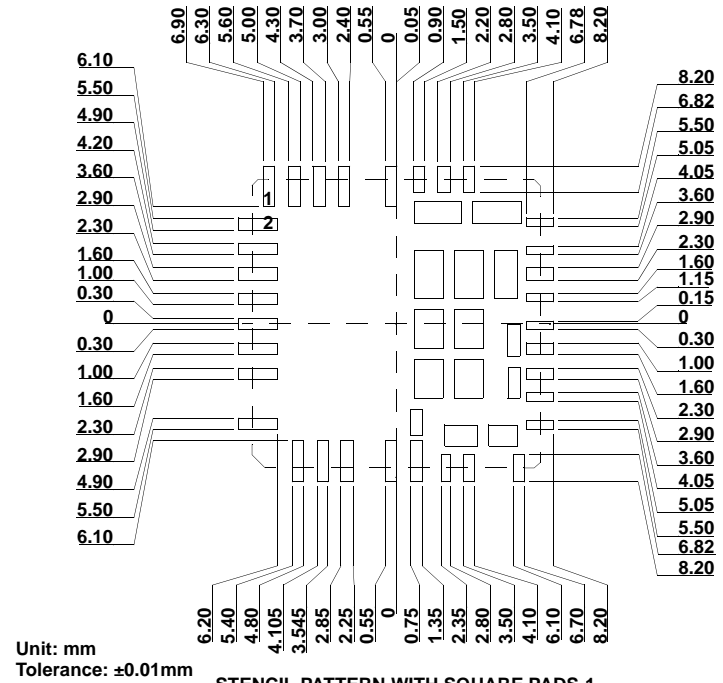
ZL9117M



TYPICAL RECOMMENDED LAND PATTERN



STENCIL PATTERN WITH SQUARE PADS-2



STENCIL PATTERN WITH SQUARE PADS-1

## NOTES:

1. Dimensions are in millimeters.
2. Unless otherwise specified, tolerance : Decimal  $\pm 0.2$ ;  
Body Tolerance  $\pm 0.2\text{mm}$
3. The configuration of the pin #1 identifier is optional, but must be located within the zone indicated. The pin #1 identifier may be either a mold or mark feature.