

CURRENT SHUNT MONITORS

–16-V to 80-V COMMON MODE RANGE

Check for Samples: [INA193A-EP](#)

FEATURES

- Wide Common-Mode Voltage:
–16 V to 80 V
- Low Error: 3.0% Over Temp (Max)
- Bandwidth: Up to 500 kHz
- Three Transfer Functions Available: 20 V/V, 50 V/V, and 100 V/V
- Complete Current Sense Solution

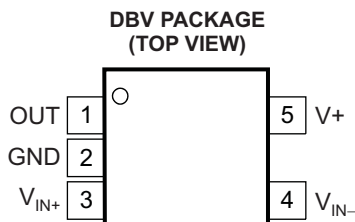
APPLICATIONS

- Welding Equipment
- Notebook Computers
- Cell Phones
- Telecom Equipment
- Automotive
- Power Management
- Battery Chargers

SUPPORTS DEFENSE, AEROSPACE, AND MEDICAL APPLICATIONS

- Controlled Baseline
- One Assembly/Test Site
- One Fabrication Site
- Available in Military (–55°C/125°C)
Temperature Range ⁽¹⁾
- Extended Product Life Cycle
- Extended Product-Change Notification
- Product Traceability

(1) Additional temperature ranges available - contact factory



DESCRIPTION

The INA193A current shunt monitors with voltage output can sense drops across shunts at common-mode voltages from –16 V to 80 V, independent of the INA19x supply voltage. They are available with three output voltage scales: 20 V/V, 50 V/V, and 100 V/V. The 500-kHz bandwidth simplifies use in current control loops.

The INA193A operates from a single 2.7-V to 18-V supply, drawing a maximum of 1300-μA of supply current. It is specified over the extended operating temperature range (–55°C to 125°C), and is offered in a space-saving SOT23 package.



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

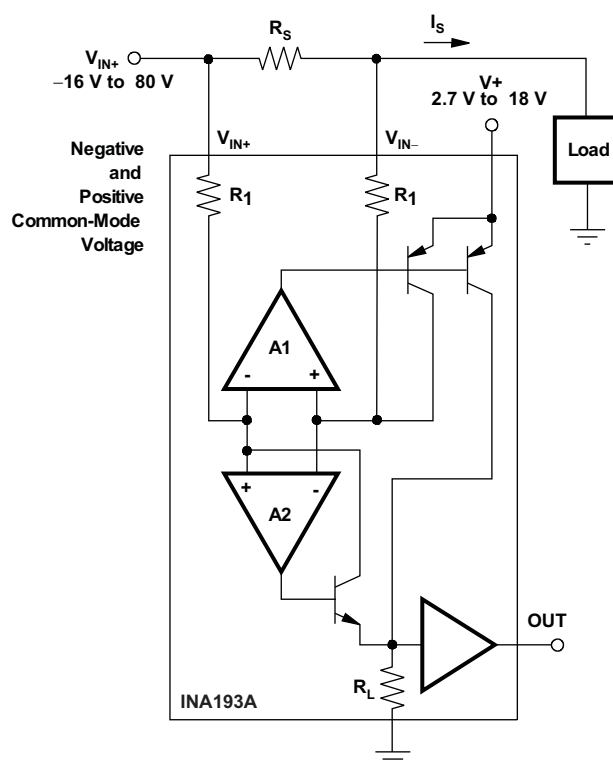
ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

ORDERING INFORMATION⁽¹⁾

| T _A | PACKAGE ⁽²⁾ | ORDERABLE PART NUMBER | TOP-SIDE MARKING |
|----------------|------------------------|-----------------------|------------------|
| –55°C to 125°C | SOT23-5 – DBV | INA193AMDBVREP | CCC |

- (1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.
- (2) Package drawings, standard packing quantities, thermal data, symbolization, and PCB design guidelines are available at www.ti.com/sc/package.

| MODEL | GAIN | PACKAGE |
|---------|--------|---------|
| INA193A | 20 V/V | SOT23-5 |



Absolute Maximum Ratings⁽¹⁾

over operating free-air temperature range (unless otherwise noted)

| | | | MIN | MAX | UNIT |
|---|----------------------------|---|-----------|------------|------|
| Supply voltage | | | | 18 | V |
| V _{IN+} V _{IN-} | Analog input voltage range | Differential (V _{IN+} – V _{IN-}) | –18 | 18 | V |
| | | Common mode ⁽²⁾ | –16 | 80 | |
| Analog outputt voltage range ⁽²⁾ | | OUT | GND – 0.3 | (V+) + 0.3 | V |
| Input current into any pin ⁽²⁾ | | | 5 | | mA |
| Operating temperature range | | | –55 | 150 | °C |
| Storage temperature range | | | –65 | 150 | °C |
| Junction temperature | | | | 150 | °C |
| ESD ratings | Human-Body Model (HBM) | | 4000 | | V |
| | Charged-Device Model (CDM) | | 1000 | | |

(1) Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) Input voltage at any pin may exceed the voltage shown if the current at that pin is limited to 5 mA.

Electrical Characteristics

$V_S = +12$ V. **Boldface** limits apply over the specified temperature range, $T_A = -55^{\circ}\text{C}$ to 125°C . All specifications at $T_A = 25^{\circ}\text{C}$, $V_S = 12$ V, $V_{IN+} = 12$ V, and $V_{SENSE} = 100$ mV (unless otherwise noted).

| PARAMETER | | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
|---|--------------|--|------------|---------------------------|----------------------------|--------------------------------|
| INPUT | | | | | | |
| Full-scale input voltage | V_{SENSE} | $V_{SENSE} = V_{IN+} - V_{IN-}$ | | 0.15 | $(V_S - 0.2)/\text{Gain}$ | V |
| Common-mode input range | V_{CM} | | -16 | | 80 | V |
| Common-mode rejection | CMR | $V_{IN+} = -16$ V to 80 V | 80 | 94 | | dB |
| Over temperature | | $V_{IN+} = 12$ V to 80 V | 100 | 120 | | dB |
| Offset voltage, RTI | V_{OS} | | | ± 0.5 | 2 | mV |
| Over temperature | | | | 0.5 | 3 | mV |
| vs temperature | dV_{OS}/dT | | | 2.5 | | $\mu\text{V}/^{\circ}\text{C}$ |
| vs power supply | PSR | $V_S = 2.7$ V to 18 V, $V_{IN+} = 18$ V | | 5 | 100 | $\mu\text{V}/\text{V}$ |
| Input bias current, V_{IN-} pin | I_B | | | ± 8 | ± 23 | μA |
| OUTPUT ($V_{SENSE} \geq 20$ mV) | | | | | | |
| Gain | G | | | 20 | | V/V |
| Gain error | | $V_{SENSE} = 20$ mV to 100 mV, $T_A = 25^{\circ}\text{C}$ | | ± 0.2 | ± 1 | % |
| Over temperature | | $V_{SENSE} = 20$ mV to 100 mV | | | ± 2 | % |
| Total output error ⁽¹⁾ | | | | ± 0.75 | ± 2.2 | % |
| Over temperature | | | | ± 1 | ± 3 | % |
| Nonlinearity error | | $V_{SENSE} = 20$ mV to 100 mV | | ± 0.002 | ± 0.1 | % |
| Output impedance | R_O | | | 1.5 | | Ω |
| Maximum capacitive load | | No sustained oscillation | | 10 | | nF |

(1) Total output error includes effects of gain error and V_{OS} .

Electrical Characteristics (continued)

$V_S = +12\text{ V}$. **Boldface** limits apply over the specified temperature range, $T_A = -55^\circ\text{C}$ to 125°C . All specifications at $T_A = 25^\circ\text{C}$, $V_S = 12\text{ V}$, $V_{IN+} = 12\text{ V}$, and $V_{SENSE} = 100\text{ mV}$ (unless otherwise noted).

| PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
|--|--|-----|-----------------------------|------------------------------|--------------------------------|
| OUTPUT ($V_{SENSE} < 20\text{ mV}$)⁽²⁾ | $-16\text{ V} \leq V_{CM} < 0\text{ V}$ $0\text{ V} \leq V_{CM} \leq V_S$, $V_S = 5\text{ V}$ $V_S < V_{CM} \leq 80\text{ V}$ | | 300 | 0.4 | mV V mV |
| VOLTAGE OUTPUT⁽³⁾ Swing to V+ power-supply rail Swing to GND⁽⁴⁾ | $R_L = 100\text{ K}\Omega$ to GND | | (V+) – 0.1 $V_{GND} + 3$ | (V+) – 0.2 $V_{GND} + 50$ | V mV |
| FREQUENCY RESPONSE | | | | | |
| Bandwidth | BW $C_{LOAD} = 5\text{ pF}$ | | 500 | | kHz |
| Phase margin | $C_{LOAD} < 10\text{ nF}$ | | 40 | | Degrees |
| Slew rate | SR | | 1 | | V/ μs |
| Settling time (1%) | t_S $V_{SENSE} = 10\text{ mV}$ to 100 mV_{PP} , $C_{LOAD} = 5\text{ pF}$ | | 2 | | μs |
| NOISE, RTI | | | | | |
| Voltage noise density | | | 40 | | nV/ $\sqrt{\text{Hz}}$ |
| POWER SUPPLY | | | | | |
| Operating range | V_S | 2.7 | | 18 | V |
| Quiescent Current | I_Q $V_{OUT} = 2\text{ V}$ $V_{SENSE} = 0\text{ mV}$ | | 700 370 | 1300 950 | μA μA |
| TEMPERATURE RANGE | | | | | |
| Specified temperature range | | –55 | | 125 | $^\circ\text{C}$ |
| Operating temperature range | | –55 | | 150 | $^\circ\text{C}$ |
| Storage temperature range | | –65 | | 150 | $^\circ\text{C}$ |
| Thermal resistance, SOT23 | θ_{JA} | | 200 | | $^\circ\text{C/W}$ |

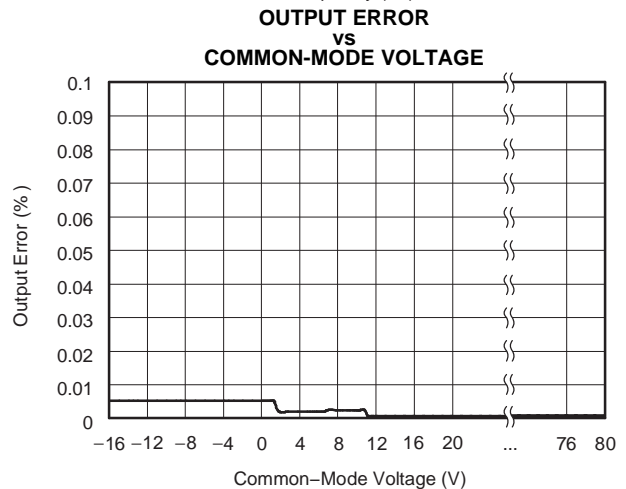
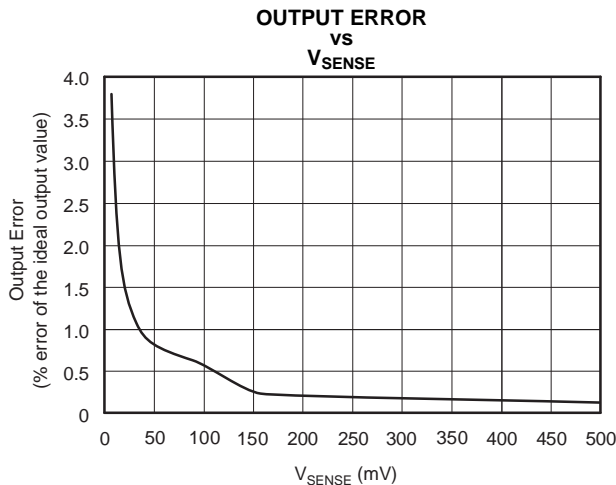
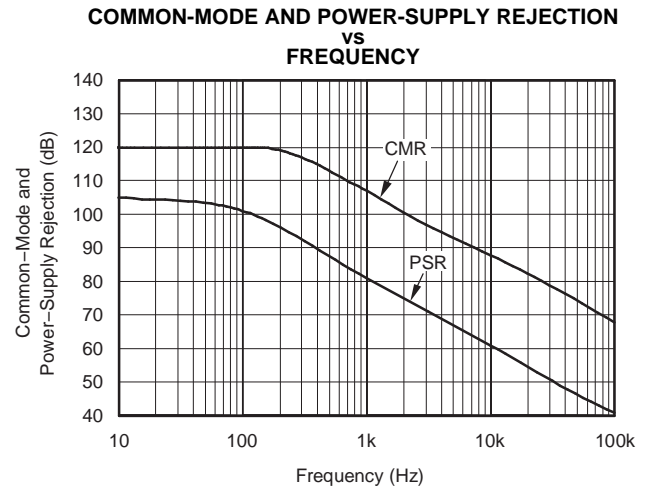
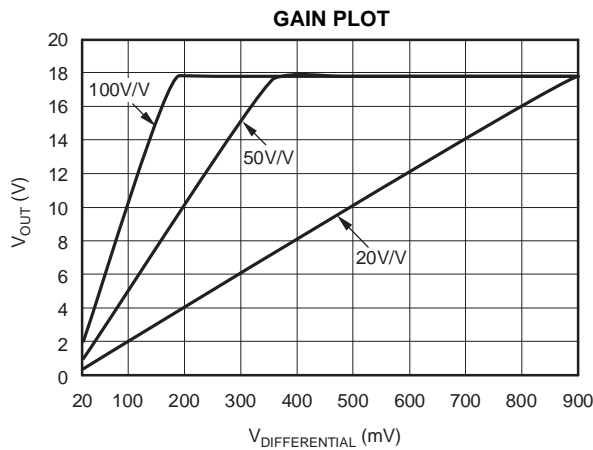
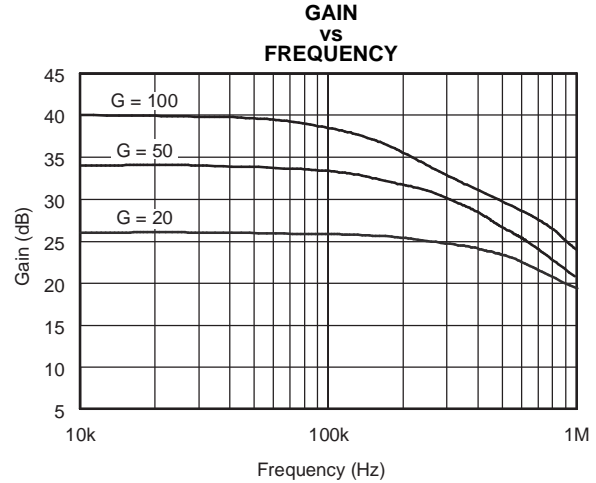
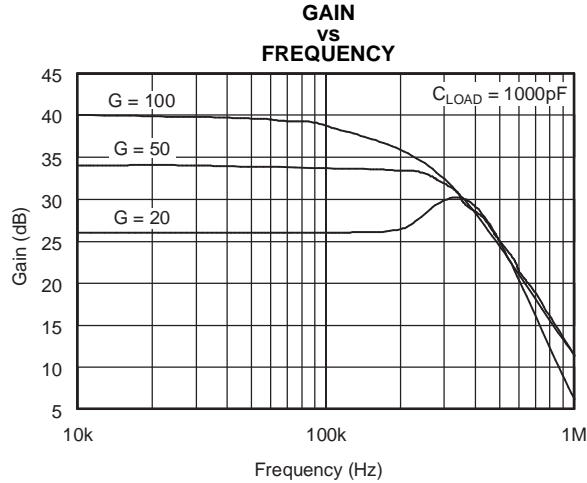
(2) For details on this region of operation, see the *Accuracy Variations as a Result of V_{SENSE} and Common-Mode Voltage* section in the Applications Information.

(3) See Typical Characteristic curve *Output Swing vs Output Current*.

(4) Specified by design

TYPICAL CHARACTERISTICS

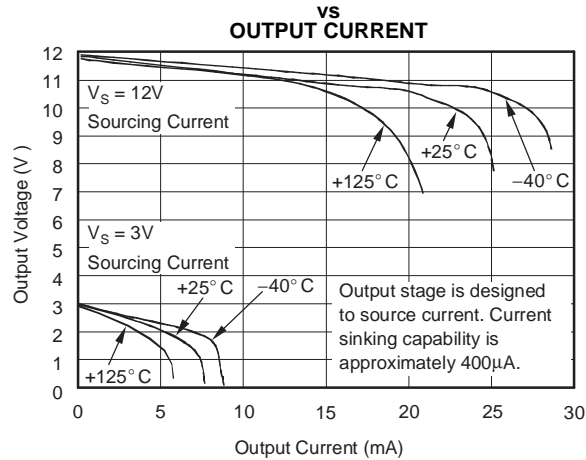
All specifications at $T_A = 25^\circ\text{C}$, $V_S = 12\text{ V}$, and $V_{IN+} = 12\text{ V}$, and $V_{SENSE} = 100\text{ mV}$ (unless otherwise noted).



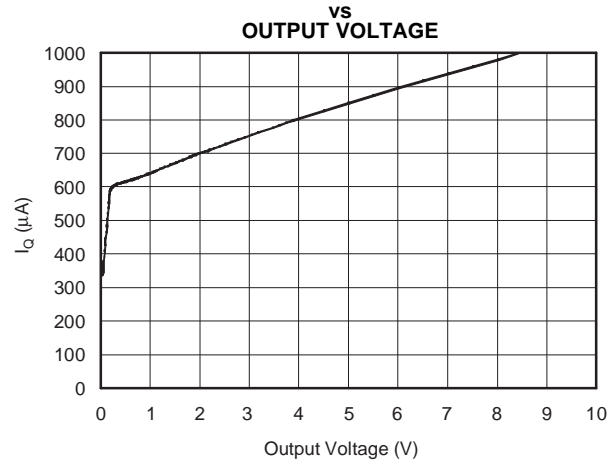
TYPICAL CHARACTERISTICS (continued)

All specifications at $T_A = 25^\circ\text{C}$, $V_S = 12\text{ V}$, and $V_{IN+} = 12\text{ V}$, and $V_{SENSE} = 100\text{ mV}$ (unless otherwise noted).

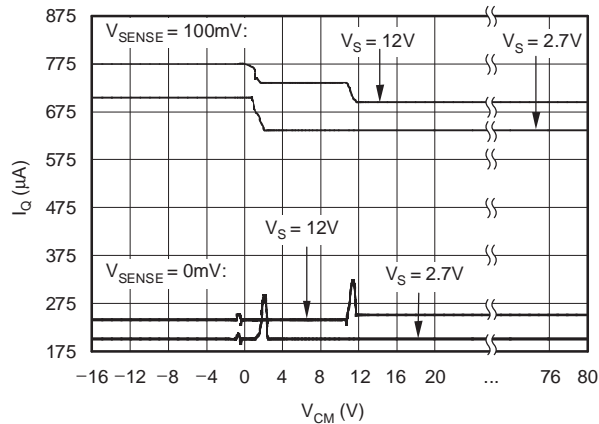
POSITIVE OUTPUT VOLTAGE SWING



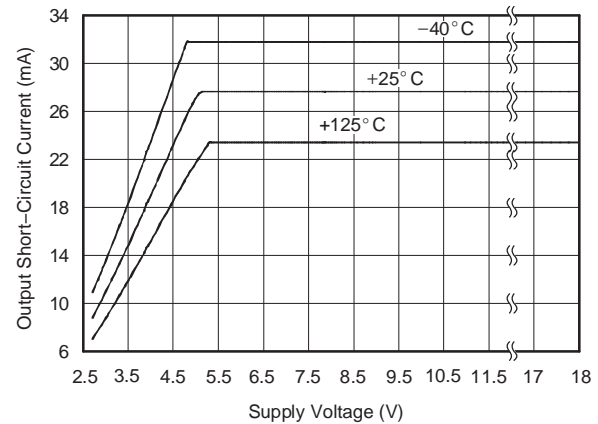
QUIESCENT CURRENT



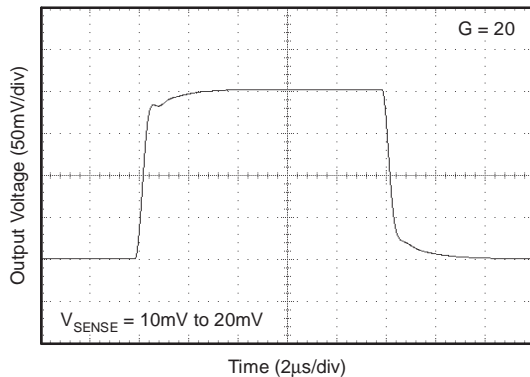
QUIESCENT CURRENT vs COMMON-MODE VOLTAGE



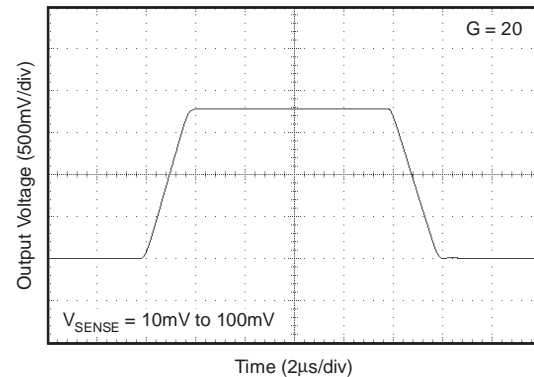
OUTPUT SHORT-CIRCUIT CURRENT vs SUPPLY VOLTAGE



STEP RESPONSE



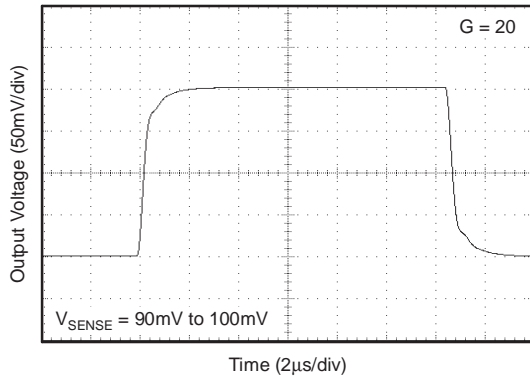
STEP RESPONSE



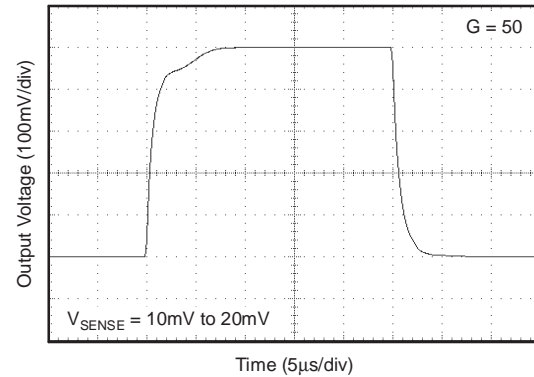
TYPICAL CHARACTERISTICS (continued)

All specifications at $T_A = 25^\circ\text{C}$, $V_S = 12\text{ V}$, and $V_{IN+} = 12\text{ V}$, and $V_{SENSE} = 100\text{ mV}$ (unless otherwise noted).

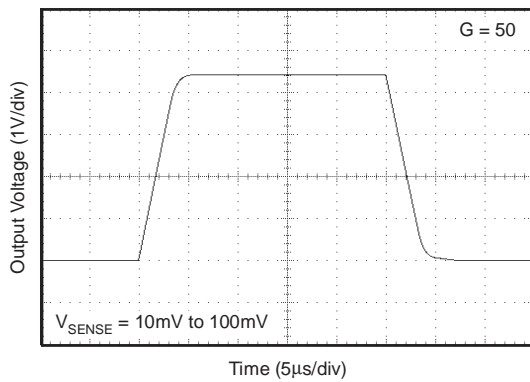
STEP RESPONSE



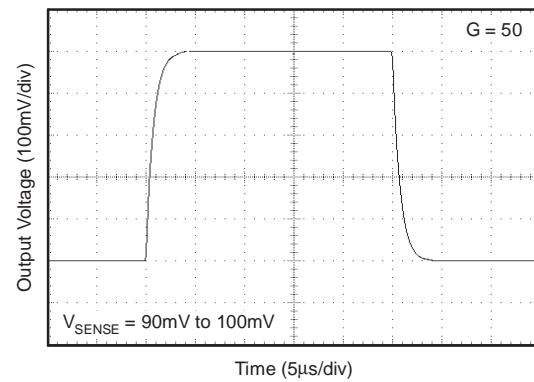
STEP RESPONSE



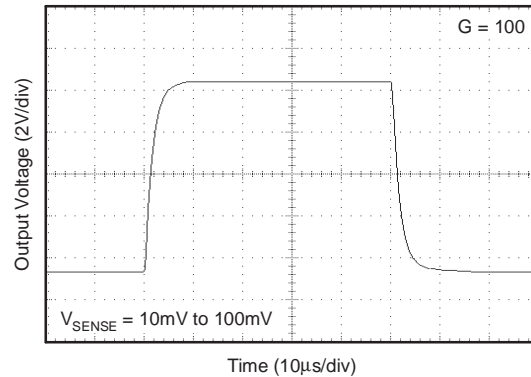
STEP RESPONSE



STEP RESPONSE



STEP RESPONSE



APPLICATION INFORMATION

Basic Connection

Figure 1 shows the basic connection of INA193A. The input pins, V_{IN+} and V_{IN-} , should be connected as closely as possible to the shunt resistor to minimize any resistance in series with the shunt resistance.

Power-supply bypass capacitors are required for stability. Applications with noisy or high impedance power supplies may require additional decoupling capacitors to reject power supply noise. Connect bypass capacitors close to the device pins.

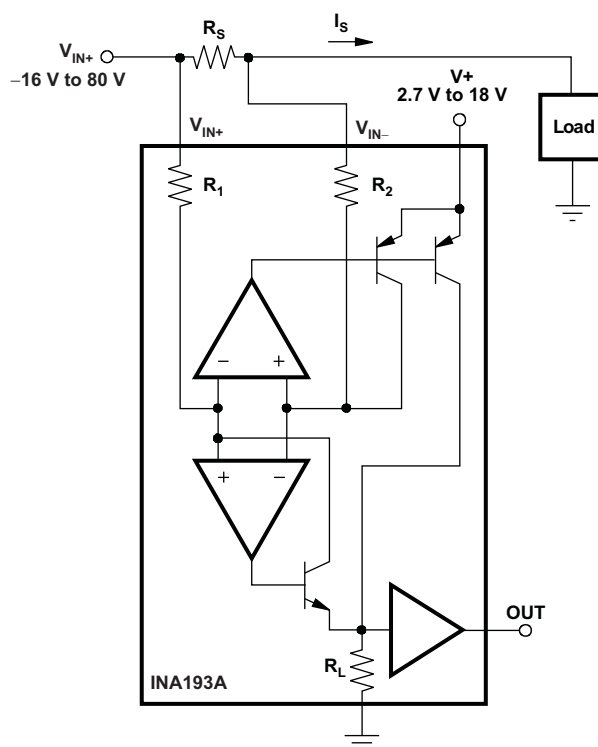


Figure 1. INA193A Basic Connection

Power Supply

The input circuitry of the INA193A can accurately measure beyond its power supply voltage, $V+$. For example, the $V+$ power supply can be 5 V, whereas the load power supply voltage is up to 80 V. The output voltage range of the OUT terminal, however, is limited by the voltages on the power-supply pin.

Accuracy Variations as a Result of V_{SENSE} and Common-Mode Voltage

The accuracy of the INA193A current shunt monitors is a function of two main variables: V_{SENSE} ($V_{IN+} - V_{IN-}$) and common-mode voltage, V_{CM} , relative to the supply voltage, V_S . V_{CM} is expressed as $(V_{IN+} + V_{IN-})/2$; however, in practice, V_{CM} is seen as the voltage at V_{IN+} because the voltage drop across V_{SENSE} is usually small.

This section addresses the accuracy of these specific operating regions:

- Normal Case 1: $V_{\text{SENSE}} \geq 20 \text{ mV}$, $V_{\text{CM}} \geq V_{\text{S}}$
Normal Case 2: $V_{\text{SENSE}} \geq 20 \text{ mV}$, $V_{\text{CM}} < V_{\text{S}}$
Low V_{SENSE} Case 1: $V_{\text{SENSE}} < 20 \text{ mV}$, $-16 \text{ V} \leq V_{\text{CM}} < 0$
Low V_{SENSE} Case 2: $V_{\text{SENSE}} < 20 \text{ mV}$, $0 \text{ V} \leq V_{\text{CM}} \leq V_{\text{S}}$
Low V_{SENSE} Case 3: $V_{\text{SENSE}} < 20 \text{ mV}$, $V_{\text{S}} < V_{\text{CM}} \leq 80 \text{ V}$

Normal Case 1: $V_{\text{SENSE}} \geq 20 \text{ mV}$, $V_{\text{CM}} \geq V_{\text{S}}$

This region of operation provides the highest accuracy. Here, the input offset voltage is characterized and measured using a two-step method. First, the gain is determined by (Equation 1).

$$G = \frac{V_{\text{OUT1}} - V_{\text{OUT2}}}{100 \text{ mV} - 20 \text{ mV}} \quad (1)$$

Where:

V_{OUT1} = Output voltage with $V_{\text{SENSE}} = 100 \text{ mV}$

V_{OUT2} = Output voltage with $V_{\text{SENSE}} = 20 \text{ mV}$

The offset voltage is then measured at $V_{\text{SENSE}} = 100 \text{ mV}$ and referred to the input (RTI) of the current shunt monitor, as shown in (Equation 2).

$$V_{\text{OSRTI}} (\text{Referred-To-Input}) = \left(\frac{V_{\text{OUT1}}}{G} \right) - 100 \text{ mV} \quad (2)$$

In the Typical Characteristics, the *Output Error vs Common-Mode Voltage* curve shows the highest accuracy for the this region of operation. In this plot, $V_{\text{S}} = 12 \text{ V}$; for $V_{\text{CM}} \geq 12 \text{ V}$, the output error is at its minimum. This case is also used to create the $V_{\text{SENSE}} \geq 20 \text{ mV}$ output specifications in the Electrical Characteristics table.

Normal Case 2: $V_{\text{SENSE}} \geq 20 \text{ mV}$, $V_{\text{CM}} < V_{\text{S}}$

This region of operation has slightly less accuracy than Normal Case 1 as a result of the common-mode operating area in which the part functions, as seen in the *Output Error vs Common-Mode Voltage* curve. As noted, for this graph $V_{\text{S}} = 12 \text{ V}$; for $V_{\text{CM}} < 12 \text{ V}$, the Output Error increases as V_{CM} becomes less than 12 V , with a typical maximum error of 0.005% at the most negative $V_{\text{CM}} = -16 \text{ V}$.

Low V_{SENSE} Case 1: $V_{\text{SENSE}} < 20 \text{ mV}$, $-16 \text{ V} \leq V_{\text{CM}} < 0$; and Low V_{SENSE} Case 3: $V_{\text{SENSE}} < 20 \text{ mV}$, $V_{\text{S}} < V_{\text{CM}} \leq 80 \text{ V}$

Although the INA193A is not designed for accurate operation in either of these regions, some applications are exposed to these conditions; for example, when monitoring power supplies that are switched on and off while V_{S} is still applied to the INA193A. It is important to know what the behavior of the devices will be in these regions.

As V_{SENSE} approaches 0 mV, in these V_{CM} regions, the device output accuracy degrades. A larger-than-normal offset can appear at the current shunt monitor output with a typical maximum value of $V_{\text{OUT}} = 300 \text{ mV}$ for $V_{\text{SENSE}} = 0 \text{ mV}$. As V_{SENSE} approaches 20 mV, V_{OUT} returns to the expected output value with accuracy as specified in the Electrical Characteristics. Figure 2 illustrates this effect using the INA195A and INA198A (Gain = 100).

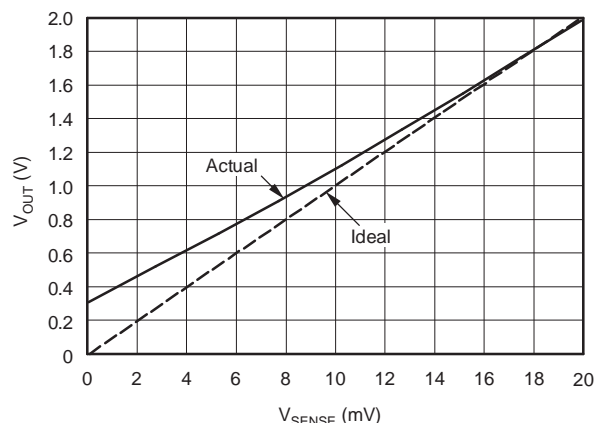
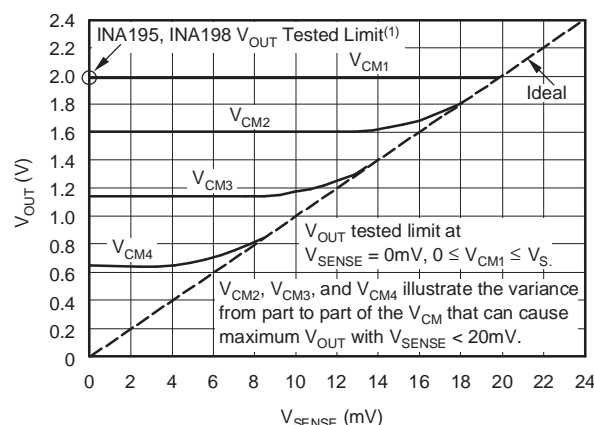


Figure 2. Example for Low V_{SENSE} Cases 1 and 3 (INA195A, INA198A: Gain = 100)

Low V_{SENSE} Case 2: $V_{SENSE} < 20$ mV, 0 V $\leq V_{CM} \leq V_S$

This region of operation is the least accurate for the INA193A. To achieve the wide input common-mode voltage range, these devices use two op amp front ends in parallel. One op amp front end operates in the positive input common-mode voltage range, and the other in the negative input region. For this case, neither of these two internal amplifiers dominates and overall loop gain is very low. Within this region, V_{OUT} approaches voltages close to linear operation levels for Normal Case 2. This deviation from linear operation becomes greatest the closer V_{SENSE} approaches 0 V. Within this region, as V_{SENSE} approaches 20 mV, device operation is closer to that described by Normal Case 2. Figure 3 illustrates this behavior for the INA195A. The V_{OUT} maximum peak for this case is tested by maintaining a constant V_S , setting $V_{SENSE} = 0$ mV and sweeping V_{CM} from 0 V to V_S . The exact V_{CM} at which V_{OUT} peaks during this test varies from part to part, but the V_{OUT} maximum peak is tested to be less than the specified V_{OUT} tested limit.



NOTE: (1) INA193, INA196 V_{OUT} Tested Limit = 0.4V.
INA194, INA197 V_{OUT} Tested Limit = 1V.

Figure 3. Example for Low V_{SENSE} Case 2 (INA195A, INA198A: Gain = 100)

Shutdown

Because the INA193A consumes a quiescent current less than 1 mA, it can be powered by either the output of logic gates or by transistor switches to supply power. Use a totem pole output buffer or gate that can provide sufficient drive along with 0.1- μ F bypass capacitor, preferably ceramic with good high frequency characteristics. This gate should have a supply voltage of 3 V or greater because the INA193A requires a minimum supply greater than 2.7 V. In addition to eliminating quiescent current, this gate also turns off the 10 μ A bias current present at each of the inputs. An example shutdown circuit is shown in [Figure 4](#).

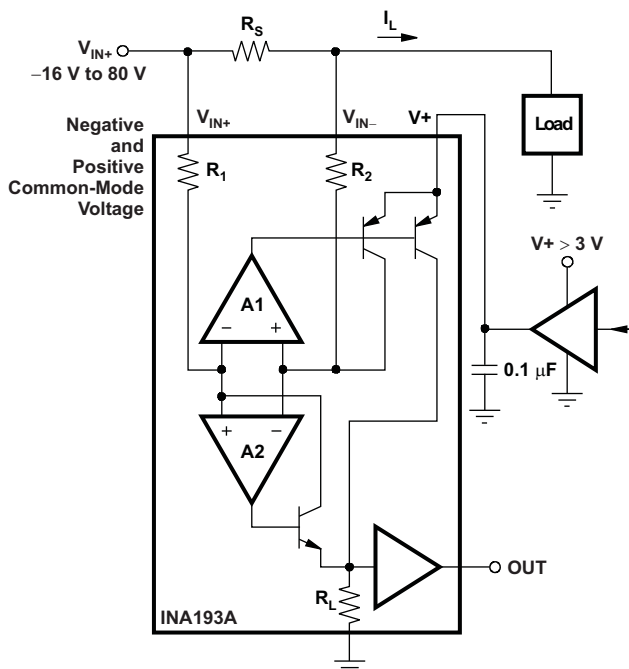


Figure 4. INA193A Example Shutdown Circuit

Selecting R_s

The value chosen for the shunt resistor, R_S , depends on the application and is a compromise between small-signal accuracy and maximum permissible voltage loss in the measurement line. High values of R_S provide better accuracy at lower currents by minimizing the effects of offset, while low values of R_S minimize voltage loss in the supply line. For most applications, best performance is attained with an R_S value that provides a full-scale shunt voltage range of 50 mV to 100 mV. Maximum input voltage for accurate measurements is 500 mV.

Transient Protection

The -16 V to 80 V common-mode range of the INA193A is ideal for withstanding automotive fault conditions ranging from 12-V battery reversal up to 80-V transients, since no additional protective components are needed up to those levels. In the event that the INA193A is exposed to transients on the inputs in excess of its ratings, then external transient absorption with semiconductor transient absorbers (zeners or Transzorbs) will be necessary. Use of MOVs or VDRs is not recommended except when they are used in addition to a semiconductor transient absorber. Select the transient absorber such that it will never allow the INA193A to be exposed to transients greater than 80 V (that is, allow for transient absorber tolerance, as well as additional voltage due to transient absorber dynamic impedance). Despite the use of internal zener type ESD protection, the INA193A does not lend itself to using external resistors in series with the inputs since the internal gain resistors can vary up to $\pm 30\%$ (if gain accuracy is not important, then resistors can be added in series with the INA193A inputs with two equal resistors on each input).

Output Voltage Range

The output of the INA193A is accurate within the output voltage swing range set by the power-supply pin, V+. This is best illustrated when using the INA195A or INA198A (which are both versions using a gain of 100), where a 100 mV full-scale input from the shunt resistor requires an output voltage swing of 10 V, and a power-supply voltage sufficient to achieve 10 V on the output.

RFI/EMI

Attention to good layout practices is always recommended. Keep traces short and, when possible, use a printed circuit board (PCB) ground plane with surface-mount components placed as close to the device pins as possible. Small ceramic capacitors placed directly across amplifier inputs can reduce RFI/EMI sensitivity. PCB layout should locate the amplifier as far away as possible from RFI sources. Sources can include other components in the same system as the amplifier itself, such as inductors (particularly switched inductors handling a lot of current and at high frequencies). RFI can generally be identified as a variation in offset voltage or dc signal levels with changes in the interfering RF signal. If the amplifier cannot be located away from sources of radiation, shielding may be needed. Twisting wire input leads makes them more resistant to RF fields.

Input Filtering

An obvious and straightforward location for filtering is at the output of the INA193A; however, this location negates the advantage of the low output impedance of the internal buffer. The only other option for filtering is at the input pins of the INA193A, which is complicated by the internal 5-k Ω + 30% input impedance; this is illustrated in [Figure 5](#). Using the lowest possible resistor values minimizes both the initial shift in gain and effects of tolerance. The effect on initial gain is given by:

$$\text{GainError\%} = 100 - \left(100 \times \frac{5\text{k}\Omega}{5\text{k}\Omega + R_{\text{FILT}}} \right) \quad (3)$$

Total effect on gain error can be calculated by replacing the 5-k Ω term with 5 k Ω – 30%, (or 3.5 k Ω) or 5 k Ω + 30% (or 6.5 k Ω). The tolerance extremes of R_{FILT} can also be inserted into the equation. If a pair of 100- Ω 1% resistors are used on the inputs, the initial gain error will be approximately 2%. Worst-case tolerance conditions will always occur at the lower excursion of the internal 5-k Ω resistor (3.5 k Ω), and the higher excursion of R_{FILT} – 3% in this case. Note that the specified accuracy of the INA193A must then be combined in addition to these tolerances. While this discussion treated accuracy worst-case conditions by combining the extremes of the resistor values, it is appropriate to use geometric mean or root sum square calculations to total the effects of accuracy variations.

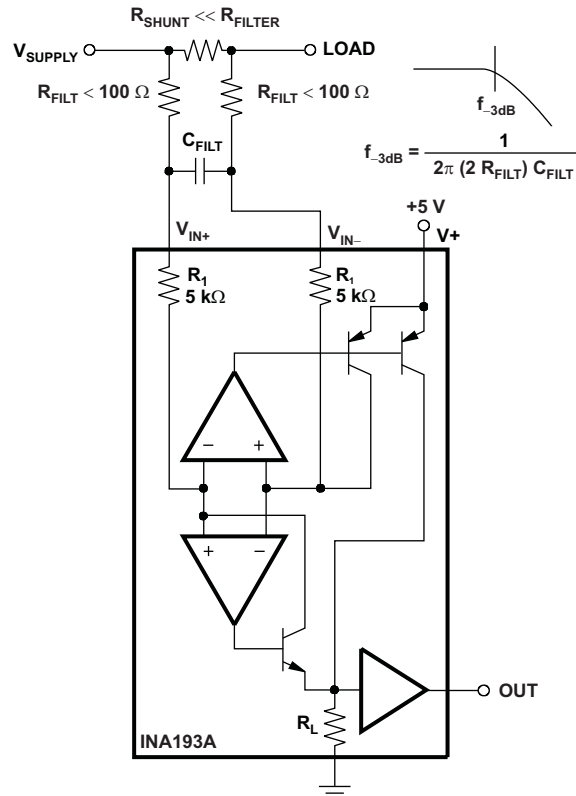


Figure 5. Input Filter (Gain Error – 15% to –2.2%)

Inside the INA193A

The INA193A uses a new, unique internal circuit topology that provides common-mode range extending from –16 V to 80 V while operating from a single power supply. The common-mode rejection in a classic instrumentation amp approach is limited by the requirement for accurate resistor matching. By converting the induced input voltage to a current, the INA193A provides common-mode rejection that is no longer a function of closely matched resistor values, providing the enhanced performance necessary for such a wide common-mode range. A simplified diagram (shown in Figure 6) shows the basic circuit function. When the common-mode voltage is positive, amplifier A2 is active.

The differential input voltage, (V_{IN+}) – (V_{IN-}) applied across R_S, is converted to a current through a resistor. This current is converted back to a voltage through R_L, and then amplified by the output buffer amplifier. When the common-mode voltage is negative, amplifier A1 is active. The differential input voltage, (V_{IN+}) – (V_{IN-}) applied across R_S, is converted to a current through a resistor. This current is sourced from a precision current mirror whose output is directed into R_L converting the signal back into a voltage and amplified by the output buffer amplifier. Patent-pending circuit architecture ensures smooth device operation, even during the transition period where both amplifiers A1 and A2 are active.

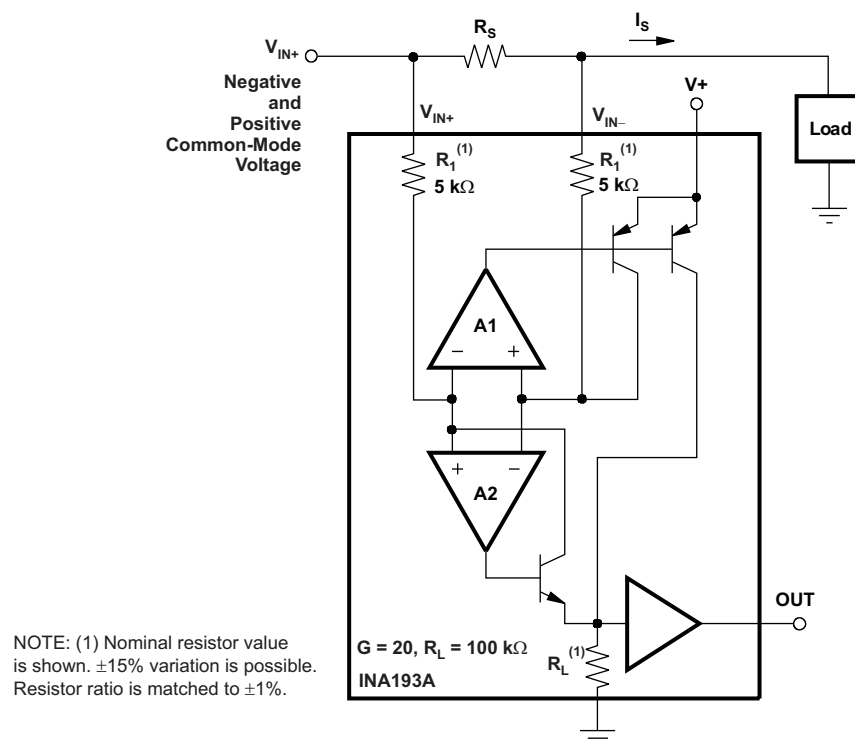


Figure 6. INA193A Simplified Circuit Diagram

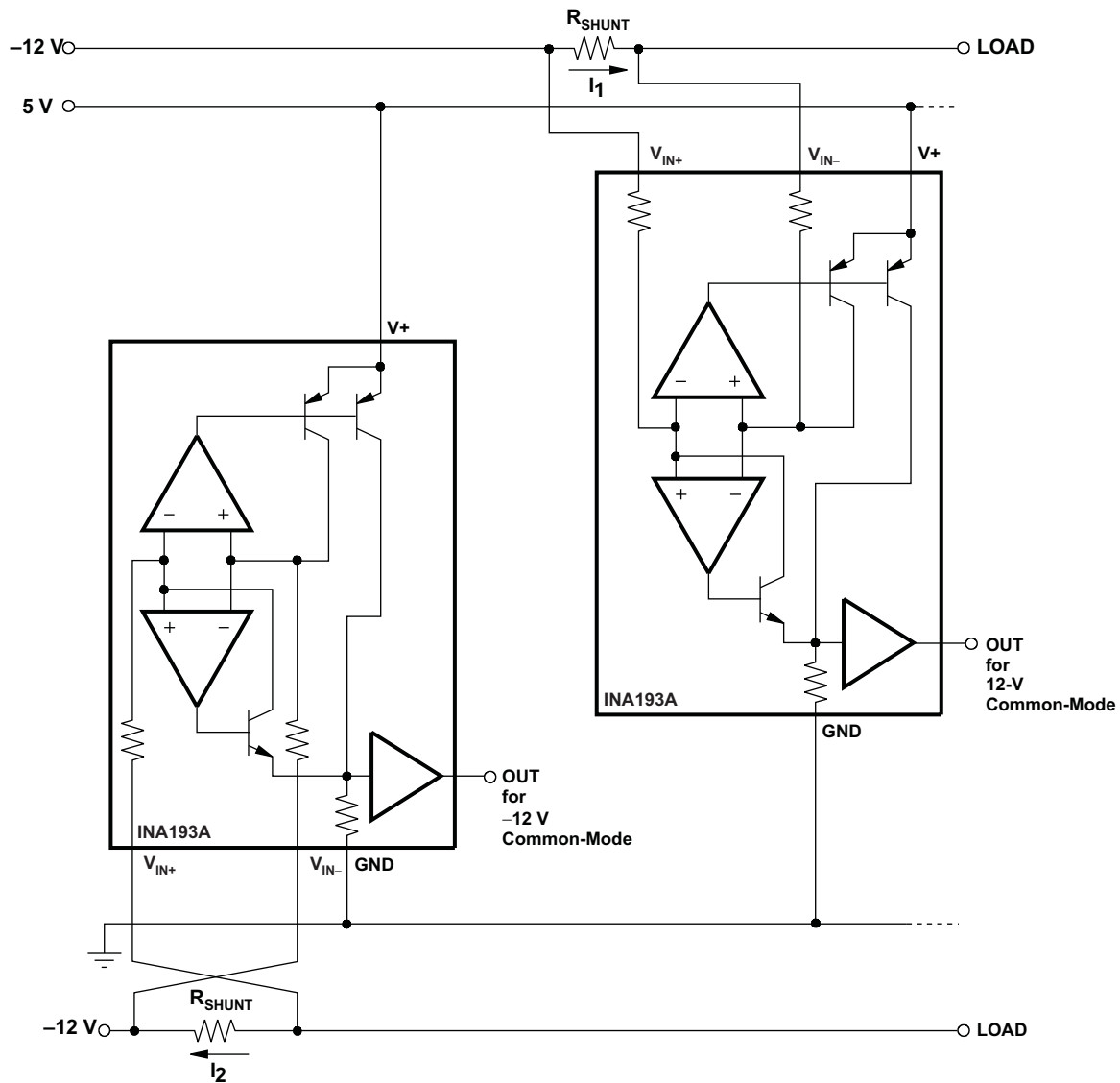


Figure 7. Monitor Bipolar Output Power-Supply Current

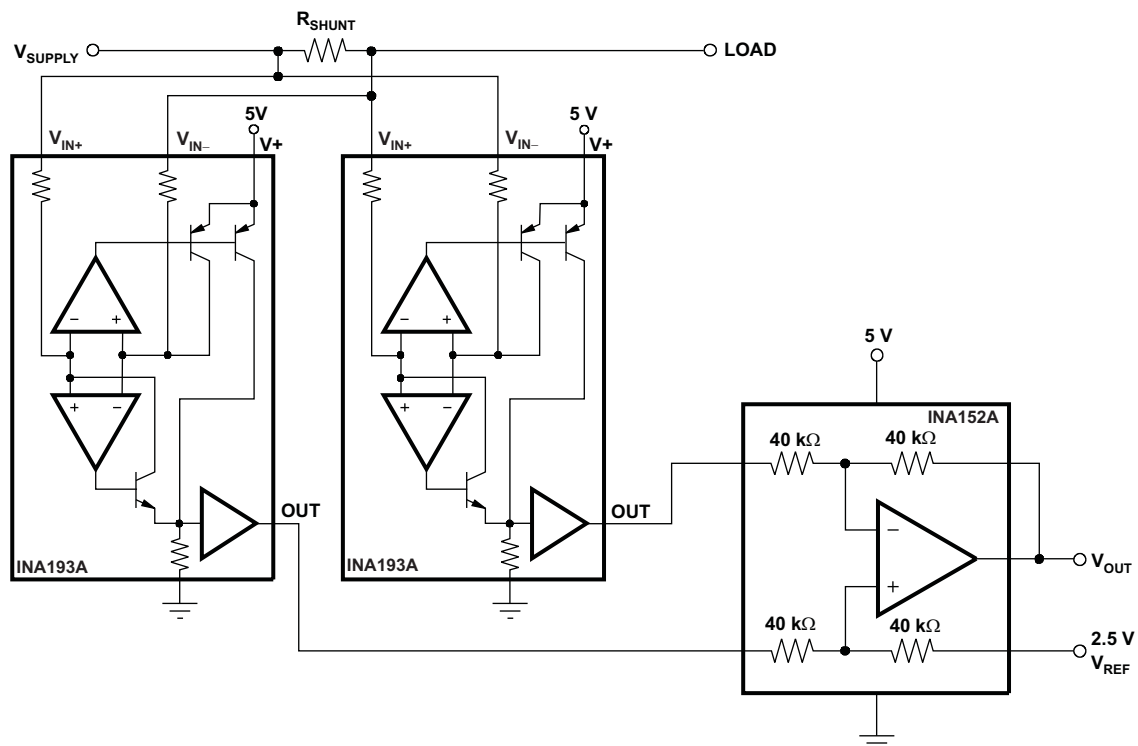


Figure 8. Bidirectional Current Monitoring

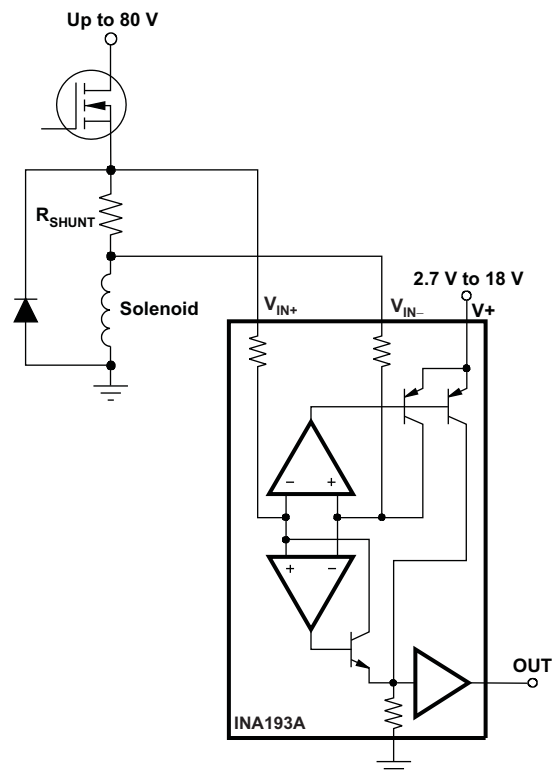


Figure 9. Inductive Current Monitor Including Flyback

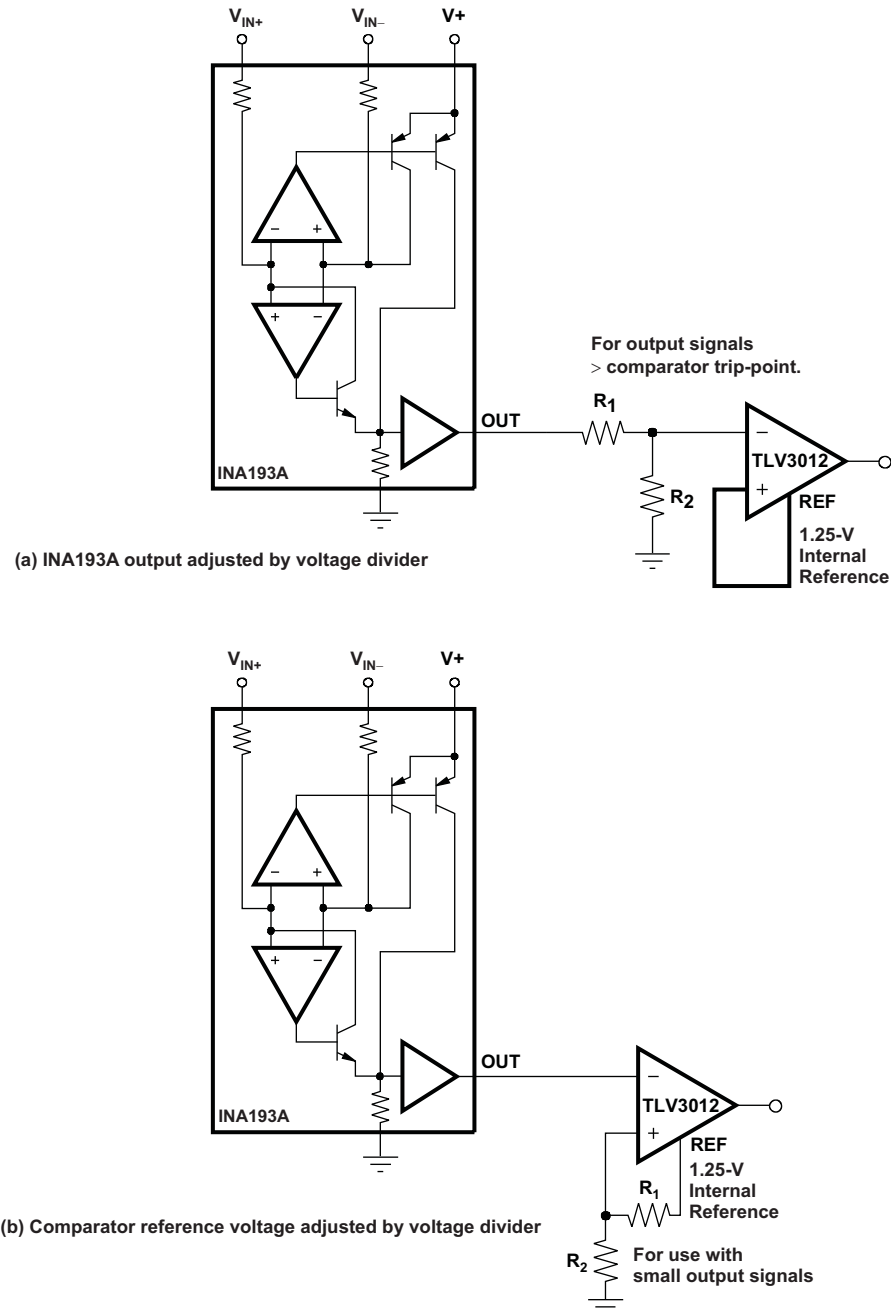


Figure 10. INA193A With Comparator

PACKAGING INFORMATION

| Orderable Device | Status (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan (2) | Lead/Ball Finish | MSL Peak Temp (3) | Op Temp (°C) | Top-Side Markings (4) | Samples |
|------------------|---------------|--------------|--------------------|------|----------------|----------------------------|------------------|----------------------|--------------|--------------------------|-------------------------|
| INA193AMDBVREP | ACTIVE | SOT-23 | DBV | 5 | 3000 | Green (RoHS & no Sb/Br) | CU NIPDAU | Level-2-260C-1 YEAR | -55 to 125 | CCC | Samples |
| INA193AMDBVREPG4 | ACTIVE | SOT-23 | DBV | 5 | 3000 | Green (RoHS & no Sb/Br) | CU NIPDAU | Level-2-260C-1 YEAR | -55 to 125 | CCC | Samples |
| V62/07638-01XE | ACTIVE | SOT-23 | DBV | 5 | 3000 | Green (RoHS & no Sb/Br) | CU NIPDAU | Level-2-260C-1 YEAR | -55 to 125 | CCC | Samples |

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBsolete: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) Multiple Top-Side Markings will be inside parentheses. Only one Top-Side Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Top-Side Marking for that device.

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TAPE AND REEL INFORMATION


*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Reel Diameter (mm) | Reel Width W1 (mm) | A0 (mm) | B0 (mm) | K0 (mm) | P1 (mm) | W (mm) | Pin1 Quadrant |
|----------------|--------------|-----------------|------|------|--------------------|--------------------|---------|---------|---------|---------|--------|---------------|
| INA193AMDBVREP | SOT-23 | DBV | 5 | 3000 | 178.0 | 9.0 | 3.23 | 3.17 | 1.37 | 4.0 | 8.0 | Q3 |

TAPE AND REEL BOX DIMENSIONS



*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
|----------------|--------------|-----------------|------|------|-------------|------------|-------------|
| INA193AMDBVREP | SOT-23 | DBV | 5 | 3000 | 180.0 | 180.0 | 18.0 |

DBV (R-PDSO-G5)

PLASTIC SMALL-OUTLINE PACKAGE



- NOTES:
- A. All linear dimensions are in millimeters.
 - B. This drawing is subject to change without notice.
 - C. Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.15 per side.
 - D. Falls within JEDEC MO-178 Variation AA.

DBV (R-PDSO-G5)

PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in millimeters.
 - B. This drawing is subject to change without notice.
 - C. Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
 - D. Publication IPC-7351 is recommended for alternate designs.
 - E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.

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