



T-77-06-10

Ultralow Drift Op Amp

AD707

FEATURES

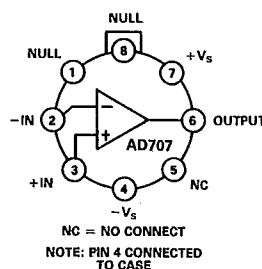
Very High DC Precision
 15 μV max Offset Voltage
 0.1 $\mu\text{V}/^\circ\text{C}$ max Offset Voltage Drift
 0.35 μV p-p max Voltage Noise (0.1 Hz to 10 Hz)
 8 $\text{V}/\mu\text{V}$ min Open-Loop Gain
 130 dB min CMRR
 120 dB min PSRR
 1 nA max Input Bias Current

AC Performance

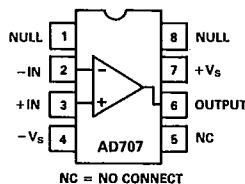
0.3 $\text{V}/\mu\text{s}$ Slew Rate
 0.9 MHz Closed-Loop Bandwidth
 Dual Version: AD708
 Available in Tape and Reel in Accordance with
 EIA-481A Standard

CONNECTION DIAGRAMS

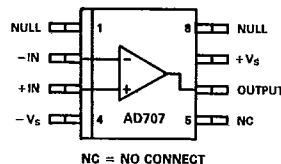
TO-99 (H)
Package



Plastic (N)
and Cerdip (Q)
Packages



SOIC (R) Package



PRODUCT DESCRIPTION

The AD707 is a low cost, high precision op amp with state-of-the-art performance that makes it ideal for a wide range of precision applications. The offset voltage spec of less than 15 μV is the best available in a bipolar op amp, and maximum input offset current is 1.0 nA. The top grade is the first bipolar monolithic op amp to offer a maximum offset voltage drift of 0.1 $\mu\text{V}/^\circ\text{C}$, and offset current drift and input bias current drift are both specified at 25 $\text{pA}/^\circ\text{C}$ maximum.

The AD707's open-loop gain is 8 $\text{V}/\mu\text{V}$ minimum over the full $\pm 10 \text{ V}$ output range when driving a 1 $\text{k}\Omega$ load. Maximum input voltage noise is 350 nV p-p (0.1 Hz to 10 Hz). CMRR and PSRR are 130 dB and 120 dB minimum, respectively.

The AD707 is available in versions specified over commercial, industrial and military temperature ranges. It is offered in 8-pin plastic mini-DIP, small outline (SOIC), hermetic cerdip and hermetic TO-99 metal can packages. Chips, MIL-STD-883B, Rev. C, and tape & reel parts are also available.

APPLICATION HIGHLIGHTS

1. The AD707's 13 $\text{V}/\mu\text{V}$ typical open-loop gain and 140 dB typical common-mode rejection ratio make it ideal for precision instrumentation applications.
2. The precision of the AD707 makes tighter error budgets possible at a lower cost.
3. The low offset voltage drift and low noise of the AD707 allow the designer to amplify very small signals without sacrificing overall system performance.
4. The AD707 can be used where chopper amplifiers are required, but without the inherent noise and application problems.
5. The AD707 is an improved pin-for-pin replacement for the LT1001.

AD707—SPECIFICATIONS (@ +25°C and ±15 V dc, unless otherwise noted)**T-79-06-10**

	Conditions	AD707J/A		AD707K/B/S		AD707C/T		Units	
		Min	Max	Min	Typ	Max	Min	Typ	Max
INPUT OFFSET VOLTAGE	Initial	30	90	10	25	5	15	μV	
	vs. Temperature	0.3	1.0	0.1	0.3	0.03	0.1	μV/°C	
	T_{min} to T_{max}	50	100	15	45	7/8/8	25	μV	
	Long-Term Stability	0.3		0.3		0.2		μV/month	
	Adjustment Range	$R_2 = 20\text{ k}\Omega$ (Figure 19)	±4		±4		±4		mV
INPUT BIAS CURRENT	T_{min} to T_{max}	1.0	2.5	0.5	1.5	0.5	1.0	nA	
		2.0	4.0	1.5	3.0	1.0	2.0	nA	
	Average Drift	15	40	15	25/25/35	10	25	pA/°C	
OFFSET CURRENT	$V_{CM} = 0\text{ V}$	0.5	2.0	0.3	1.5	0.1	1.0	nA	
	T_{min} to T_{max}	2.0	4.0	1.0	2.0	0.2	1.5	nA	
	Average Drift	2	40	1	25/25/35	1	25	pA/°C	
INPUT VOLTAGE NOISE	0.1 to 10 Hz	0.23	0.6	0.23	0.6	0.23	0.35	μV p-p	
	$f = 10\text{ Hz}$	10.3	15	10.3	14	10.3	13	nV/√Hz	
	$f = 100\text{ Hz}$	10.0	13.0	10.0	12	10.0	11.0	nV/√Hz	
	$f = 1\text{ kHz}$	9.6	11.0	9.6	11.0	9.6	11.0	nV/√Hz	
INPUT CURRENT NOISE	0.1 Hz to 10 Hz	14	35	14	30	14	30	pA p-p	
	$f = 10\text{ Hz}$	0.32	0.9	0.32	0.8	0.32	0.8	pA/√Hz	
	$f = 100\text{ Hz}$	0.14	0.27	0.14	0.23	0.14	0.23	pA/√Hz	
	$f = 1\text{ kHz}$	0.12	0.18	0.12	0.17	0.12	0.17	pA/√Hz	
COMMON-MODE REJECTION RATIO	$V_{CM} = \pm 13\text{ V}$	120	140	130	140	130	140	dB	
	T_{min} to T_{max}	120	140	130	140	130	140	dB	
OPEN-LOOP GAIN	$V_O = \pm 10\text{ V}$							V/μV	
	$R_{LOAD} \geq 2\text{ k}\Omega$	3	13	5	13	8	13	V/μV	
	T_{min} to T_{max}	3	13	5	13	8	13	V/μV	
	$R_{LOAD} \geq 1\text{ k}\Omega$	3	13	5	13	8	13	V/μV	
POWER SUPPLY REJECTION RATIO	$V_S = \pm 3\text{ V}$ to $\pm 18\text{ V}$	110	130	115	130	120	130	dB	
	T_{min} to T_{max}	110	130	115	130	120	130	dB	
FREQUENCY RESPONSE	Closed-Loop Bandwidth	0.5	0.9	0.5	0.9	0.5	0.9	MHz	
	Slew Rate	0.15	0.3	0.15	0.3	0.15	0.3	V/μs	
INPUT RESISTANCE	Differential	24	100	45	200	60	200	MΩ	
	Common Mode		200		300		400	GΩ	
OUTPUT CHARACTERISTICS	Voltage								
	$R_{LOAD} \geq 10\text{ k}\Omega$	13.5	14	13.5	14	13.5	14	±V	
	$R_{LOAD} \geq 2\text{ k}\Omega$	12.5	13.0	12.5	13.0	12.5	13.0	±V	
	$R_{LOAD} \geq 1\text{ k}\Omega$	12.0	12.5	12.0	12.5	12.0	12.5	±V	
	$R_{LOAD} \geq 2\text{ k}\Omega$								
T_{min} to T_{max}	12.0	13.0	12.0	13.0	12.0	13.0	±V		
OPEN-LOOP OUTPUT RESISTANCE		60		60		60		Ω	
POWER SUPPLY Current, Quiescent	$V_S = \pm 15\text{ V}$	2.5	3	2.5	3	2.5	3	mA	
	Power Consumption, No Load	75	90	75	90	75	90	mW	
	$V_S = \pm 3\text{ V}$	7.5	9.0	7.5	9.0	7.5	9.0	mW	
TEMPERATURE RANGE	Operating, Rated Performance								
	Commercial	0 to +70°C	AD707JN, AD707JR	AD707KN, AD707KR ¹		AD707CQ, AD707CH			
	Industrial	-40°C to +85°C	AD707AQ, AD707AH	AD707BQ, AD707BH					
	Military	-55°C to +125°C	AD707AR	AD707SQ, AD707SH		AD707TQ, AD707TH			

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	Conditions	Min	AD707J/A Typ	Max	Min	AD707K/B/S Typ	Max	Min	AD707C/T Typ	Max	Units
PACKAGE OPTIONS ²											
Plastic (N-8)		AD707JN			AD707KN			AD707CQ/TQ, AD707TQ/883B			
Cerdip (Q-8)		AD707AQ			AD707BQ/SQ, AD707SQ/883B			AD707CQ/TQ, AD707TQ/883B			
TO-99 (H-08A)		AD707AH			AD707BH/SH, AD707SH/883B			AD707CH/TH, AD707TH/883B			
SOIC (R-8)		AD707JR, AD707AR			AD707KR						
Tape and Reel		AD707JR-Reel, AD707AR-Reel			AD707KR-Reel						
Chips		AD707J-Chips			AD707S-Chips						

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NOTES

¹AD707KR devices are production tested at +25°C only. All T_{min} to T_{max} specifications are guaranteed but not 100% tested for this grade.²For outline information see Package Information section.

All min and max specifications are guaranteed. Specifications in boldface are tested on all production units at final electrical test. Results from those tests are used to calculate outgoing quality levels.

Specifications subject to change without notice.

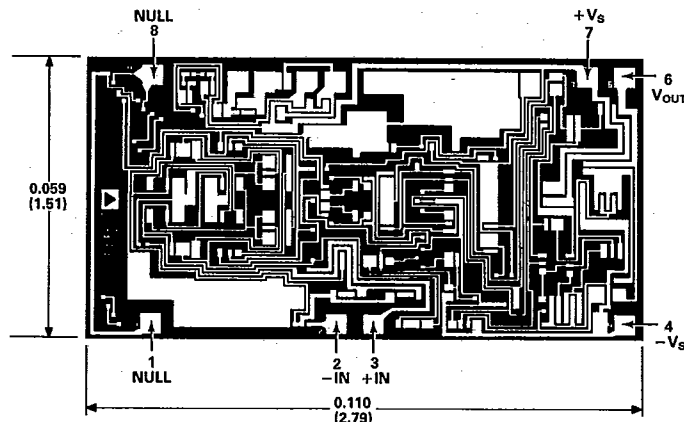
ABSOLUTE MAXIMUM RATINGS¹

Supply Voltage	±22 V
Internal Power Dissipation ²	500 mW
Input Voltage	± V_S
Output Short Circuit Duration	Indefinite
Differential Input Voltage	+ V_S and - V_S
Storage Temperature Range (Q, H)	-65°C to +150°C
Storage Temperature Range (N, R)	-65°C to +125°C
Lead Temperature Range (Soldering 60 sec)	+300°C

NOTES

¹Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.²8-pin plastic package: $\theta_{JA} = 165^\circ\text{C/Watt}$; 8-pin cerdip package: $\theta_{JA} = 110^\circ\text{C/Watt}$; 8-pin small outline package: $\theta_{JA} = 155^\circ\text{C/Watt}$; 8-pin header package: $\theta_{JA} = 200^\circ\text{C/Watt}$.

METALIZATION PHOTOGRAPH

Dimensions shown in inches and (mm).
Contact factory for latest dimensions.

AD707—Typical Characteristics

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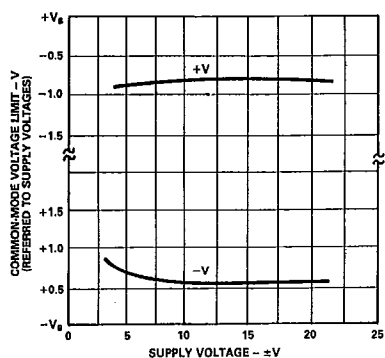


Figure 1. Input Common-Mode Range vs. Supply Voltage

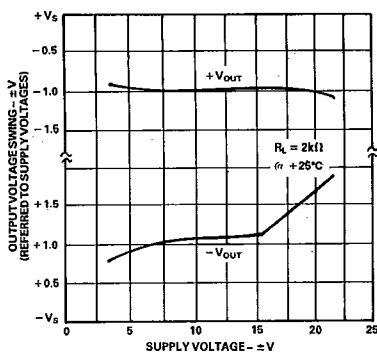


Figure 2. Output Voltage Swing vs. Supply Voltage

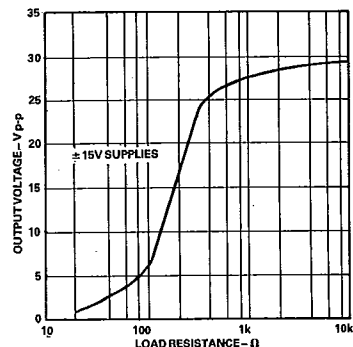


Figure 3. Output Voltage Swing vs. Load Resistance

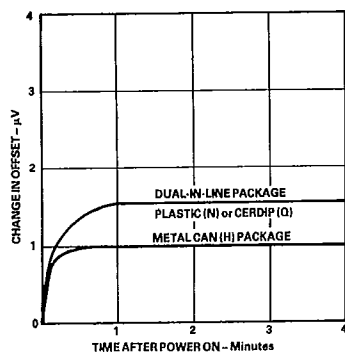


Figure 4. Offset Voltage Warm-Up Drift

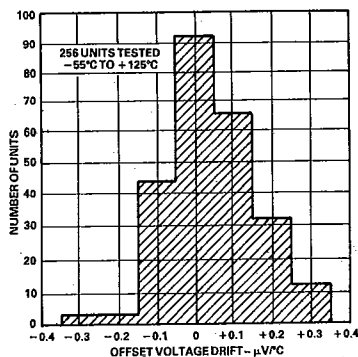


Figure 5. Typical Distribution of Offset Voltage Drift

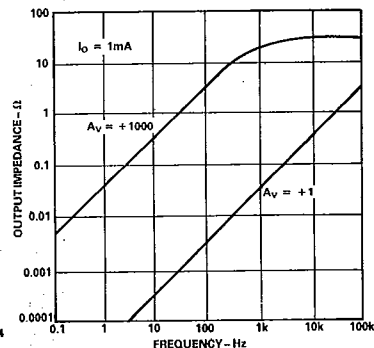


Figure 6. Output Impedance vs. Frequency

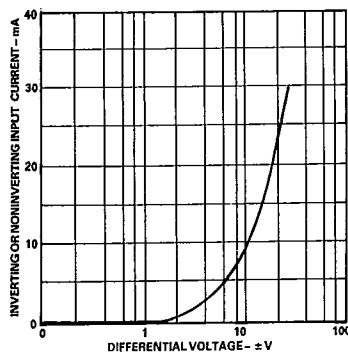


Figure 7. Input Current vs. Differential Input Voltage

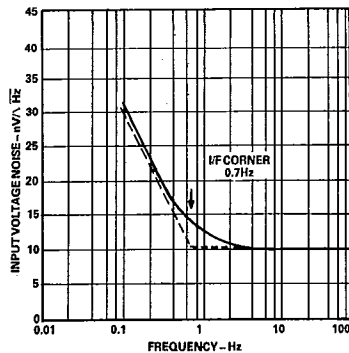


Figure 8. Input Noise Spectral Density

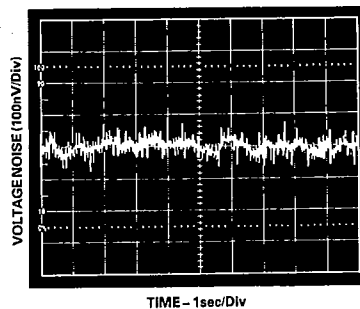


Figure 9. 0.1 Hz to 10 Hz Voltage Noise

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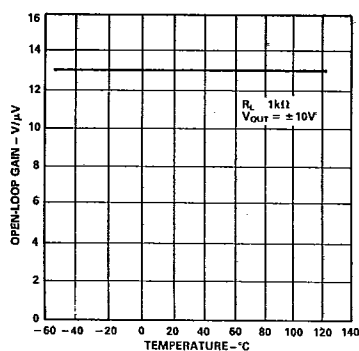


Figure 10. Open-Loop Gain vs. Temperature

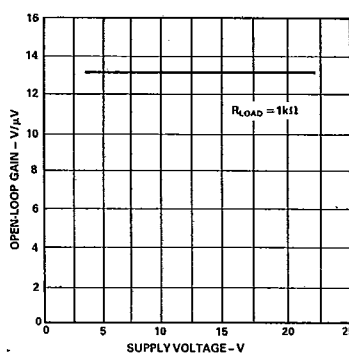


Figure 11. Open-Loop Gain vs. Supply Voltage

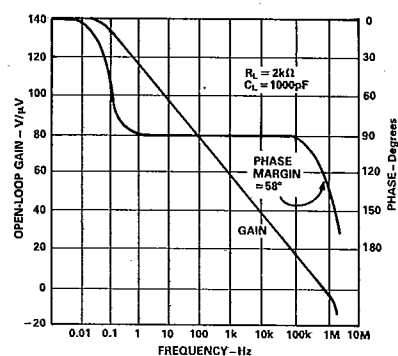


Figure 12. Open-Loop Gain and Phase vs. Frequency

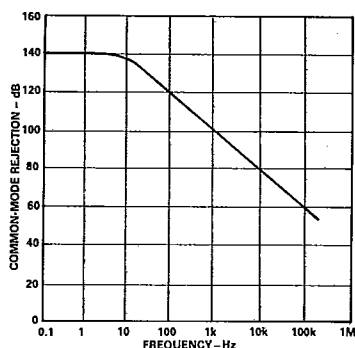


Figure 13. Common-Mode Rejection vs. Frequency

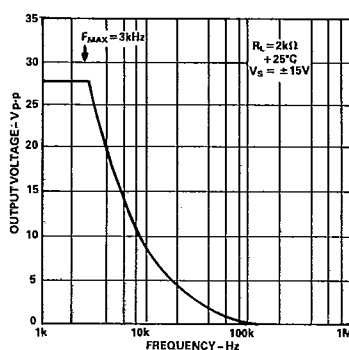


Figure 14. Large Signal Frequency Response

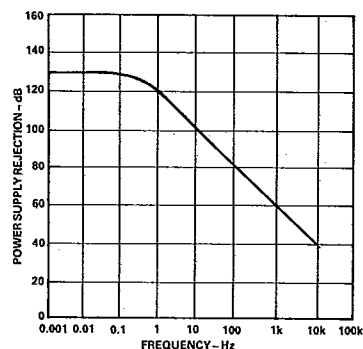


Figure 15. Power Supply Rejection vs. Frequency

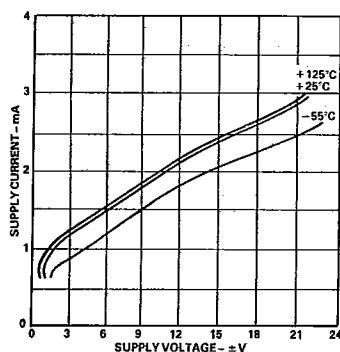


Figure 16. Supply Current vs. Supply Voltage

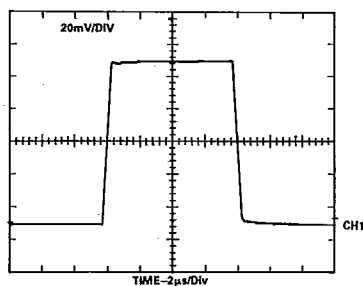


Figure 17. Small Signal Transient Response;
 $A_V = +1$, $R_L = 2\text{ k}\Omega$, $C_L = 50\text{ pF}$

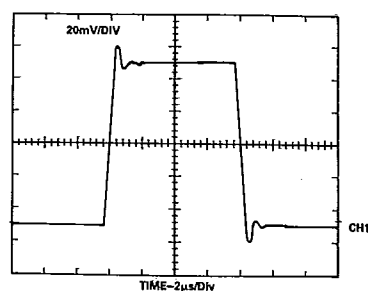


Figure 18. Small Signal Transient Response;
 $A_V = +1$, $R_L = 2\text{ k}\Omega$, $C_L = 1000\text{ pF}$

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OFFSET NULLING

The input offset voltage of the AD707 is the lowest available in a bipolar op amp, but if additional nulling is required, the circuit shown in Figure 19 offers a null range of 200 μ V. For wider null capability, omit R1 and substitute a 20 k Ω potentiometer for R2.

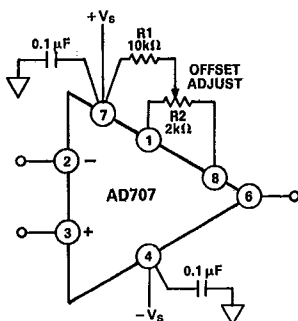


Figure 19. External Offset Nulling and Power Supply Bypassing

GAIN LINEARITY INTO A 1 k Ω LOAD

The gain and gain linearity of the AD707 are the highest available among monolithic bipolar amplifiers. Unlike other dc precision amplifiers, the AD707 shows no degradation in gain or gain linearity when driving loads in excess of 1 k Ω over a ± 10 V output swing. This means high gain accuracy is assured over the output range. Figure 20 shows the gain of the AD707, AD OP-07, and the OP-77 amplifiers when driving a 1 k Ω load.

The AD707 will drive 10 mA of output current with no significant effect on its gain or linearity.

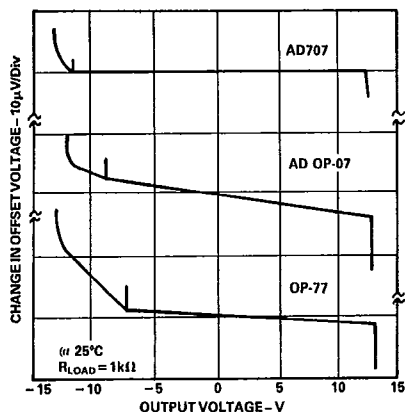


Figure 20. Gain Linearity of the AD707 vs. Other DC Precision Op Amps

OPERATION WITH A GAIN OF 100

Demonstrating the outstanding dc precision of the AD707 in practical applications, Table I shows an error budget calculation for the gain of -100 configuration shown in Figure 21.

Table I. Error Budget

Error Source	Maximum Error Contribution $A_V = 100$ (C Grade) (Full Scale: $V_{OUT} = 10$ V, $V_{IN} = 100$ mV)	
V_{OS}	15 μ V/100 mV	= 150 ppm
I_{OS}	(100 Ω)(1 nA)/100 mV	= 1 ppm
Gain (2 k Ω Load)	(100 V/8 $\times 10^6$)/100 mV	= 13 ppm
Noise	0.35 μ V/100 mV	= 4 ppm
V_{OS} Drift	(0.1 V/ $^{\circ}$ C)/100 mV	= 1 ppm/ $^{\circ}$ C
		= 168 ppm
		+1 ppm/ $^{\circ}$ C

Total Unadjusted Error

$$\text{at } +25^{\circ}\text{C} = 168 \text{ ppm} > 12 \text{ Bits}$$

$$\text{at } -55^{\circ}\text{C to } +125^{\circ}\text{C} = 268 \text{ ppm} > 11 \text{ Bits}$$

With Offset Calibrated Out

$$\text{at } +25^{\circ}\text{C} = 17 \text{ ppm} > 15 \text{ Bits}$$

$$\text{at } -55^{\circ}\text{C to } +125^{\circ}\text{C} = 117 \text{ ppm} > 13 \text{ Bits}$$

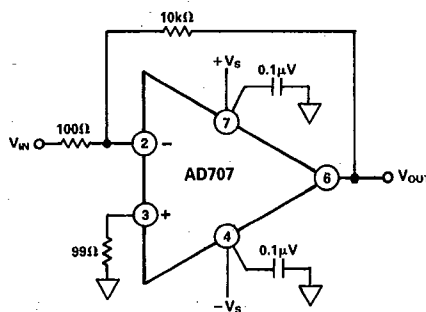


Figure 21. Gain of -100 Configuration

Although the initial offset voltage of the AD707 is very low, it is nonetheless the major contributor to system error. In cases requiring additional accuracy, the circuit shown in Figure 19 can be used to null out the initial offset voltage. This method will also cancel the effects of input offset current error. With the offsets nulled, the AD707C will add less than 17 ppm of error.

This error budget assumes no error in the resistor ratio and no errors from power supply variation (the 120 dB minimum PSRR of the AD707C makes this a good assumption). The external resistors can cause gain error from mismatch and drift over temperature.

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18-BIT SETTLING TIME

Figure 22 shows the AD707 settling to within $80 \mu\text{V}$ of its final value for a 20 V output step in less than $100 \mu\text{s}$ (in the test configuration shown in Figure 23). To achieve settling to 18 bits, any amplifier specified to have a gain of $4 \text{ V}/\mu\text{V}$ would appear to be good enough, however, this is not the case. In order to truly achieve 18-bit accuracy, the gain linearity must be better than 4 ppm.

The gain nonlinearity of the AD707 does not contribute to the error, and the gain itself only contributes 0.1 ppm. The gain error, along with the V_{OS} and V_{OS} drift errors do not comprise 1 LSB of error in a 18-bit system over the military temperature range. If calibration is used to null offset errors, the AD707 resolves up to 20 bits at $+25^\circ\text{C}$.

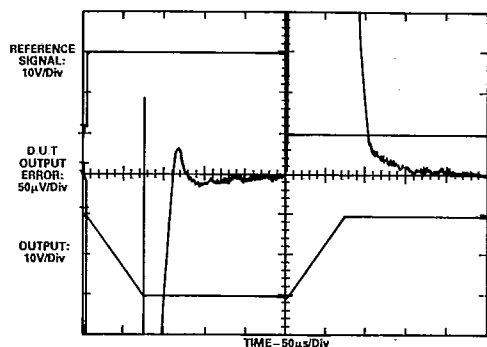


Figure 22. 18-Bit Settling

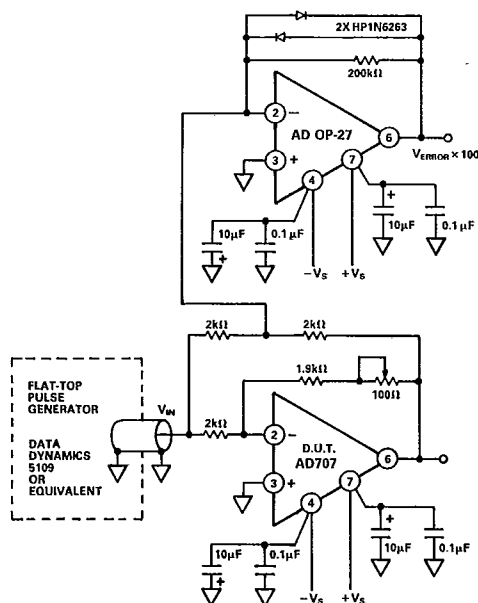


Figure 23. Op Amp Settling Time Test Circuit

140 dB CMRR INSTRUMENTATION AMPLIFIER

The extremely tight dc specifications of the AD707 enable the designer to build very high performance, high gain instrumentation amplifiers without having to select matched op amps for the crucial first stage. For the second stage, the lowest grade AD707 is ideally suited. The CMRR is typically the same as the high grade parts, but does not exact a premium for drift performance (which is less critical in the second stage). Figure 24 shows an example of the classic instrumentation amp. Figure 25 shows that the circuit has at least 140 dB of common-mode rejection for a $\pm 10 \text{ V}$ common-mode input at a gain of 1001 ($R_G = 20 \Omega$).

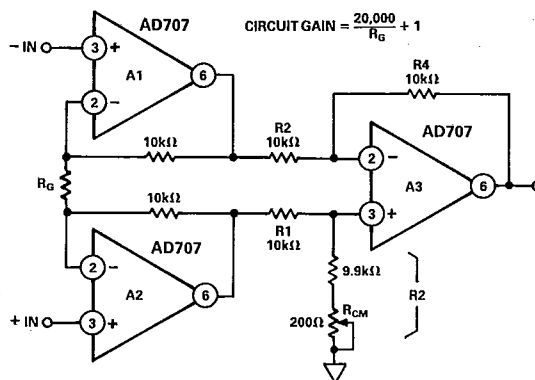


Figure 24. A 3 Op Amp Instrumentation Amplifier

High CMRR is obtained by first adjusting R_{CM} until the output does not change as the input is swept through the full common-mode range. The value of R_G should then be selected to achieve the desired gain. Matched resistors should be used for the output stage so that R_{CM} is as small as possible. The smaller the value of R_{CM} , the lower the noise introduced by potentiometer wiper vibrations. To maintain the CMRR at 140 dB over a 20°C range, the resistor ratios in the output stage, R_1/R_2 and R_3/R_4 , must track each other better than $10 \text{ ppm}/^\circ\text{C}$.

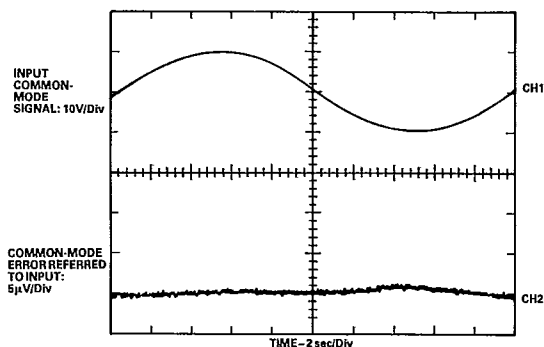


Figure 25. Instrumentation Amplifier Common-Mode Rejection

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PRECISION CURRENT TRANSMITTER

The AD707's excellent dc performance, especially the low offset voltage, low offset voltage drift and high CMRR, makes it possible to make a high precision voltage-controlled current transmitter using a variation of the Howland Current Source circuit (Figure 26). This circuit provides a bidirectional load current which is derived from a differential input voltage.

The performance and accuracy of this circuit will depend almost entirely on the tolerance and selection of the resistors. The scale resistor (R_{SCALE}) and the four feedback resistors directly affect the accuracy of the load current and should be chosen carefully or trimmed.

As an example of the accuracy achievable, assume I_L must be 10 mA, and the available V_{IN} is only 10 mV.

$$R_{SCALE} = 10 \text{ mV}/10 \text{ mA} = 1 \Omega$$

I_{ERROR} due to the AD707C:

$$\begin{aligned} \text{Maximum } I_{ERROR} &= 2(V_{OS})/R_{SCALE} + 2(V_{OS} \text{ Drift})/R_{SCALE} + \\ &\quad I_{OS} (100 \text{ k}/R_{SCALE}) \\ &= 2 (15 \mu\text{V})/1 \Omega + 2 (0.1 \mu\text{V}/^\circ\text{C})/1 \Omega \\ &\quad + 1 \text{ nA} (100 \text{ k})/1 \Omega (1.5 \text{ nA @ } 125^\circ\text{C}) \\ &= 30 \mu\text{A} + 0.2 \mu\text{A}/^\circ\text{C} + 100 \mu\text{A} \\ &\quad (150 \mu\text{A @ } 125^\circ\text{C}) \\ &= 130 \mu\text{A}/10 \text{ mA} = 1.3\% \text{ @ } 25^\circ\text{C} \\ &= 120 \mu\text{A}/10 \text{ mA} = 2.00.25\% \text{ @ } 125^\circ\text{C} \end{aligned}$$

Low drift, high accuracy resistors are required to achieve high precision.

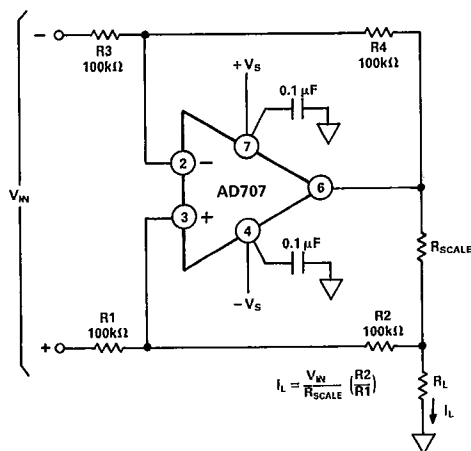


Figure 26. Precision Current Source/Sink