

Title	<i>Reference Design Report for a High Efficiency ($\geq 85\%$), High Power Factor (>0.9) TRIAC Dimmable 14 W LED Driver Using LinkSwitchTM-PH LNK406EG</i>
Specification	90 VAC – 265 VAC Input; 28 V _{TYP} , 0.5 A Output
Application	LED Driver
Author	Applications Engineering Department
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Summary and Features

- Superior performance and end user experience
 - TRIAC dimmer compatible (including low cost leading edge type)
 - No output flicker
 - $>1000:1$ dimming range
 - Clean monotonic start-up – no output blinking
 - Fast start-up (<300 ms) – no perceptible delay
 - Consistent dimming performance unit to unit
- Highly energy efficient
 - $\geq 85\%$ at 115 VAC, $\geq 87\%$ at 230 VAC
- Low cost, low component count and small printed circuit board footprint solution
 - Regulated output current with no current sensing required
 - Frequency jitter for smaller, lower cost EMI filter components
- Integrated protection and reliability features
 - Output open circuit / output short-circuit protected with auto-recovery
 - Line input overvoltage shutdown extends voltage withstand during line faults.
 - Auto-recovering thermal shutdown with large hysteresis protects both components and printed circuit board
 - No damage during brown-out or brown-in conditions
- IEC 61000-4-5 ringwave, IEC 61000-3-2 Class C and EN55015 B conducted EMI compliant

PATENT INFORMATION

The products and applications illustrated herein (including transformer construction and circuits external to the products) may be covered by one or more U.S. and foreign patents, or potentially by pending U.S. and foreign patent applications assigned to Power Integrations. A complete list of Power Integrations' patents may be found at www.powerint.com. Power Integrations grants its customers a license under certain patent rights as set forth at <http://www.powerint.com/ip.htm>.



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Important Note: Although this board is designed to satisfy safety isolation requirements, the engineering prototype has not been agency approved. Therefore, all testing should be performed using an isolation transformer to provide the AC input to the prototype board.



1 Introduction

The document describes a high power factor (PF) TRIAC dimmable LED driver designed to drive a nominal LED string voltage of 28 V at 0.5 A from an input voltage range of 90 VAC to 265 VAC. The LED driver utilizes the LNK406EG from the LinkSwitch-PH family of ICs.

LinkSwitch-PH ICs allow the implementation of cost effective and low component count LED drivers which both meet power factor and harmonics limits and also offer enhanced end user experience. This includes ultra-wide dimming range, flicker-free operation (even with low cost with AC line TRIAC dimmers) and fast, clean turn on.

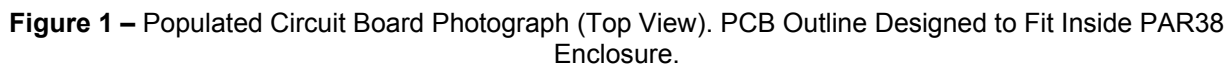
The topology used is an isolated flyback operating in continuous conduction mode. Output current regulation is sensed entirely from the primary side eliminating the need for secondary side feedback components. No external current sensing is required on the primary side either as this is performed inside the IC further reducing components and losses. The internal controller adjusts the MOSFET duty cycle to maintain a sinusoidal input current and therefore high power factor and low harmonic currents.

The LNK406EG also provides a sophisticated range of protection features including auto-restart for open control loop and output short-circuit conditions. Line overvoltage provides extended line fault and surge withstand, output overvoltage protects the supply should the load be disconnected and accurate hysteretic thermal shutdown ensures safe average PCB temperatures under all conditions.

In any LED luminaire the driver determines many of the performance attributes experienced by the end user including startup time, dimming, flicker and unit to unit consistency. For this design a focus was given to compatibility with as wide a range of dimmers and as large of a dimming range as possible, at both 115 VAC and 230 VAC. However simplification of the design is possible for both single input voltage operation, no dimming or operation with a limited range of (higher quality) dimmers.

This document contains the LED driver specification, schematic, PCB diagram, bill of materials, transformer documentation and typical performance characteristics.





2 Power Supply Specification

The table below represents the minimum acceptable performance of the design. Actual performance is listed in the results section.

Description	Symbol	Min	Typ	Max	Units	Comment
Input						
Voltage ^a	V_{IN}	90	115	265	VAC	2 Wire – no P.E.
Frequency	f_{LINE}	47	50/60	64	Hz	
Output						
Output Voltage	V_{OUT}	24	28	32	V	$V_{OUT} = 28$, $V_{IN} = 115$ VAC, 25°C
Output Current ^a	I_{OUT}	0.475	0.5	0.525	A	
Total Output Power						
Continuous Output Power	P_{OUT}		14		W	
Efficiency						
Full Load	η	80			%	Measured at P_{OUT} 25 °C
Environmental						
Conducted EMI		CISPR 15B / EN55015B				IEC 61000-4-5 , 200 A
Safety		Designed to meet IEC950 / UL1950 Class II				
Ring Wave (100 kHz)						
Differential Mode (L1-L2)			2.5		kV	
Common mode (L1/L2-PE)						
Power Factor		0.9				Measured at $V_{OUT(TYP)}$, $I_{OUT(TYP)}$ and 115/230 VAC
Harmonics ^c		EN 61000-3-2 Class D (C)				
Ambient Temperature ^b	T_{AMB}			60	°C	Free convection, sea level

Notes:

^a When configured for phase controlled (TRIAC) dimming, to give widest dimming range, the output current for a LinkSwitch-PH design intentionally varies with line voltage. Therefore the output current specification is defined at a single line voltage only. For this design a line voltage of 115 VAC was selected. At higher line voltages the output current will increase and reduce with lower line voltages. The typical output current variation is +20% for a +200% in line voltage. A single resistor value change can be used to center the nominal output current for a given nominal line voltage. See Table 1 for the feedback resistor value vs. nominal line voltage.

^b Maximum ambient temperature may be increased by adding a small heat sink to the LinkSwitch-PH device. For example a strip of aluminum the width of the board and the height of the existing electrolytic capacitors increases maximum allowable ambient to 70 °C for a device temperature of 100 °C. Higher device temperatures, up to 115 °C, are allowable providing a reduction in output current tolerance is acceptable.

^c For input power <25 W, Class C compliance is gained when Class D harmonic current levels are met.



The schematic diagram illustrates a 500 W, 28 V, 18 A, 100 kHz, Class D, full-bridge, zero-voltage-switching (ZVS) power converter. The input is 90-265 VAC, which is rectified by BR1 (2KBP06M, 600 V) and filtered by L1 (1000 μH) and L2 (1000 μH). The rectified output is connected to the LinkSwitch-III (U1, LNK406EG) via R12 (10 kΩ) and R13 (10 kΩ). The LinkSwitch-III is controlled by a feedback loop consisting of R14 (374 kΩ), R15 (374 kΩ), C12 (220 nF), and C11 (470 nF). The LinkSwitch-III is connected to a full-bridge inverter consisting of D1 (DL4007), D2 (UF4007), D3 (UF4004), and D4 (RS1B). The inverter output is connected to a transformer (T1, RM64-LP) via R2 (2 MΩ), R3 (2 MΩ), and C3 (400 V). The transformer output is connected to a full-bridge rectifier (D5, D6) and filtered by C5 (22 μF) and C7 (50 V). The output is connected to a load (R11, 20 kΩ) and a feedback network (R9, R10, C6, C8). The output voltage is 28 V, 500 mA, 18 A, 100 kHz, Class D, full-bridge, zero-voltage-switching (ZVS) power converter.

Figure 3 – Schematic.

4 Circuit Description

The LinkSwitch-PH device is a controller and integrated 725 V power MOSFET intended for use in LED driver applications. The LinkSwitch-PH is configured for use in a single-stage continuous conduction mode flyback topology and provides a primary side regulated constant current output while maintaining high power factor from the AC input.

4.1 Input Filtering

Fuse F1 provides protection from component failure and RV1 provides a clamp to limit the maximum voltage during differential line surge events. A 275 VAC rated part was selected, being slightly above the maximum specified operating voltage of 265 VAC. Diode bridge BR1 rectifies the AC line voltage with capacitor C2 providing a low impedance path (decoupling) for the primary switching current. A low value of capacitance (sum of C1 and C2) is necessary to maintain a power factor of greater than 0.9.

EMI filtering is provided by inductors L1-L3, C1 and Y1 safety rated C8. Resistor R12 and R13 across L1 and L2 damp any resonances between the input inductors, capacitors and the AC line impedance which would ordinarily show up on the conducted EMI measurements.

4.2 LinkSwitch-PH Primary

One side of the transformer (T1) is connected to the DC bus and the other to the DRAIN (D) pin of the LinkSwitch-PH. During the on-time of the MOSFET current ramps through the primary storing energy which is then delivered to the output during the MOSFET off time. An RM8 core size was selected due to its small board area footprint. As the bobbin did not meet the 6.2 mm safety creepage distance required for 230 VAC operation, flying leads were used to terminate the secondary winding into the PC board.

To provide peak line voltage information to U1 the incoming rectified AC peak charges C3 via D1. This is then fed into the VOLTAGE MONITOR (V) pin of U1 as a current via R2 and R3. The resistor tolerance will cause V pin current variation unit to unit so 1% resistor types were selected to minimize this variation. The V pin current is also used by the device to set the line input over-voltage and under voltage protection thresholds. Undervoltage ensures a defined turn on voltage threshold unit to unit and overvoltage extends the rectified line voltage withstand (during surges and line swells) to the 725 BV_{DSS} rating of the internal MOSFET. Resistor R1 provides a discharge path for C3 with a time constant much longer than that of the rectified AC to prevent the V pin current being modulated at the line frequency.

The V pin current and the FEEDBACK (FB) pin current are used internally to control the average output LED current. For phase angle dimming applications a 49.9 k Ω resistor is used on the R pin (R4) and 4 M Ω (R2+R3) on the V pin to provide a linear relationship between input voltage and the output current and maximizing the dim range. Resistor R4



also sets the internal line input brown-in, brown-out and input overvoltage protection thresholds.

During the MOSFET on-time, diode D2 and VR1 clamp the drain voltage to a safe level due to the effects of leakage inductance. Diode D3 is necessary to prevent reverse current from flowing through U1 while the voltage across C2 falls to below the reflected output voltage (V_{OR}).

Diode D5, C5, R7 and R8 generate a primary bias supply from an auxiliary winding on the transformer. Capacitor C4 provides local decoupling for the BYPASS (BP) pin of U1 which is the supply pin for the internal controller. During start-up C4 is charged to ~6 V from an internal high-voltage current source tied to the DRAIN pin. This allows the part to start switching at which point the operating supply current is provided from the bias supply via R5. Diode D4 isolates the BP pin from C5 to prevent the start-up time increasing due to charging of both C4 and C5.

The use of an external bias supply (via D4 and R5) is recommended to give the lowest device dissipation and highest efficiency however these components may be omitted if desired. This ability to be self powered provides improved phase angle dimming performance as the IC is able to maintain operation even when the input conduction phase angle is very small giving a low equivalent input voltage.

Capacitor C4 also selects the output power mode, 10 μ F was selected (reduced power mode) to minimize the device dissipation and minimize heat sinking requirements.

4.3 Feedback

The bias winding voltage is used to sense the output voltage indirectly, eliminating secondary side feedback components. The voltage on the bias winding is proportional to the output voltage (set by the turns ratio between the bias and secondary windings). Resistor R6 converts the bias voltage into a current which is fed into the FB pin of U1. The internal engine within U1 combines the FB pin current, the V pin current, and drain current information to provide a constant output current over a 2:1 output voltage range whilst maintaining high input power factor.

To limit the output voltage at no-load an output overvoltage clamp is set by D6, C7, R10, VR2, C6, Q2 and R9. Should the output load be disconnected then the bias voltage will increase until VR2 conducts, turning on Q2 and reducing the current into the FB pin. When this current drops below 20 μ A the part enters auto-restart and switching is disabled for 800 ms allowing time for the output (and bias) voltages to fall.



4.4 Output Rectification

The transformer secondary winding is rectified by D7 and filtered by C9 and C10. An ultrafast diode was selected for low cost and the combined value of C9 and C10 was selected to give an LED ripple current equal to 40% of the mean value. For designs where lower ripple is desirable the output capacitance value can be increased. A small pre-load is provided by R11 which limits the output voltage under no-load conditions.

4.5 TRIAC Phase Dimming Control Compatibility

The requirement to provide output dimming with low cost, TRIAC based, leading edge phase dimmers introduced a number of trade offs in the design.

Due to the much lower power consumed by LED based lighting the current drawn by the overall lamp is below the holding current of the TRIAC within the dimmer. This causes undesirable behaviors such as limited dim range and/or flickering as the TRIAC fires inconsistently. The relatively large impedance the LED lamp presents to the line allows significant ringing to occur due to the inrush current charging the input capacitance when the TRIAC turns on. This too can cause similar undesirable behavior as the ringing may cause the TRIAC current to fall to zero and turn off.

To overcome these issues two circuits, the Active Damper and Passive Bleeder were incorporated. The drawback of these circuits is increased dissipation and therefore reduced efficiency of the supply. For non-dimming application these components can simply be omitted.

The Active Damper consists of components R14, R15, Q1, and C11 in conjunction with R16. This circuit limits the inrush current that flows to charge C2 when the TRIAC turns on by placing R16 in series for the first 1 ms of the conduction period. After approximately 1 ms, Q1 turns on and shorts R16. This keeps the power dissipation on R16 low and allows a larger value during current limiting. Resistor R14, R15 and C11 provide the 1 ms delay after the TRIAC conducts. The SCR selected for Q1 is a low current, low cost device in a TO-92 package.

The Passive Bleeder circuit is comprised of C12 and R17. This keeps the input current above the TRIAC holding current while the input current corresponding to the driver increases during each AC half-cycle preventing the TRIAC from oscillating on and off at the start of each conduction angle period.

This arrangement provided flicker-free dimming operation with all the phase angle dimmers tested including units from Europe, China, Korea and both leading and lagging edge types.



5 PCB Layout

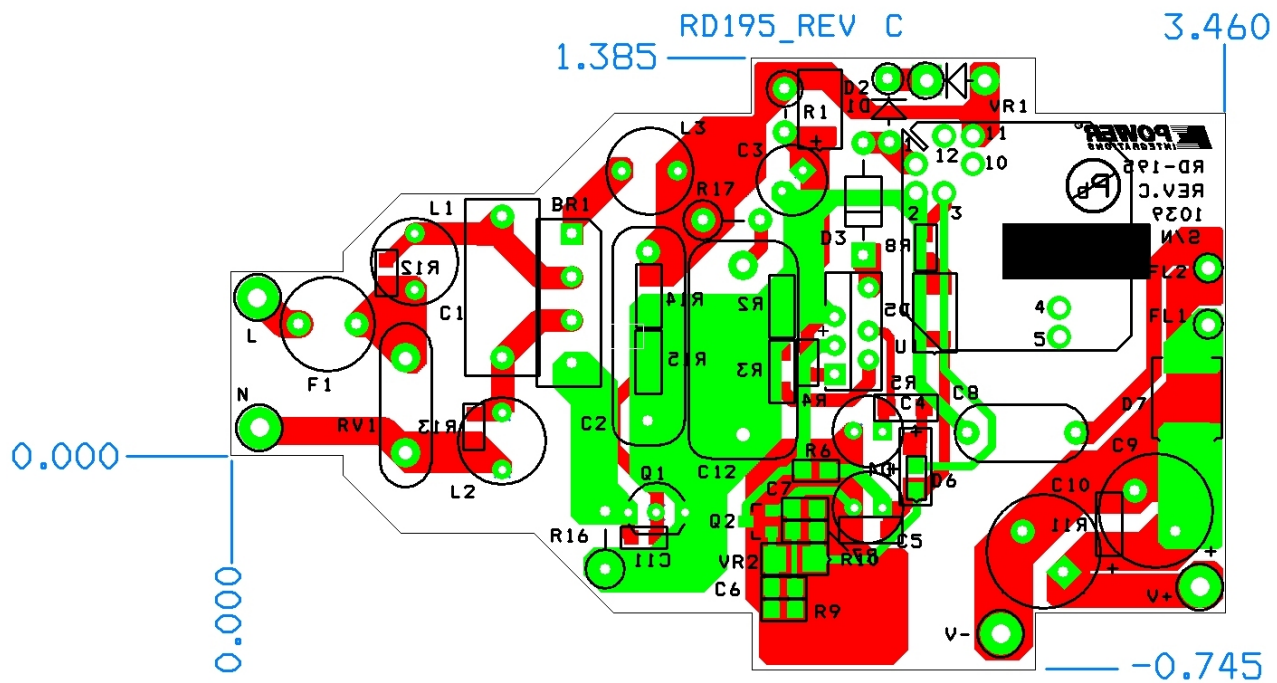


Figure 4 – Printed Circuit Layout (Dimensions in Inches).



6 Bill of Material

6.1 Electrical

Item	Qty	Ref Des	Description	Mfg Part Number	Mfg
1	1	BR1	600 V, 2 A, Bridge Rectifier, Glass Passivated	2KBP06M-E4/51	Vishay
2	1	C1	47 nF, 275 VAC, Film, X2	ECQU2A473ML	Panasonic
3	1	C2	100 nF, 630 V, Film	ECQ-E6104KF	Panasonic
4	1	C3	1 μ F, 400 V, Electrolytic, (6.3 x 11)	EKMG401ELL1R0MF11D	United Chemi-Con
5	1	C4	10 μ F, 16 V, Electrolytic, Gen. Purpose, (5 x 11)	EKMG160ELL100ME11D	United Chemi-Con
6	1	C5	22 μ F, 50 V, Electrolytic, Low ESR, 900 m Ω , (5 x 11.5)	ELXZ500ELL220MEB5D	Nippon Chemi-Con
7	1	C6	100 nF, 50 V, Ceramic, X7R, 0805	ECJ-2YB1H104K	Panasonic
8	1	C7	1 μ F, 50 V, Ceramic, X7R, 0805	0805D105KAT2A	AVX
9	1	C8	2.2 nF, Ceramic, Y1	440LD22-R	Vishay
10	2	C9, C10	330 μ F, 50 V, Electrolytic, Very Low ESR, 28 m Ω , (10 x 25)	EKZE500ELL331MJ25S	Nippon Chemi-Con
11	1	C11	470 nF, 50 V, Ceramic, X7R, 0805	GRM21BR71H474KA88L	Murata
12	1	C12	220 nF, 630 V, Film	ECQ-E6224KF	Panasonic
13	1	D1	1000 V, 1 A, Rectifier, Glass Passivated, DO-213AA (MELF)	DL4007-13-F	Diodes, Inc
14	1	D2	1000 V, 1 A, Ultrafast Recovery, 75 ns, DO-41	UF4007-E3	Vishay
15	1	D3	400 V, 1 A, Ultrafast Recovery, 50 ns, DO-41	UF4004-E3	Vishay
16	1	D4	100 V, 1 A, Fast Recovery, 150 ns, SMA	RS1B-13-F	Diodes, Inc
17	1	D5	400V, 1 A, Rectifier, Fast Recovery, MELF (DL-41)	DL4936-13-F	Diodes, Inc
18	1	D6	250 V, 0.2 A, Fast Switching, 50 ns, SOD-323	BAV21WS-7-F	Diodes, Inc
19	1	D7	100 V, 3 A, Ultrafast Recovery, 25 ns, SMC	ES3D-13-F	Diodes, Inc
20	1	F1	3.15 A, 250 V, Slow, TR5	37213150411	Wickman
22	3	L1, L2, L3	1000 μ H, 0.3 A	RLB0914-102KL	Bourns
22	1	Q1	SCR, 600 V, 1.25 A, TO-92	X0202MA 2BL2	ST Micro
23	1	Q2	NPN, Small Signal BJT, 40 V, 0.2 A, SOT-23	MMBT3904LT1G	On Semir
24	1	R1	510 k Ω , 5%, 1/2 W, Carbon Film	CFR-50JB-510K	Yageo
25	2	R2, R3	2.00 M Ω , 1%, 1/4 W, Thick Film, 1206	ERJ-8ENF2004V	Panasonic
26	1	R4	49.9 k Ω , 1%, 1/8 W, Thick Film, 0805	ERJ-6ENF4992V	Panasonic
27	1	R5	3 k Ω , 5%, 1/8 W, Thick Film, 0805	ERJ-6GEYJ302V	Panasonic
28	1	R6	150 k Ω , 1%, 1/8 W, Thick Film, 0805	ERJ-6ENF1503V	Panasonic
29	1	R7	10 k Ω , 5%, 1/4 W, Thick Film, 1206	ERJ-8GEYJ103V	Panasonic
30	1	R8	150 Ω , 5%, 1/8 W, Thick Film, 0805	ERJ-6GEYJ151V	Panasonic
31	1	R9	1 k Ω , 5%, 1/8 W, Thick Film, 0805	ERJ-6GEYJ102V	Panasonic
32	3	R10, R12, R13	10 k Ω , 5%, 1/8 W, Thick Film, 0805	ERJ-6GEYJ103V	Panasonic
33	1	R11	20 k Ω , 5%, 1/4 W, Thick Film, 1206	ERJ-8GEYJ203V	Panasonic
34	1	R14, R15	374 k Ω , 1%, 1/4 W, Thick Film, 1206	ERJ-8ENF3743V	Panasonic
35	1	R16	130 Ω , 5%, 2 W, Metal Oxide	RSF200JB-130R	Yageo
36	1	R17	510 Ω , 5%, 2 W, Metal Oxide	RSF200JB-510R	Yageo
37	1	RV1	275 V, 80J, 10 mm, RADIAL	ERZ-V10D431	Panasonic



38	1	T1	Bobbin, RM8 Low Profile, Vertical, 12 pins Custom Transformer	B65812-P1010-D1 SNX-R1523	Epcos Santronics USA
39	1	U1	LinkSwitch, eSIP	LNK406EG	Power Integrations
40	1	VR1	200 V, 5 W, 5%, TVS, DO204AC (DO-15)	P6KE200ARLG	On Semi
41	1	VR2	39 V, 5%, 500 mW, DO-213AA (MELF)	ZMM5259B-7	Diodes, Inc

6.2 Mechanical

Item	Qty	Ref Des	Description	Mfg Part Number	Mfg
42	1	L	Test Point, WHT, THRU-HOLE MOUNT	5012	Keystone
43	1	V+	Test Point, RED, THRU-HOLE MOUNT	5010	Keystone
44	1	V-	Test Point, BLK, THRU-HOLE MOUNT	5011	Keystone
45	1	N	Test Point, BLK, THRU-HOLE MOUNT	5011	Keystone
46	1	FL1	PCB Terminal Hole, #22 AWG	N/A	N/A
47	1	FL2	PCB Terminal Hole, #22 AWG	N/A	N/A



7 Transformer Specification

7.1 Electrical Diagram

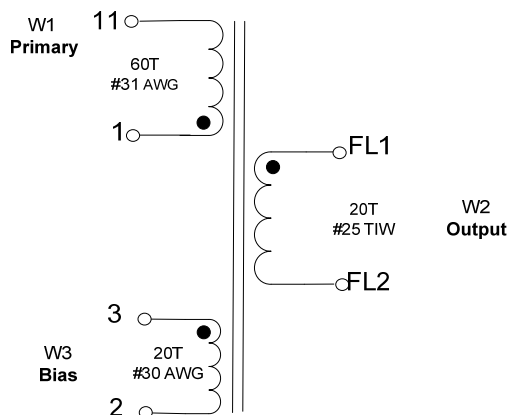


Figure 5 – Transformer Electrical Diagram.

7.2 Electrical Specifications

Electrical Strength	1 second, 60 Hz, from pins 1, 2, 3, 11 to FL1, FL2	3000 VAC
Primary Inductance	Pins 1-11, all other windings open, measured at 100 kHz, 0.4 VRMS	1150 μ H, $\pm 20\%$
Resonant Frequency	Pins 1-11, all other windings open	750 kHz (Min.)
Primary Leakage Inductance	Pins 1-11, with FL1-FL2 shorted, measured at 100 kHz, 0.4 VRMS	20 μ H (Max.)

7.3 Materials

Item	Description
[1]	Core: RM8/I, 3F3, ALG = 319 nH/n ²
[2]	Bobbin: 12 pin vertical, CSV-RM8-1S-12P, Philips or equivalent with mounting clip, CLI/P-RM8
[3]	Tape: Polyester film, 3M 1350F-1 or equivalent, 9 mm wide
[4]	Wire: Magnet, #31 AWG, solderable double coated
[5]	Wire: Magnet, #30 AWG, solderable double coated
[6]	Wire: Triple Insulated, Furukawa TEX-E or Equivalent, #25 TIW
[7]	Transformer Varnish: Dolph BC-359 or equivalent

7.4 Transformer Build Diagram

Pins Side

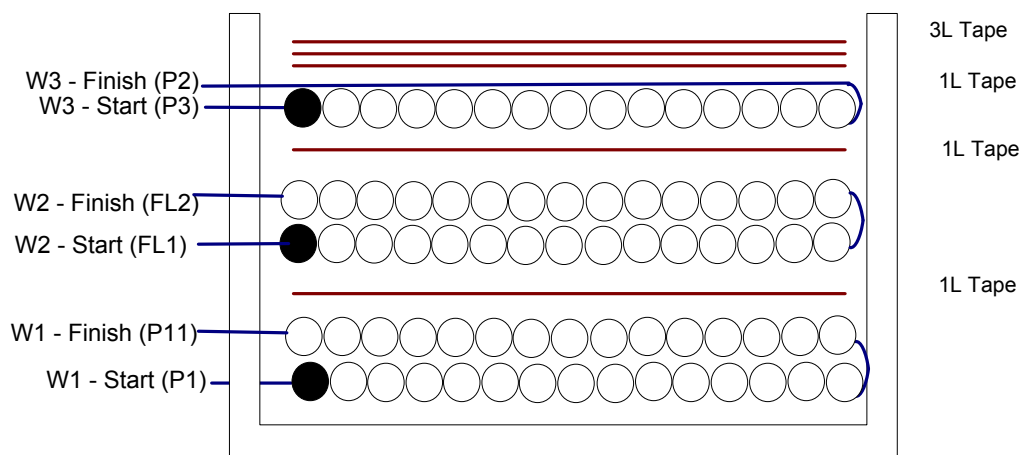


Figure 6 – Transformer Build Diagram.

7.5 Transformer Construction

Bobbin Preparation	Place the bobbin item [2] on the mandrel such that pin side on the left side. Winding direction is the clockwise direction.
WD 1 (Primary)	Starting at pin 1, wind 60 turns of wire item [4] in two layers. Finish at pin 11.
Insulation	Apply one layer of tape item [3].
WD 2 (Secondary)	Leave about 1" of wire item [6], use small tape to mark as FL1, enter into slot of secondary side of bobbin, wind 20 turns in two layers. At the last turn exit the same slot, leave about 1", and mark as FL2.
Insulation	Apply one layer of tape item [3].
WD 3 (Bias)	Starting at pin 3, wind 20 turns of wire item [5], spreading the wire, finish at pin 2.
Finish Wrap	Apply three layers of tape item [3] for finish wrap.
Final Assembly	Cut FL1 and FL2 to 0.75". Grind core to get 1.15 mH inductance value. Assemble and secure core halves. Dip impregnate using varnish item [7].



8 Transformer Design Spreadsheet

ACDC_LinkSwitch-PH_042910; Rev.1.0; Copyright Power Integrations 2010	INPUT	INFO	OUTPUT	UNIT	LinkSwitch-PH_042910: Flyback Transformer Design Spreadsheet
ENTER APPLICATION VARIABLES					
Dimming required	YES	<i>Info</i>	YES		!!! Info. When configured for dimming, best output current line regulation is achieved over a single input voltage range.
VACMIN			90	V	Minimum AC Input Voltage
VACMAX	265		265	V	Maximum AC input voltage
fL			50	Hz	AC Mains Frequency
VO	28.00			V	Typical output voltage of LED string at full load
VO_MAX			30.80	V	Maximum expected LED string Voltage.
VO_MIN			25.20	V	Minimum expected LED string Voltage.
V_OVP			33.88	V	Over-voltage protection setpoint
IO	0.50				Typical full load LED current
PO			14.0	W	Output Power
n			0.8		Estimated efficiency of operation
VB	28		28	V	Bias Voltage
ENTER LinkSwitch-PH VARIABLES					
LinkSwitch-PH	LNK406			Universal	115 Doubled/230V
Chosen Device		LNK406	Power Out	22.5W	22.5W
Current Limit Mode	RED		RED		Select "RED" for reduced Current Limit mode or "FULL" for Full current limit mode
ILIMITMIN			1.19	A	Minimum current limit
ILIMITMAX			1.36	A	Maximum current limit
fS			66000	Hz	Switching Frequency
fSmin			62000	Hz	Minimum Switching Frequency
fSmax			70000	Hz	Maximum Switching Frequency
IV			39.9	uA	V pin current
RV			4	M-ohms	Upper V pin resistor
RV2			1E+12	M-ohms	Lower V pin resistor
IFB			158.8	uA	FB pin current (85 uA < IFB < 210 uA)
RFB1			157.5	k-ohms	FB pin resistor
VDS			10	V	LinkSwitch-PH on-state Drain to Source Voltage
VD	0.50			V	Output Winding Diode Forward Voltage Drop (0.5 V for Schottky and 0.8 V for PN diode)
VDB	0.70			V	Bias Winding Diode Forward Voltage Drop
Key Design Parameters					
KP	0.87		0.87		Ripple to Peak Current Ratio (For PF > 0.9, 0.4 < KP < 0.9)
LP			1150	uH	Primary Inductance
VOR	85.00		85	V	Reflected Output Voltage.
Expected IO (average)			0.51	A	Expected Average Output Current



KP_VACMAX			1.11		Expected ripple current ratio at VACMAX
TON_MIN			1.86	us	Minimum on time at maximum AC input voltage
ENTER TRANSFORMER CORE/CONSTRUCTION VARIABLES					
Core Type	RM8/I		RM8/I		
Bobbin		<i>RM8/I_BOBBIN</i>		<i>P/N:</i>	*
AE			0.63	cm^2	Core Effective Cross Sectional Area
LE			3.84	cm	Core Effective Path Length
AL			3000	nH/T^2	Ungapped Core Effective Inductance
BW			10	mm	Bobbin Physical Winding Width
M			0	mm	Safety Margin Width (Half the Primary to Secondary Creepage Distance)
L	2.00		2		Number of Primary Layers
NS	20		20		Number of Secondary Turns
DC INPUT VOLTAGE PARAMETERS					
VMIN			127	V	Peak input voltage at VACMIN
VMAX			375	V	Peak input voltage at VACMAX
CURRENT WAVEFORM SHAPE PARAMETERS					
DMAX			0.42		Minimum duty cycle at peak of VACMIN
Iavg			0.51	A	Average Primary Current
IP			0.95	A	Peak Primary Current (calculated at minimum input voltage VACMIN)
IRMS			0.31	A	Primary RMS Current (calculated at minimum input voltage VACMIN)
TRANSFORMER PRIMARY DESIGN PARAMETERS					
LP			1150	uH	Primary Inductance
NP			60		Primary Winding Number of Turns
NB			20		Bias Winding Number of Turns
ALG			323	nH/T^2	Gapped Core Effective Inductance
BM			2897	Gauss	Maximum Flux Density at PO, VMIN (BM<3100)
BP			3506	Gauss	Peak Flux Density (BP<3700)
BAC			1267	Gauss	AC Flux Density for Core Loss Curves (0.5 X Peak to Peak)
ur			1455		Relative Permeability of Ungapped Core
LG			0.22	mm	Gap Length (Lg > 0.1 mm)
BWE			20	mm	Effective Bobbin Width
OD			0.34	mm	Maximum Primary Wire Diameter including insulation
INS			0.06	mm	Estimated Total Insulation Thickness (= 2 * film thickness)
DIA			0.28	mm	Bare conductor diameter
AWG			30	AWG	Primary Wire Gauge (Rounded to next smaller standard AWG value)
CM			102	Cmils	Bare conductor effective area in circular mils
CMA			330	Cmils/Amp	Primary Winding Current Capacity (200 < CMA < 600)
TRANSFORMER SECONDARY DESIGN PARAMETERS (SINGLE OUTPUT EQUIVALENT)					
Lumped parameters					
ISP			2.82	A	Peak Secondary Current
ISRMS			1.01	A	Secondary RMS Current
IRIPPLE			0.88	A	Output Capacitor RMS Ripple Current



CMS			203	Cmils	Secondary Bare Conductor minimum circular mils
AWGS			27	AWG	Secondary Wire Gauge (Rounded up to next larger standard AWG value)
DIAS			0.36	mm	Secondary Minimum Bare Conductor Diameter
ODS			0.50	mm	Secondary Maximum Outside Diameter for Triple Insulated Wire
VOLTAGE STRESS PARAMETERS					
VDRAIN			553	V	Estimated Maximum Drain Voltage assuming maximum LED string voltage (Includes Effect of Leakage Inductance)
PIVS			160	V	Output Rectifier Maximum Peak Inverse Voltage (calculated at VOVP, excludes leakage inductance spike)
PIVB			160	V	Bias Rectifier Maximum Peak Inverse Voltage (calculated at VOVP, excludes leakage inductance spike)
FINE TUNING (Enter measured values from prototype)					
V pin Resistor Fine Tuning					
RV1			4.00	M-ohms	Upper V Pin Resistor Value
RV2			1E+12	M-ohms	Lower V Pin Resistor Value
VAC1			115.0	V	Test Input Voltage Condition1
VAC2			230.0	V	Test Input Voltage Condition2
IO_VAC1			0.50	A	Measured Output Current at VAC1
IO_VAC2			0.50	A	Measured Output Current at VAC2
RV1 (new)			4.00	M-ohms	New RV1
RV2 (new)			20911.63	M-ohms	New RV2
V_OV			319.6	V	Typical AC input voltage at which OV shutdown will be triggered
V_UV			66.3	V	Typical AC input voltage beyond which power supply can startup
FB pin resistor Fine Tuning					
RFB1			157	k-ohms	Upper FB Pin Resistor Value
RFB2			1E+12	k-ohms	Lower FB Pin Resistor Value
VB1			25.2	V	Test Bias Voltage Condition1
VB2			30.8	V	Test Bias Voltage Condition2
IO1			0.50	A	Measured Output Current at Vb1
IO2			0.50	A	Measured Output Current at Vb2
RFB1 (new)			157.5	k-ohms	New RFB1
RFB2(new)			1.00E+12	k-ohms	New RFB2



9 Performance Data

All measurements performed at room temperature

9.1 Power Efficiency

9.1.1 27 V

Hz	V _{IN} (VAC)	P _{IN} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	Efficiency (%)	PF
60	90	15	26.9	0.46	12.37	82	
60	100	15.4	26.9	0.48	12.91	84	
60	115	15.9	27	0.5	13.50	85	0.98
60	130	16.4	27	0.52	14.04	86	
Hz	V _{IN} (VAC)	P _{IN} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	Efficiency (%)	PF
50	195	18.3	27.2	0.58	15.78	86	
50	210	18.7	27.2	0.59	16.05	86	
50	230	19.3	27.2	0.61	16.59	86	0.93
50	245	19.6	27.3	0.62	16.93	86	
50	265	20.1	27.3	0.63	17.20	86	

9.1.2 24 V

Hz	V _{IN} (VAC)	P _{IN} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	Efficiency (%)	PF
60	90	13.1	23.6	0.46	10.86	83	
60	100	13.5	23.7	0.48	11.38	84	
60	115	13.9	23.8	0.5	11.90	86	0.98
60	130	14.4	23.8	0.52	12.38	86	
Hz	V _{IN} (VAC)	P _{IN} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	Efficiency (%)	PF
50	195	16.2	24	0.58	13.92	86	
50	210	16.6	24.1	0.59	14.22	86	
50	230	17.2	24.1	0.61	14.70	85	0.92
50	245	17.6	24.2	0.62	15.00	85	
50	265	18.1	24.23	0.64	15.51	86	



9.1.3 30 V

Hz	V _{IN} (VAC)	P _{IN} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	Efficiency (%)	PF
60	90	16.8	29.6	0.47	13.91	83	
60	100	17.2	29.7	0.49	14.55	85	
60	115	17.7	29.7	0.5	14.85	84	0.98
60	130	18.2	29.8	0.522	15.56	85	
Hz	V _{IN} (VAC)	P _{IN} (W)	V _{OUT} (V)	I _{OUT} (mA)	P _{OUT} (W)	Efficiency (%)	PF
50	195	20.2	30	0.58	17.40	86%	
50	210	20.6	30	0.59	17.70	86%	
50	230	21.2	30.1	0.61	18.36	87%	0.93
50	245	21.5	30.1	0.62	18.66	87%	
50	265	22.1	30.1	0.63	18.96	86%	

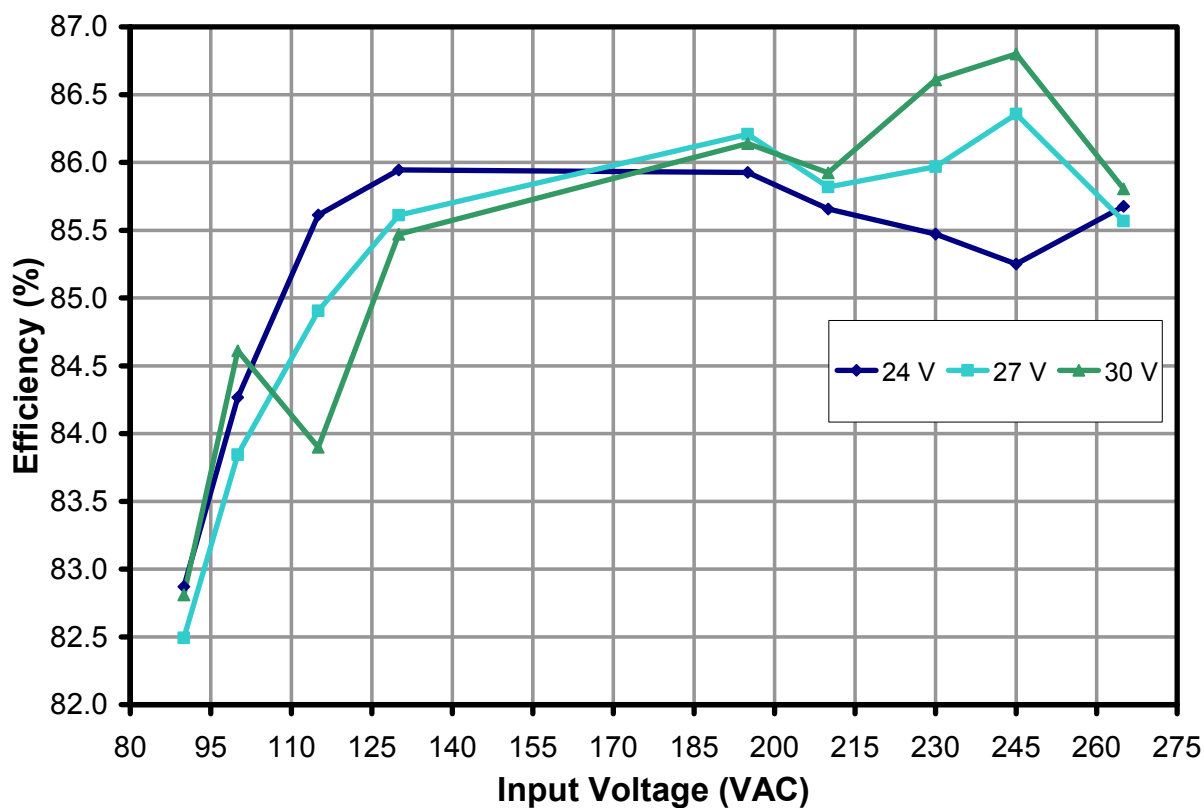


Figure 7– Efficiency vs. Input Voltage, Room Temperature.



9.2 Regulation

9.2.1 Output Voltage and Line

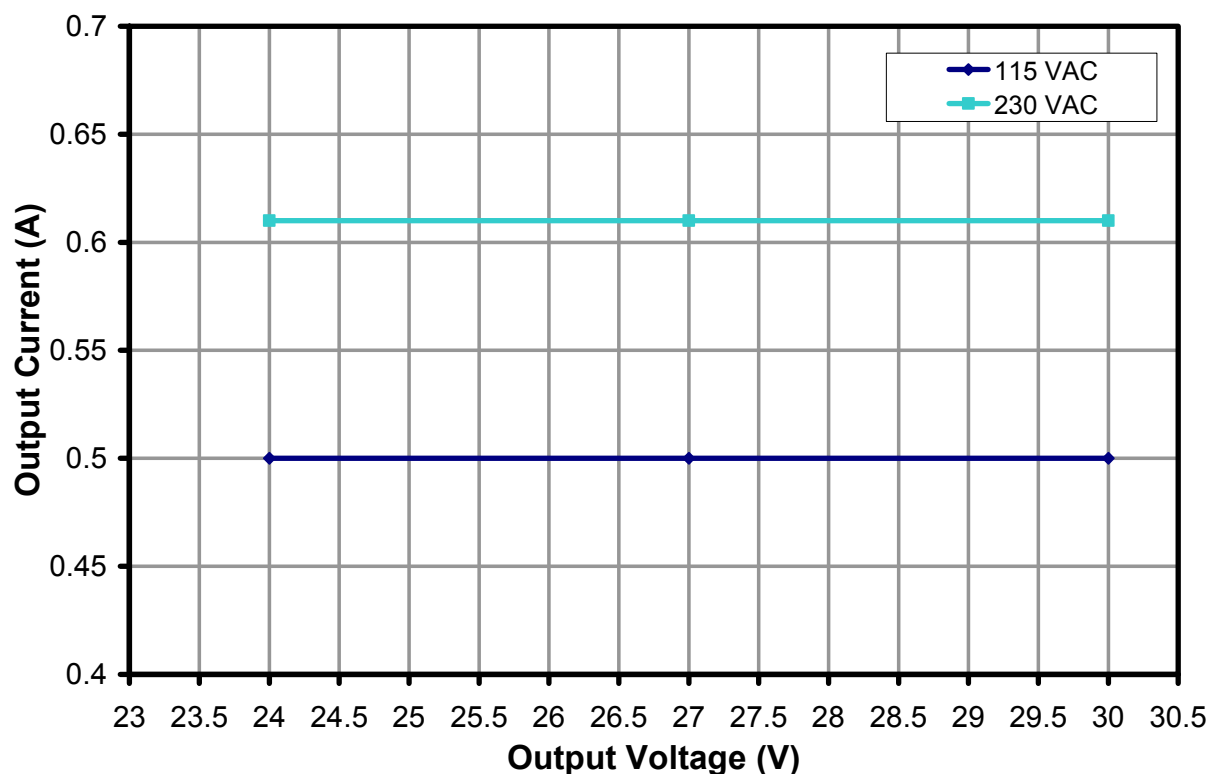


Figure 8 – Voltage and Line Regulation, Room Temperature.

The line regulation result shown above is typical for a design where the phase angle dimming mode of U1 is selected (to provide a very wide dimming range). For a given line voltage the output current can be centered by changing the value of the FEEDBACK resistor (R6). The table below shows the resistor values to adjust the mean output current at specific input voltages,

Line Voltage (VAC)	Value of R6 (kΩ)
100	147
115	150
230	178

Table 1 – Feedback Resistor Value to Center Output Current at Different Nominal Line Voltages.



9.2.2 Input Voltage and Output Current Regulation

Note: 24 V and 27 V data identical at low-line input, and 27 V and 30 V data identical at high-line input.

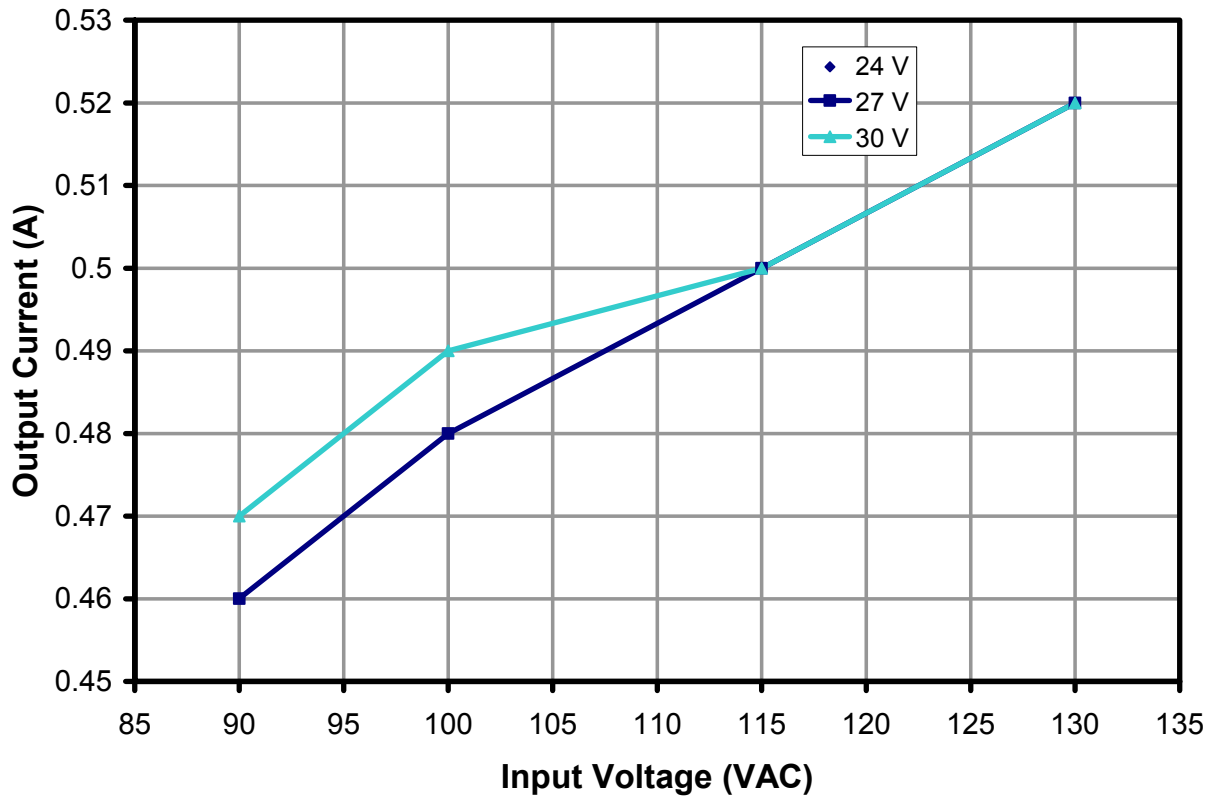


Figure 9 – Low Line Regulation, Room Temperature, Full Load.

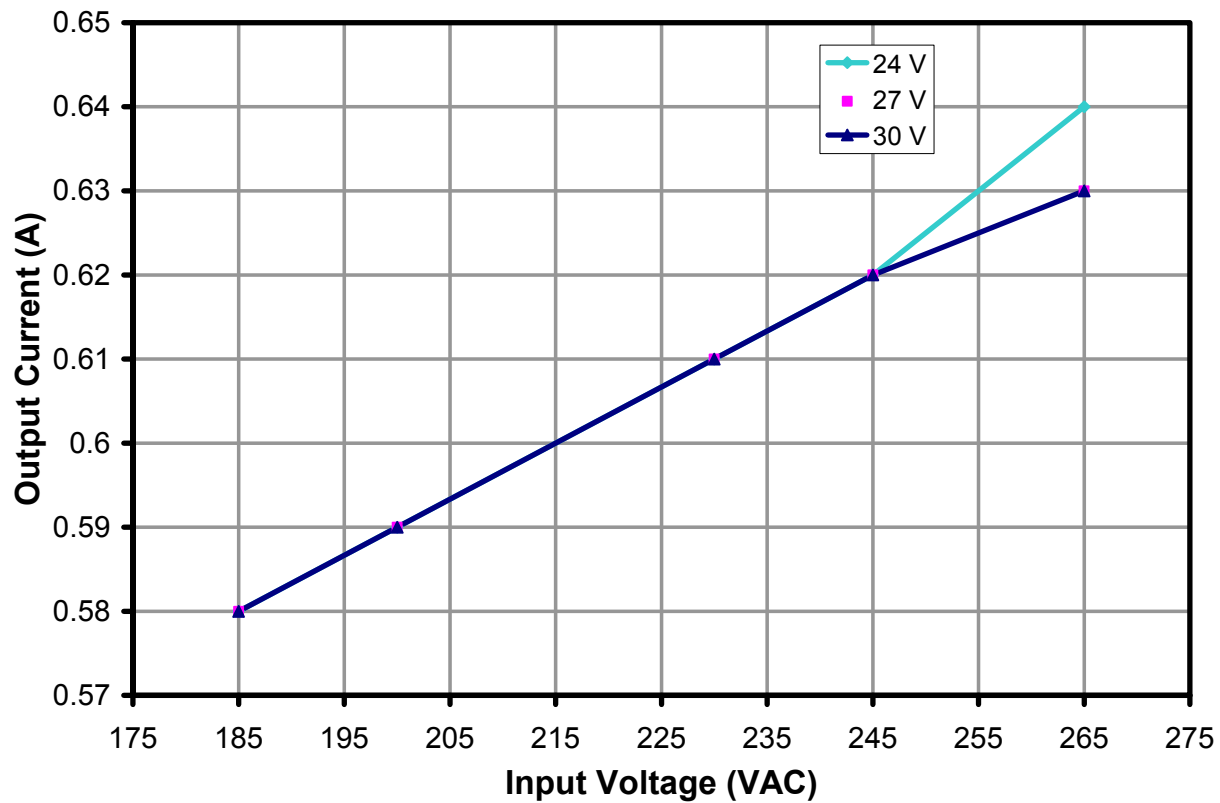


Figure 10 – High-Line Regulation, Room Temperature, Full Load.



10 Thermal Performance

Images captured after running for 30 minutes at room temperature (25 °C), full load. This indicates an operating temperature of 100 °C at 50 °C for the LinkSwitch-PH. The addition of a small heat sink (width of board) to the device reduces the operating temperature by ~25 °C.

10.1 $V_{IN} = 115 \text{ VAC}$ (U1: No Heat Sink)

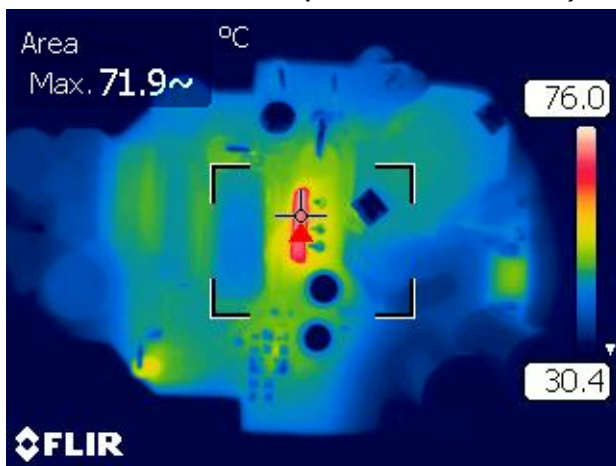


Figure 11 – Top Side.

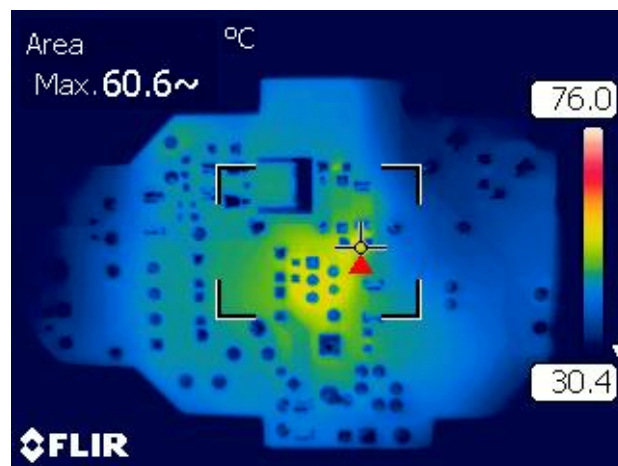


Figure 12 – Bottom Side.

10.2 $V_{IN} = 230 \text{ VAC}$ (U1: No Heat Sink)

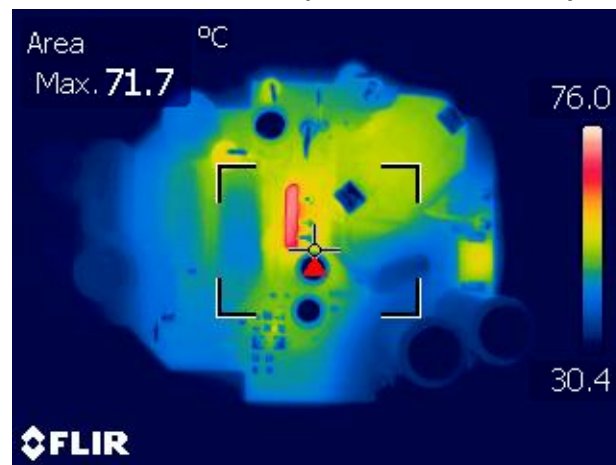


Figure 13 – Top Side.

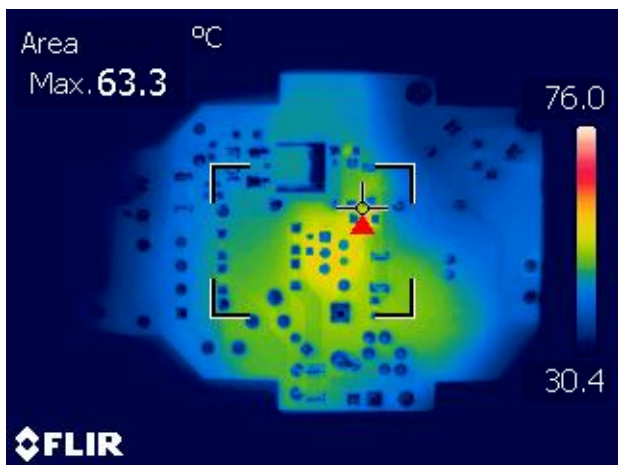


Figure 14 – Bottom Side.

11 Harmonic Data

Per IEC 61000-3-2 (2005) for Class C compliance for an active input power <25 W requires meeting Class D limits. Where Figures 15 and 16 show Class D limits these are intended to show the limits for Class C compliance (Class D limits).

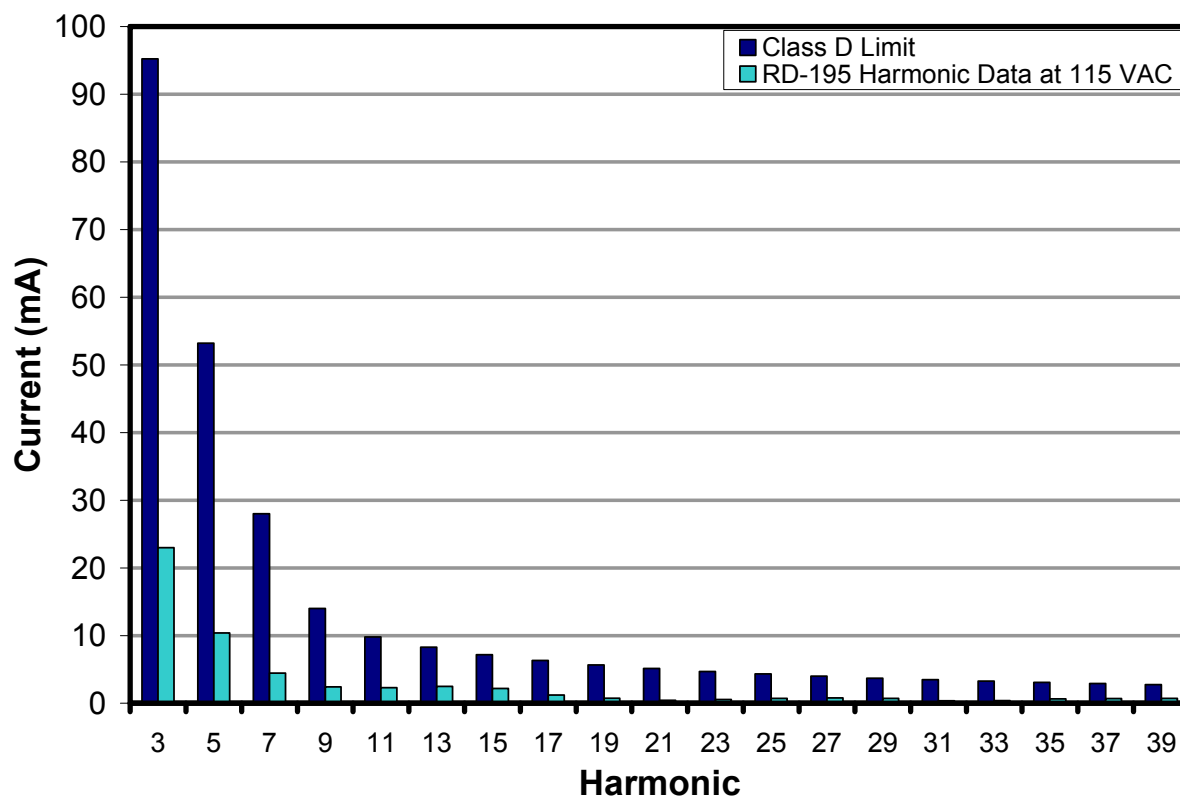


Figure 15 – 115 VAC Harmonic, Room Temperature, Full Load.



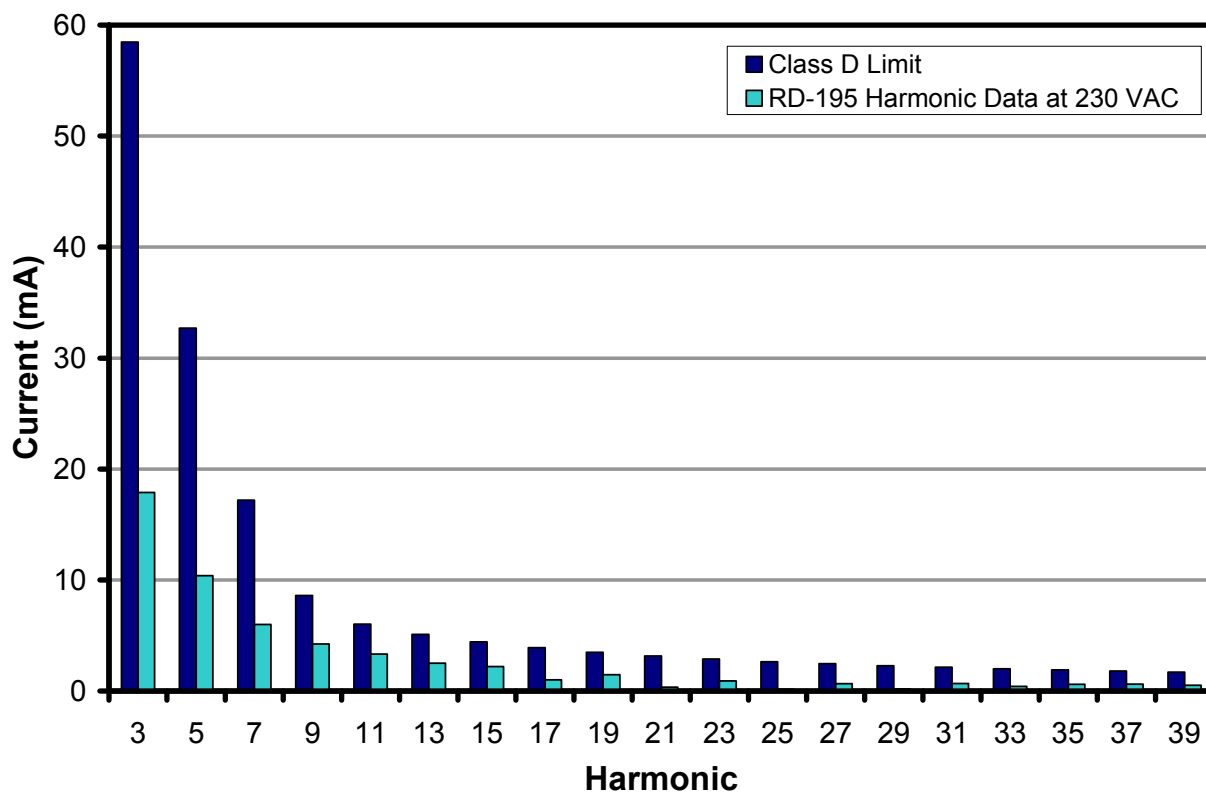


Figure 16 – 230 VAC Harmonic, Room Temperature, Full Load.

V _{IN} = 115 VAC		
THD (%)	Limit (%)	Margin (%)
21.0	33	12.0
V _{IN} = 230 VAC		
THD (%)	Limit (%)	Margin (%)
27.8	33	5.2



12 Waveforms

12.1 Input Line Voltage and Current

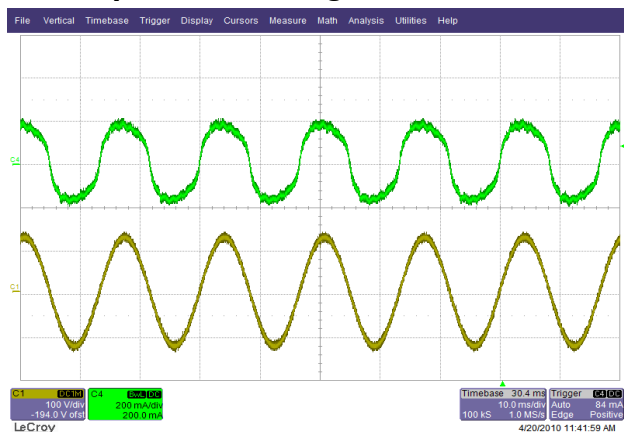


Figure 17 – 90 VAC, Full Load.
Upper: I_{IN} , 0.2 A / div.
Lower: V_{IN} , 100 V, 10 ms / div.

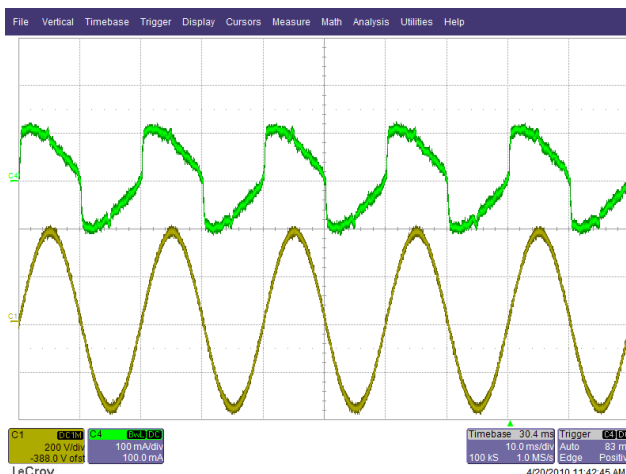


Figure 18 – 265 VAC, Full Load.
Upper: I_{IN} , 0.1 A / div.
Lower: V_{IN} , 200 V / div., 10 ms / div.

12.2 Drain Voltage and Current

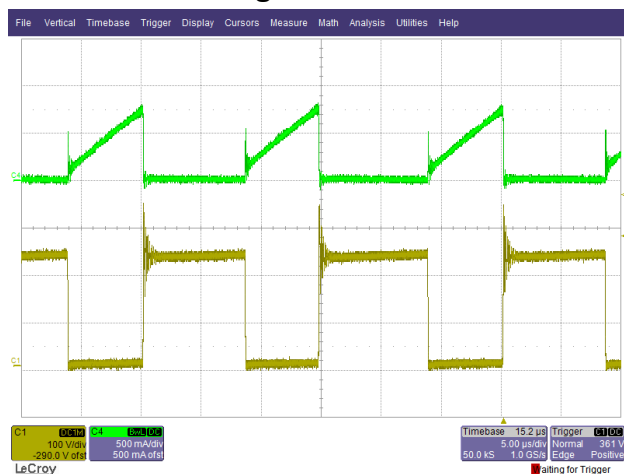


Figure 19 – 90 VAC, Full Load.
Upper: I_{DRAIN} , 0.5 A / div.
Lower: V_{DRAIN} , 100 V, 5 μ s / div.

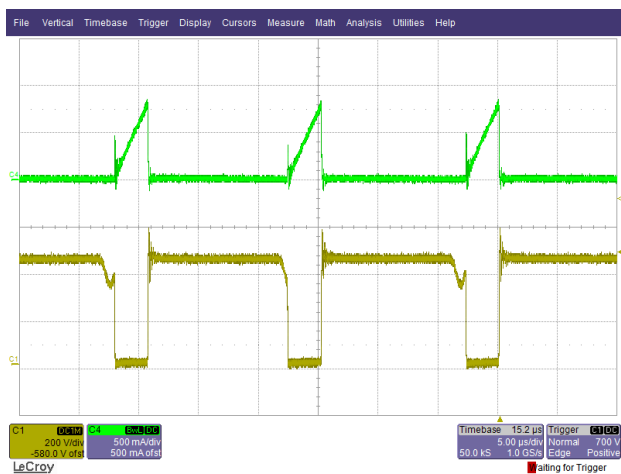


Figure 20 – 265 VAC, Full Load.
Upper: I_{DRAIN} , 0.5 A / div.
Lower: V_{DRAIN} , 200 V / div., 5 μ s / div.



12.3 Output Voltage and Ripple Current

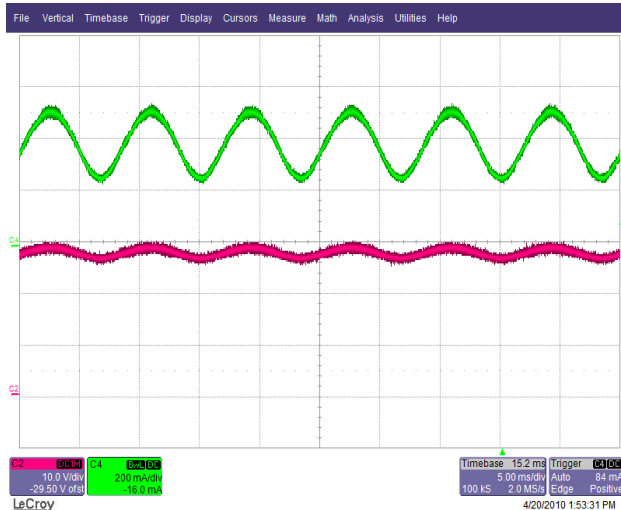


Figure 21 – 90 VAC, Full Load.
Upper: I_{RIPPLE} , 0.2 A / div.
Lower: V_{OUT} , 10 V, 5 ms / div.



Figure 22 – 265 VAC, Full Load.
Upper: I_{RIPPLE} , 0.2 A / div.
Lower: V_{OUT} , 10 V, 5 ms / div.

12.4 Output Voltage and Drain Current Start-up Profile

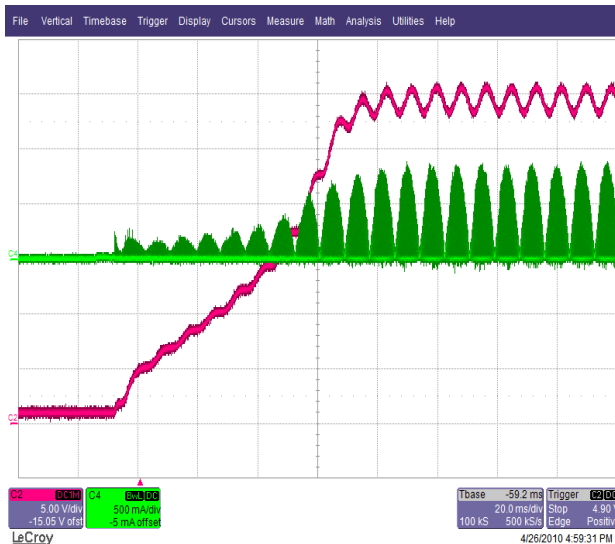


Figure 23 – 90 VAC, Full Load.
Upper: I_{DRAIN} , 0.5 A / div.
Lower: V_{OUT} , 5 V, 20 ms / div.



Figure 24 – 265 VAC, Full Load.
Upper: I_{RIPPLE} , 0.5 A / div.
Lower: V_{OUT} , 5 V, 10 ms / div.



12.5 Output Current and Drain Voltage During Shorted Output

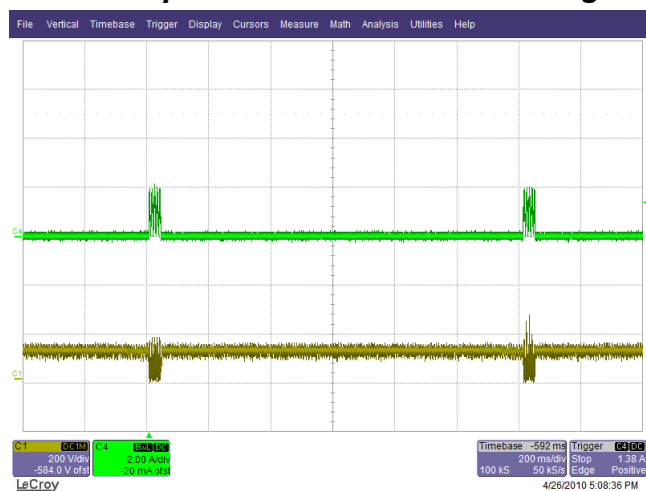


Figure 25 – 90 VAC, Full Load.
Upper: I_{OUT} , 2 A / div.
Lower: V_{DRAIN} , 200 V, 200 ms / div.

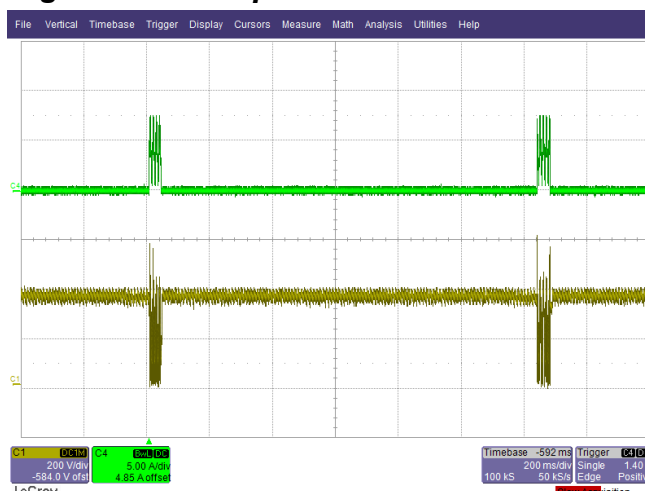


Figure 26 – 265 VAC, Full Load.
Upper: I_{OUT} , 5 A / div.
Lower: V_{OUT} , 200 V, 200 ms / div.

12.6 Open Load Output Voltage

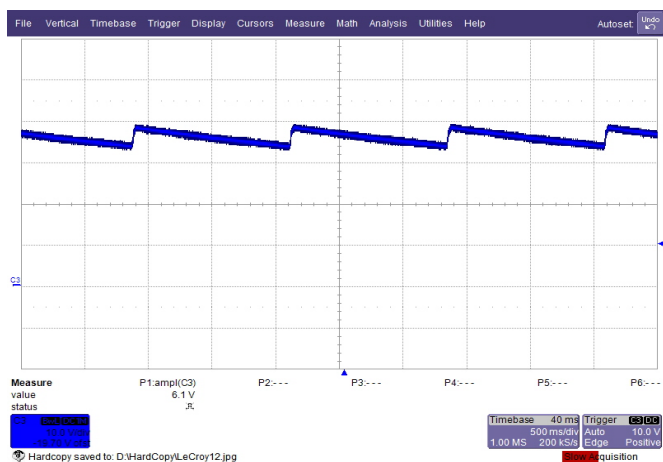


Figure 27 – Output Voltage: 115 VAC.
 V_{OUT} , 10 V / div., 500 ms / div.

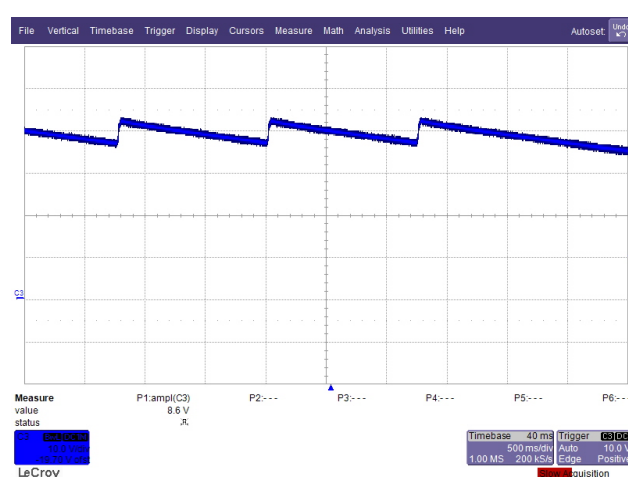


Figure 28 – Output Voltage: 230 VAC.
 V_{OUT} , 10 V / div., 500 ms / div.



13 Dimming

13.1 Input Phase vs. Output

Note: Due to operation of TRIAC based phase dimmers maximum conduction angle was limited to 165 °C.

115 VAC / 60 Hz Phase Angle (°)	I _{OUT} (mA)	230 VAC / 50 Hz Phase Angle (°)	I _{OUT} (mA)
167	485	167	580
98	250	95	310
67	130	59	140
46	67	36	60
39	37	27	32
15	3	11	7
9	1	7	4
7	0.5	5	3
0	0	5	1

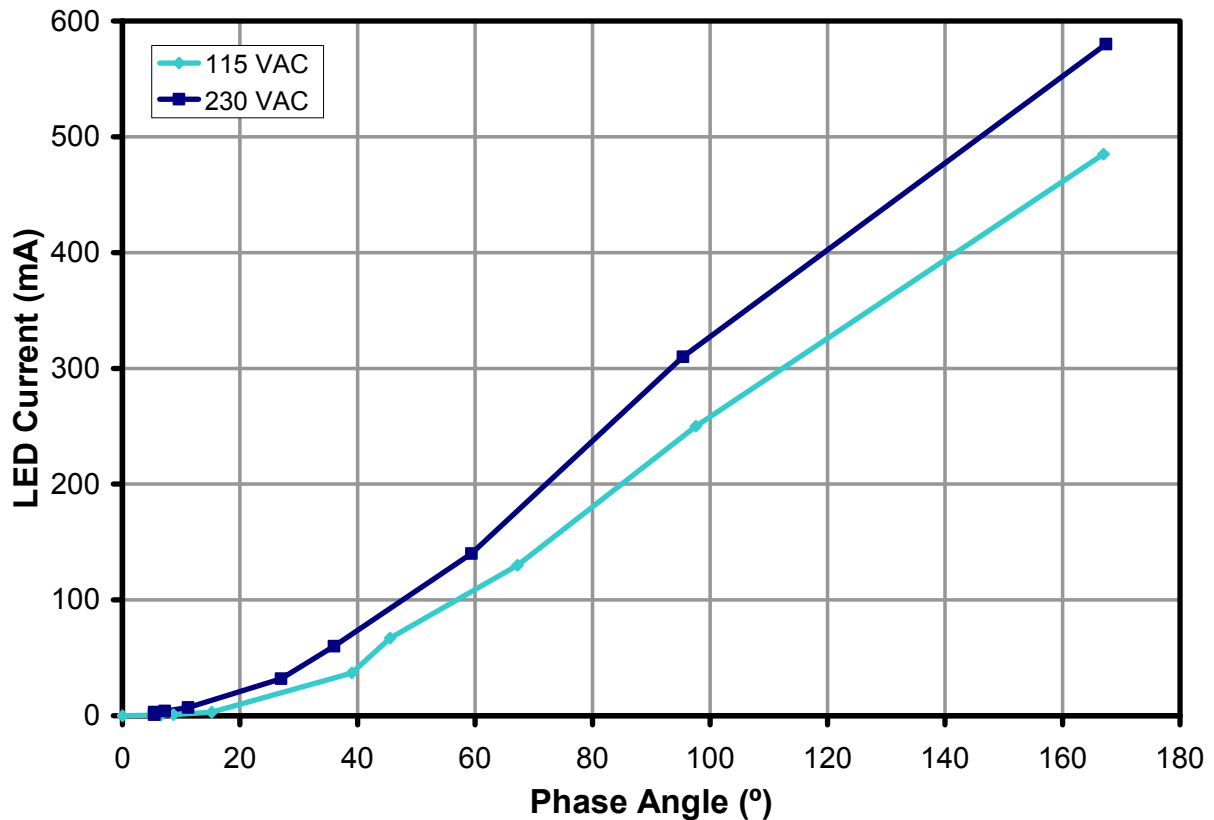


Figure 29 – Input Phase vs. Output Current.

13.2 Output Voltage and Input Current Waveforms

13.2.1 $V_{IN} = 115 \text{ VAC} / 60 \text{ Hz}$

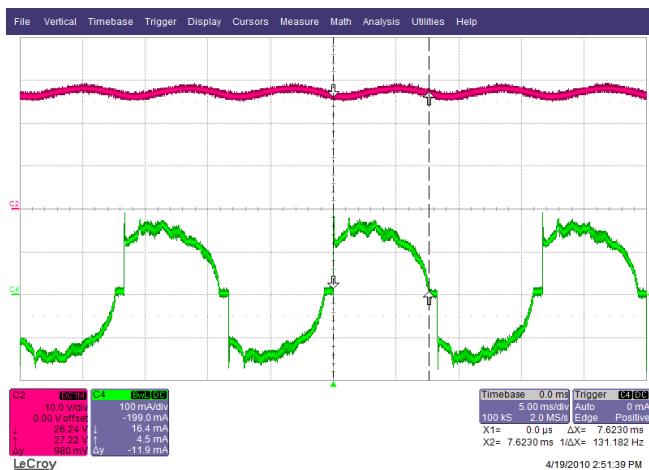


Figure 30 – 115 VAC, Full Phase.
Upper: V_{OUT} , 10 V / div.
Lower: I_{IN} , 0.1 A / div., 5 ms / div.

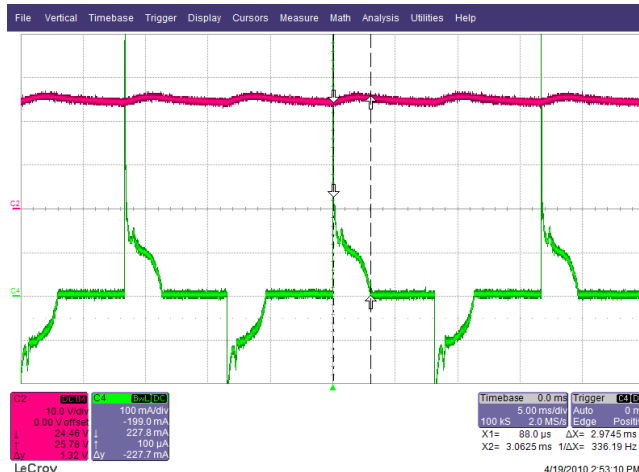


Figure 31 – 115 VAC, 65° Phase.
Upper: V_{OUT} , 10 V / div.
Lower: I_{IN} , 0.1 A / div., 5 ms / div.

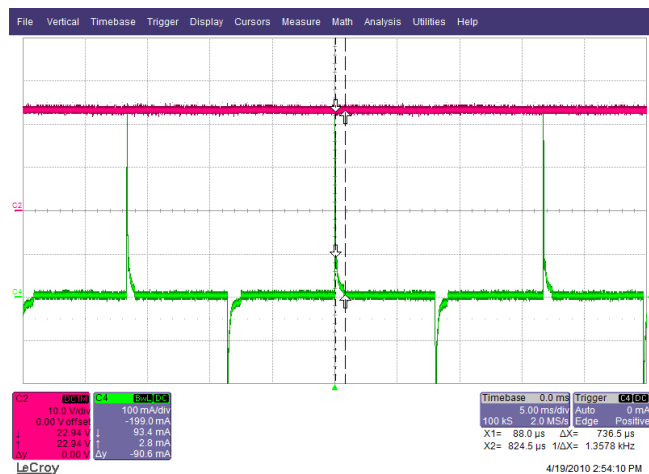


Figure 32 – 115 VAC, 16° Phase.
Upper: V_{OUT} , 10 V / div.
Lower: I_{IN} , 0.1 A / div., 5 ms / div.



Figure 33 – 115 VAC, 8° Phase.
Upper: V_{OUT} , 10 V / div.
Lower: I_{IN} , 0.1 A / div., 5 ms / div.



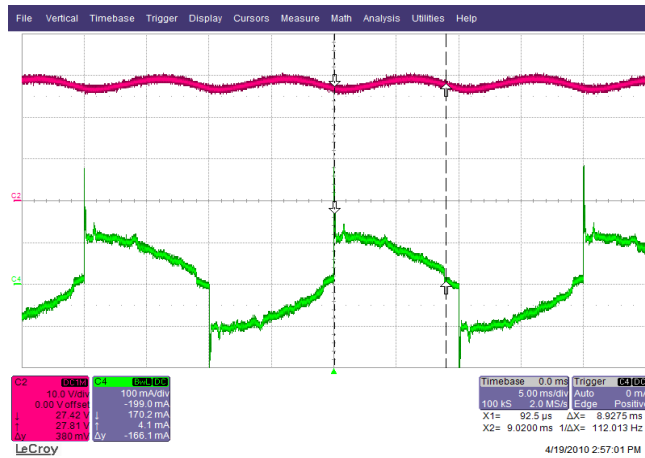
13.2.2 $V_{IN} = 230 \text{ VAC} / 50\text{Hz}$ 

Figure 34 – 230 VAC, Full Phase.
Upper: V_{OUT} , 10 V / div.
Lower: I_{IN} , 0.1 A / div., 5 ms / div.



Figure 35 – 230 VAC, 54° Phase.
Upper: V_{OUT} , 10 V / div.
Lower: I_{IN} , 0.1 A / div., 5 ms / div.



Figure 36 – 230 VAC, 6° Phase.
Upper: V_{OUT} , 10 V / div.
Lower: I_{IN} , 0.1 A / div., 5 ms / div.



Figure 37 – 230 VAC, 5° Phase.
Upper: V_{OUT} , 10 V / div.
Lower: I_{IN} , 0.1 A / div., 5 ms / div.



14 Line Surge

Differential and common input line 200 A ring wave testing was completed on a single test unit to IEC61000-4-5. Input voltage was set at 230 VAC / 60 Hz. Output was loaded at full load and operation was verified following each surge event.

Surge Level (V)	Input Voltage (VAC)	Injection Location	Injection Phase (°)	Test Result (Pass/Fail)
2500	230	L to N	90	Pass
2500	230	L to N	90	Pass
2500	230	L to PE	90	Pass
2500	230	L to PE	90	Pass
2500	230	N to PE	90	Pass
2500	230	N to PE	90	Pass

Unit passes under all test conditions.



15 Conducted EMI

Note: Blue results represents peak detector vs. quasi peak limit line. For actual margin to limit (quasi peak measurement vs. quasi peak limit) please refer to the table.

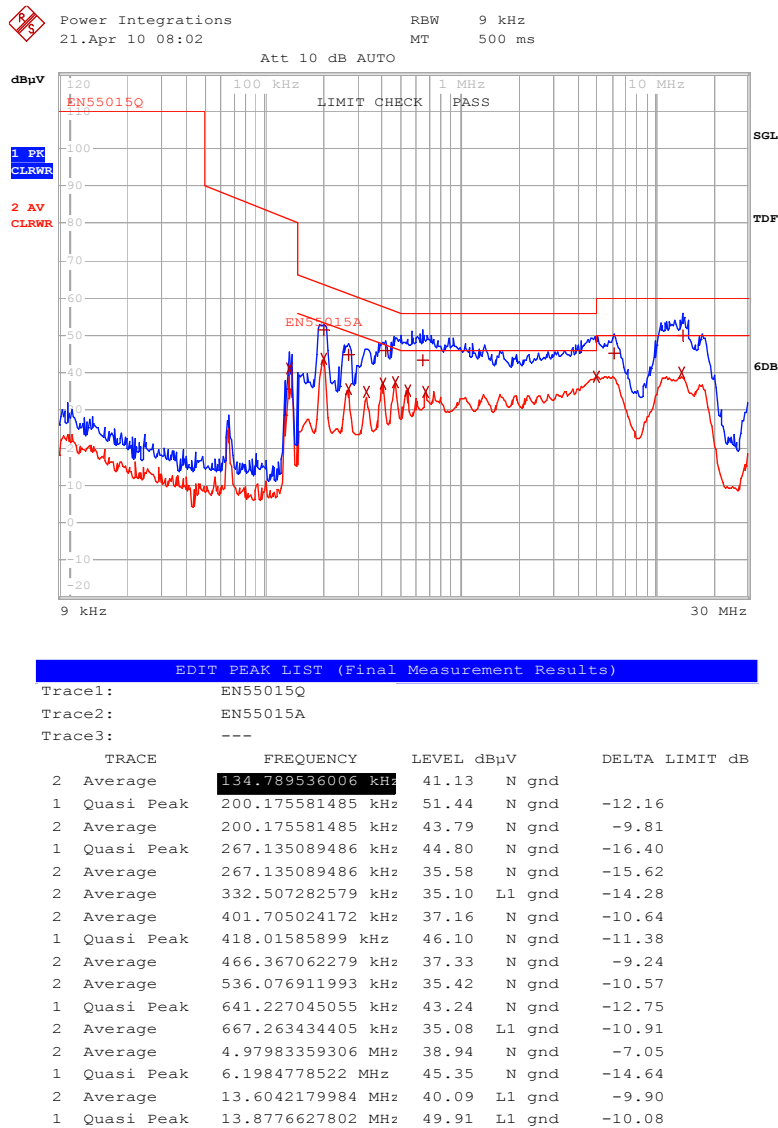


Figure 38 – Conducted EMI, Maximum Steady State Load, 115 VAC, 60 Hz, and EN55015 B Limits.



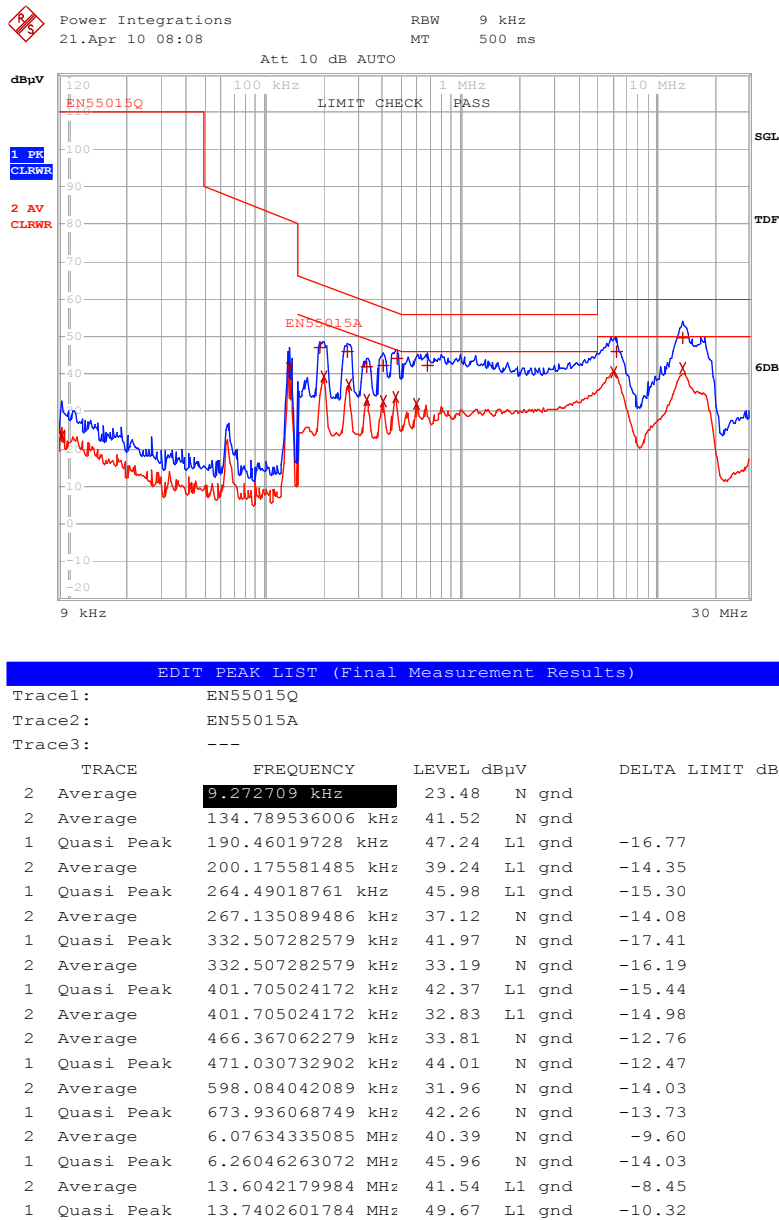


Figure 39 – Conducted EMI, Maximum Steady State Load, 230 VAC, 60 Hz, and EN55015 B Limits.

16 Revision History

Date	Author	Revision	Description & changes	Reviewed
14-Dec-10	DK	1.0	Initial Release	Apps & Mktg
13-May-11	DK	1.1	Corrected D7 mfg part number	Apps & Mktg



17 Appendix

17.1 Dimming Test with TRIAC Dimmer Switches

17.1.1 $V_{IN} = 115 \text{ VAC}$, 60 Hz

Style	Country	Manufacturer	Model Number	Dimming Test Data		
				Max. Current (mA)	Min. Current without Off Switch (mA)	Compatibility Notes
Rotary						
1	Taiwan		WS-5005	458	0	Increase preload, R7 = 5 KΩ, R11 = 10 KΩ
2	Taiwan	Diing Chung	DC-306	480	0	
3	Japan	Toshiba	WE0905	450	0	Increase preload, R7 = 5 KΩ, R11 = 10 KΩ
4	Japan	Panasonic	WN575149	418	0	Increase preload, R7 = 5 KΩ, R11 = 10 KΩ
Slider						
1	USA	Lutron	TGLV-600PR	420	42	
2	USA	Skylark	S-600PR	422	0	
3	USA	Leviton	6615-POW	460	87	
4	USA	Cooper	S106P	451	0	
5	Japan	Panasonic	WT7615	423	0	Increase preload, R7 = 5KΩ, R11 = 10 KΩ



17.1.2 $V_{IN} = 230 \text{ VAC}$, 50 Hz

Note output was not normalized (value of feedback resistor adjusted) for 230 VAC operation. When normalized a value of ~600 mA equates to a value of ~500 mA.

Style	Country	Manufacturer	Rated Power (if marked)	Model Number	Dimming Test Data		
					Max. Current (mA)	Min.Current without Off Switch (mA)	Compatibility Notes
Rotary							
1	Taiwan	Diing Chung		DG-306	578	0	Increase preload, R7 = 5 KΩ, R11 = 10 KΩ
2	China	TCL	630 W	Not marked	600	132	
3	China	Sang Bo Lang	300 W	Not marked	600	128	
4	China	EBAHuang		Not marked	575	0	
5	China	SB Electric	600 W	Not marked	559	0	
6	China	Myongbo		Not marked	600	76	
7	China	KBE	650 W	Not marked	575	0	Increase preload, R7 = 5 KΩ, R11 = 10 KΩ
8	China	CLIPMEI		Not marked	600	55	
9	China	MANK	200 W	Not marked	600	160	
10	German	Rev	300 W	Not marked	567	0	
11	German	Busch	600 W	2250	577	73	
12	German	MERTEN	400 W	572499	591	58	
13	German	Busch	420 W (trailing edge)	6513	577	110	
14	German	Berker		2875	568	88	
15	Korea	Anam		Not marked	594	175	
16	Korea	Shin Sung	500 W	Not marked	599	143	
17	Korea	Jin Heoung	500 W	Fantasia	593	170	
18	Korea	Shin Sung	700 W	Not marked	600	120	
19	Italy	RELCO	300 W	RH34LED PT	560	0	
20	Italy	RELCO	160 W	RM34DMA	594	112	
21	Italy	RELCO	500 W	RTM34LED DAXS	478	50	
22	Italy	RELCO	500 W	RM34DMA	600	112	
23	Italy	RELCO	300 W	RTS34.43RLI	600	0	
24	Italy	RELCO	500 W	RT34DSL	600	112	



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Power Integrations Worldwide Sales Support Locations

WORLD HEADQUARTERS

5245 Hellyer Avenue
San Jose, CA 95138, USA.
Main: +1-408-414-9200
Customer Service:
Phone: +1-408-414-9665
Fax: +1-408-414-9765
e-mail:
usasales@powerint.com

GERMANY

Rueckertstrasse 3
D-80336, Munich
Germany
Phone: +49-89-5527-3911
Fax: +49-89-5527-3920
e-mail:
eurosales@powerint.com

JAPAN

Kosei Dai-3 Building
2-12-11, Shin-Yokohama,
Kohoku-ku, Yokohama-shi,
Kanagawa 222-0033
Japan
Phone: +81-45-471-1021
Fax: +81-45-471-3717
e-mail: japansales@powerint.com

TAIWAN

5F, No. 318, Nei Hu Rd., Sec. 1
Nei Hu District
Taipei 114, Taiwan R.O.C.
Phone: +886-2-2659-4570
Fax: +886-2-2659-4550
e-mail:
taiwansales@powerint.com

CHINA (SHANGHAI)

Rm 1601/1610, Tower 1
Kerry Everbright City
No. 218 Tianmu Road West
Shanghai, P.R.C. 200070
Phone: +86-021-6354-6323
Fax: +86-021-6354-6325
e-mail:
chinasales@powerint.com

INDIA

#1, 14th Main Road
Vasanthanagar
Bangalore-560052
India
Phone: +91-80-4113-8020
Fax: +91-80-4113-8023
e-mail:
indiasales@powerint.com

KOREA

RM 602, 6FL
Korea City Air Terminal B/D, 159-6
Samsung-Dong, Kangnam-Gu,
Seoul, 135-728
Korea
Phone: +82-2-2016-6610
Fax: +82-2-2016-6630
e-mail: koreasales@powerint.com

EUROPE HQ

1st Floor, St. James's House
East Street, Farnham
Surrey GU9 7TJ
United Kingdom
Phone: +44 (0) 1252-730-141
Fax: +44 (0) 1252-727-689
e-mail:
eurosales@powerint.com

CHINA (SHENZHEN)

Rm A, B & C 4th Floor, Block C,
Electronics Science and
Technology Building
2070 Shennan Zhong Road
Shenzhen, Guangdong,
P.R.C. 518031
Phone: +86-755-8379-3243
Fax: +86-755-8379-5828
e-mail:
chinasales@powerint.com

ITALY

Via De Amicis 2
20091 Bresso MI
Italy
Phone: +39-028-928-6000
Fax: +39-028-928-6009
e-mail:
eurosales@powerint.com

SINGAPORE

51 Newton Road,
#19-01/05 Goldhill Plaza
Singapore, 308900
Phone: +65-6358-2160
Fax: +65-6358-2015
e-mail:
singaporesales@powerint.com

APPLICATIONS HOTLINE

World Wide +1-408-414-9660

APPLICATIONS FAX

World Wide +1-408-414-9760



Power Integrations, Inc.

Tel: +1 408 414 9200 Fax: +1 408 414 9201
www.powerint.com