

Power Operational Amplifiers

RoHS
COMPLIANT

FEATURES

- Low Cost
- Wide Common Mode Range
- Standard Supply Voltage
- Single Supply: 10V to 50V SMPS input
- Output Current: 150 mA Continuous
- Output Voltage 50V to 340V (single supply)
- 350 V/ μ s Slew Rate
- 200 kHz Power Bandwidth
- On-board Power Supply



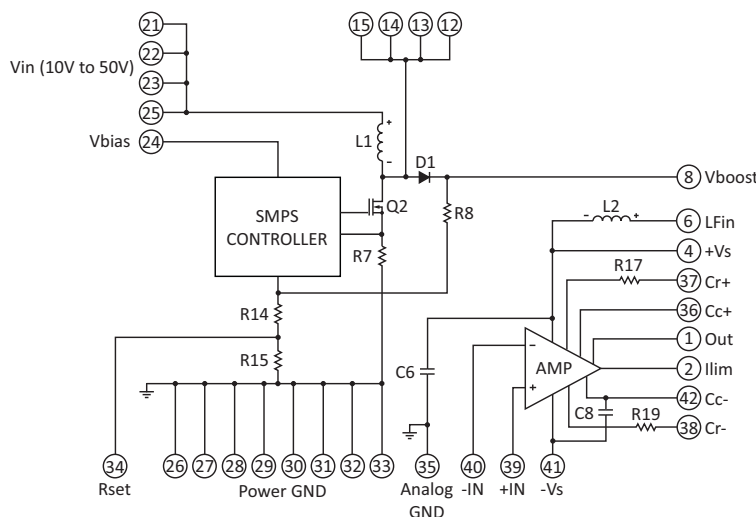
APPLICATIONS

- Piezoelectric Positioning and Actuation
- Electrostatic Deflection
- Deformable Mirror Actuators
- Chemical and Biological Stimulators

DESCRIPTION

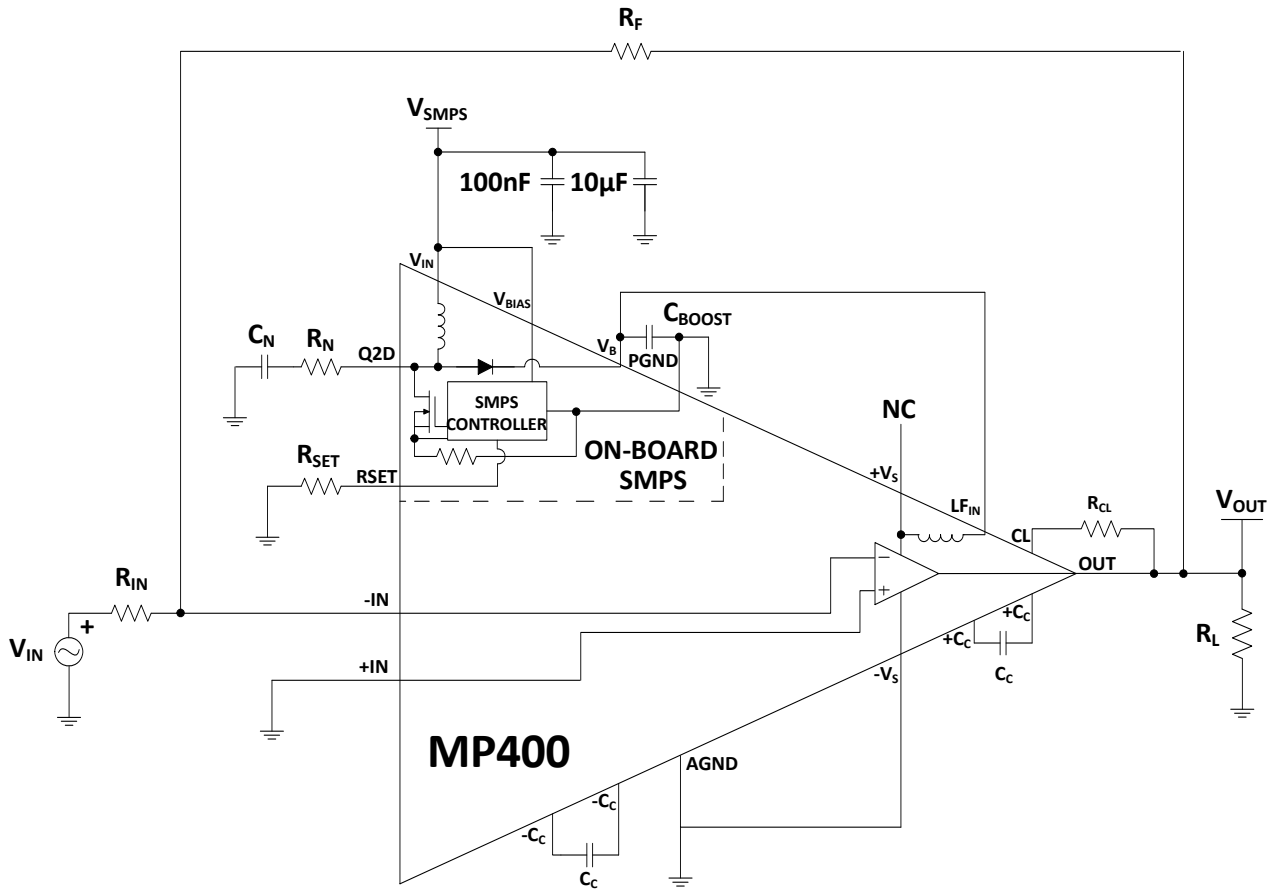
The MP400FC combines a high voltage, high speed precision power op amp with a supply voltage boost function in an integrated thermally conductive module. The voltage boost function uses a switch mode power supply (SMPS) to boost the input power supply voltage. This allows the user the benefits of using a standard 12 V or 24 V bus without the need to design a high voltage supply to power the op amp. The SMPS voltage is adjustable from 50-350 V, allowing for op amp output voltages up to 340 V. External phase compensation provides the user with the flexibility to tailor gain, slew rate and bandwidth for a specific application. The unique design of this amplifier provides extremely high slew rates in pulse applications while maintaining low quiescent current. The output stage is well protected with a user defined current limit. Safe Operating Area (SOA) must be observed for reliable operation.

Figure 1: Equivalent Schematic



TYPICAL CONNECTION

Figure 2: Typical Connection



PINOUT AND DESCRIPTION TABLE

Figure 3: External Connections

			C_C	<u>42</u>
			$-V_S$	<u>41</u>
<u>1</u>	OUT		$-IN$	<u>40</u>
<u>2</u>	CL		$+IN$	<u>39</u>
<u>3</u>	NC		C_R	<u>38</u>
<u>4</u>	$+V_S$		C_{R+}	<u>37</u>
<u>5</u>	NC		C_{C+}	<u>36</u>
<u>6</u>	LF_{IN}		AGND	<u>35</u>
<u>7</u>	NC		RESET	<u>34</u>
<u>8</u>	V_B	MP400	PGND	<u>33</u>
<u>9</u>	NC	(from backplate)	PGND	<u>32</u>
<u>10</u>	NC		PGND	<u>31</u>
<u>11</u>	NC		PGND	<u>30</u>
<u>12</u>	Q2D		PGND	<u>29</u>
<u>13</u>	Q2D		PGND	<u>28</u>
<u>14</u>	Q2D		PGND	<u>27</u>
<u>15</u>	Q2D		PGND	<u>26</u>
<u>16</u>	NC		V_{IN}	<u>25</u>
<u>17</u>	NC		V_{BIAS}	<u>24</u>
<u>18</u>	NC		V_{IN}	<u>23</u>
<u>19</u>	NC		V_{IN}	<u>22</u>
<u>20</u>	NC		V_{IN}	<u>21</u>

Unused pins should be left open. This is mandatory for pins 3, 5, 7, 9, 11 and 16.

Pin Number	Name	Description
1	OUT	The output. Connect this pin to load and to the feedback resistor.
2	CL	Connect to the current limit resistor, and then the OUT pin. Output current flows into/out of this pin through R_{CL} .
4	$+V_S$	The positive supply rail. Leave open when using on-board SMPS.
6	LF_{IN}	The supply filter. When using the on-board SMPS, connect this pin to V_B to power the amplifier. This filters the SMPS current through a 47 μ H inductor. The current to this pin can not exceed 200 mA. See applicable section.
8	V_B	This is the output of the high voltage SMPS and typically is tied to pin 6, LF_{IN} . Other loads can be added to this pin as long as the maximum output power of the SMPS is not exceeded. For proper operation, an external high voltage, low ESR capacitor must be connected to this pin. See applicable section.
12, 13, 14, 15	Q2D	Drain node of the SMPS MOSFET switch. An external RC snubber may be connected from this node to power ground to reduce or eliminate overshoot and ringing at switch turn off, reducing switching noise on the SMPS.
21, 22, 23, 25	V_{in}	Input voltage pins for the on-board high voltage switch mode power supply. Supply with 10-50 V.
24	V_{bias}	Input voltage pin for the boost controller circuitry. This pin is typically tied to V_{IN} .

MP400FC

Pin Number	Name	Description
26-33	PGND	Power ground. SMPS switching circuits are referenced to ground through these pins.
34	RSET	SMPS voltage set resistor connecton. The 'Set Resistor' is connected from this pin to PGND to set the SMPS voltage. Select value based on desired V_{BOOST} . See applicable section.
35	AGND	Analog ground for amplifier circuit. AGND and PGND are connected at one point on the unit. Avoid external connections between AGND and PGND.
36, 37	+CC	Positive compensation capacitor connection. Select value based on Phase Compensation. See applicable section.
38, 42	-CC	Negative compensation capacitor connection. Select value based on Phase Compensation. See applicable section.
39	+IN	The non-inverting input.
40	-IN	The inverting input.
41	-Vs	The negative supply rail. This pin is typically connected to AGND. However, an external negative supply voltage can be connected to this pin.
All Others	NC	No connection.

SPECIFICATIONS

All Min/Max characteristics and specifications are guaranteed over the Specified Operating Conditions. Typical performance characteristics and specifications are derived from measurements taken at typical supply voltages and $T_C = 25^\circ\text{C}$. $+V_S$ and $-V_S$ denote the positive and negative supply voltages to the output stage.

ABSOLUTE MAXIMUM RATINGS

Parameter	Symbol	Min	Max	Units
Supply Voltage, Total, SMPS	$+V_{\text{SMPS}}$ to GND		50	V
Supply Voltage, Total, Amplifier	$+V_S$ to $-V_S$		350	V
Output Current, peak within SOA	I_O		200	mA
Power Dissipation, Internal, DC, Amplifier	P_D		14.2	W
Output Power, SMPS	$P_{\text{OUT, SMPS}}$		67	W
Input Voltage, differential	$V_{\text{IN (Diff)}}$	-16	+16	V
Input Voltage, common mode	V_{cm}	$-V_S$	$+V_S$	V
Temperature, pin solder, 10s max.			225	$^\circ\text{C}$
Temperature, junction ¹	T_J		150	$^\circ\text{C}$
Temperature Range, storage		-40	+105	$^\circ\text{C}$
Operating Temperature Range, case	T_C	-40	+85	$^\circ\text{C}$

1. Long term operation at the maximum junction temperature will result in reduced product life. Derate power dissipation to achieve high MTTF.

AMPLIFIER INPUT

Parameter	Test Conditions	Min	Typ	Max	Units
Offset Voltage, initial			8	40	mV
Offset Voltage vs. Temperature	0 to 85°C (Case)		-63		$\mu\text{V}/^\circ\text{C}$
Offset Voltage vs. Supply				32	$\mu\text{V}/\text{V}$
Bias Current, initial ¹			8.5	200	pA
Offset Current, initial			12	400	pA
Input Resistance, DC			10^6		Ω
Common Mode Voltage Range, pos.			$+V_S - 2$		V
Common Mode Voltage Range, neg.			$-V_S + 5.5$		V
Common Mode Rejection, DC		90	118		dB
Noise	700 kHz bandwidth		418		$\mu\text{V RMS}$

1. Doubles for every 10°C of temperature increase.

AMPLIFIER GAIN

Parameter	Test Conditions	Min	Typ	Max	Units
Open Loop @ 15 Hz		89	120		dB
Gain Bandwidth Product @ 1 MHz			1		MHz
Power Bandwidth, 300 V _{P-P}	+V _S = 160 V, -V _S = -160 V		200		kHz
Phase Margin	Full temp range		50		°

AMPLIFIER OUTPUT

Parameter	Test Conditions	Min	Typ	Max	Units
Voltage Swing	I _O = 10 mA		V _S - 2		V
Voltage Swing	I _O = 100 mA		V _S - 8.6	V _S - 12	V
Voltage Swing	I _O = 150 mA		V _S - 10		V
Current, continuous, DC		150			mA
Slew Rate		100	350		V/μs
Settling Time, to 0.1%	2 V Step		1		μs
Resistance, No load	R _{LIM} = 6.2 Ω		44		Ω
Current, quiescent, amplifier only		0.2	0.7	2.5	mA

SMPS

Parameter	Test Conditions	Min	Typ	Max	Units
Input Voltage, V _{IN}		10		50	V
SMPS Output Voltage, V _B		46.75		365	V
SMPS Output Current, I _S	V _B = 10x V _{IN}	150			mA
Output Voltage Tolerance	V _B ≤ 10x V _{IN} , I _S ≤ 150 mA, R _{SET} = 1%		+/-2	6.5	%
Voltage Boost			10		x input V

THERMAL

Parameter	Test Conditions	Min	Typ	Max	Units
Resistance, DC, junction to case	Full temp range, f<60 Hz		7.7	8.8	°C/W
Resistance, junction to air	Full temp range		46		°C/W
Temperature Range, case		0		70	°C

TYPICAL PERFORMANCE GRAPHS

Figure 4: Power Response

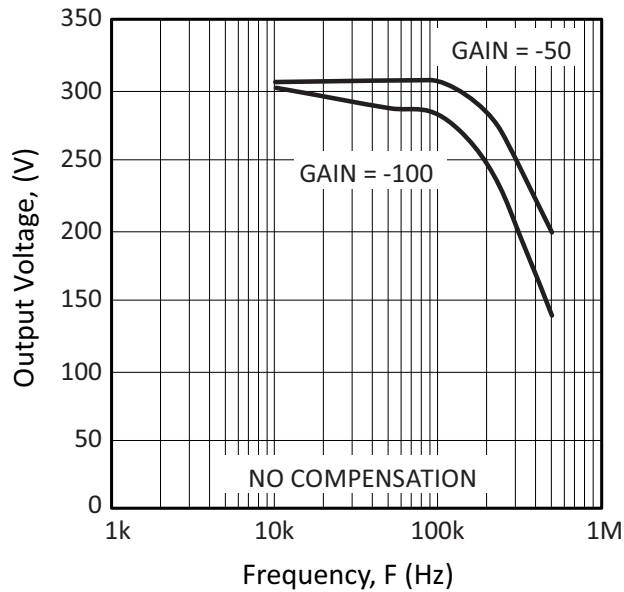


Figure 5: Current Limit

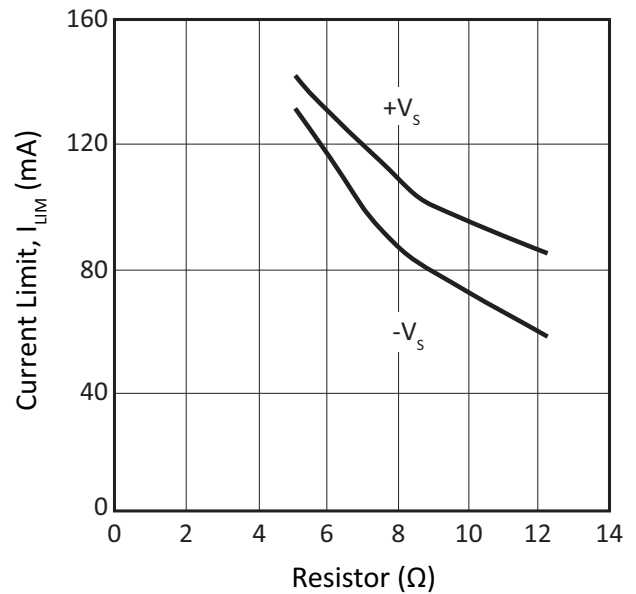


Figure 6: Power Supply Rejection

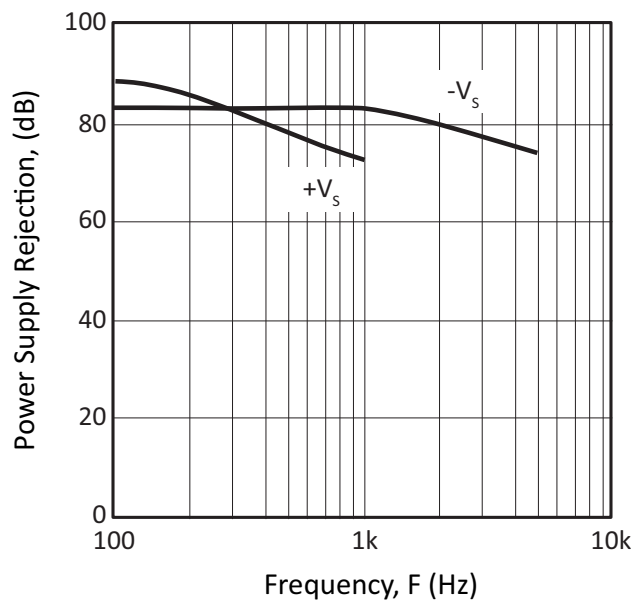


Figure 7: Amplifier Internal Power Derating

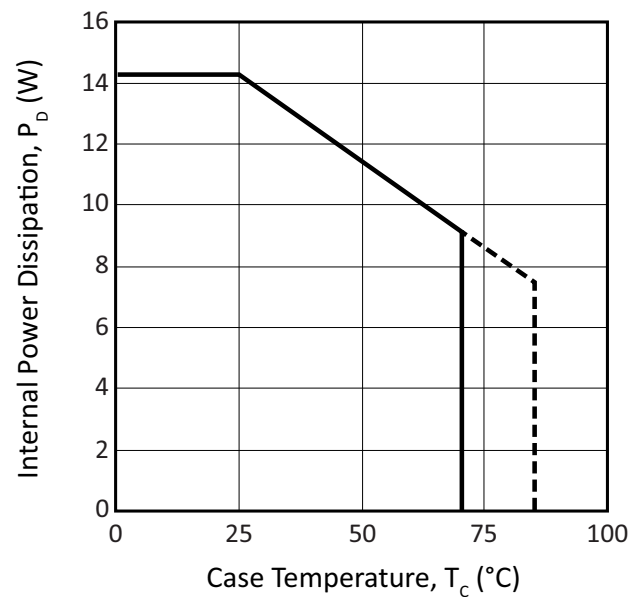


Figure 8: Output Voltage Swing

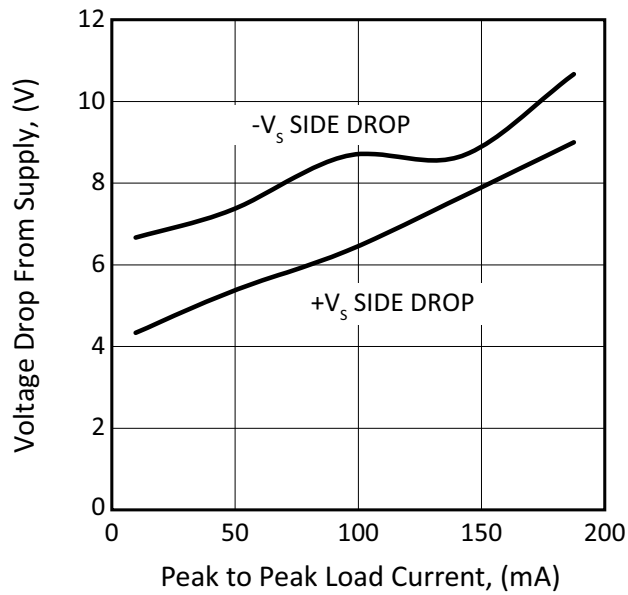


Figure 9: Common Mode Rejection

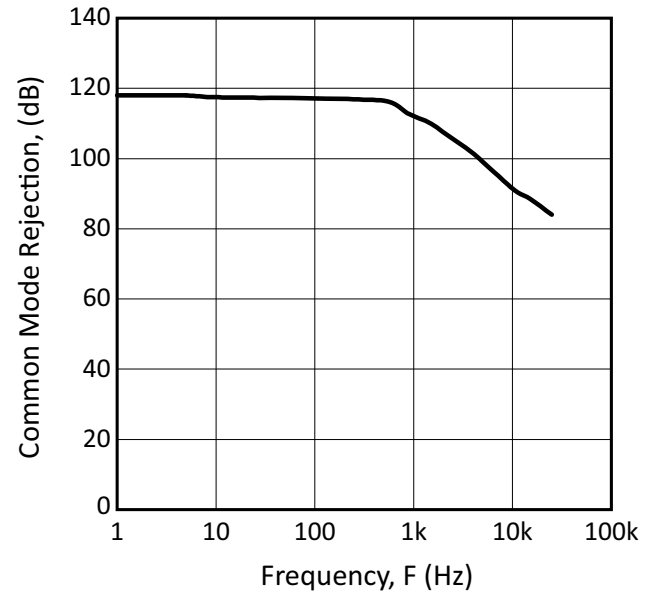


Figure 10: Efficiency vs. SMPS Current

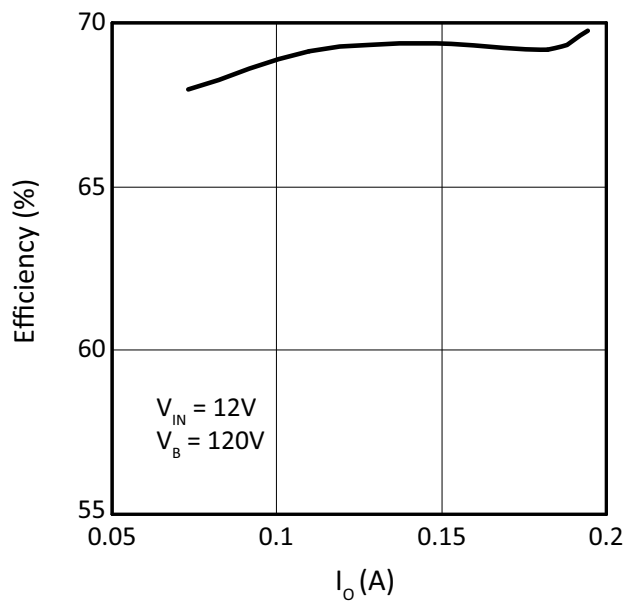


Figure 11: Efficiency vs. SMPS Current

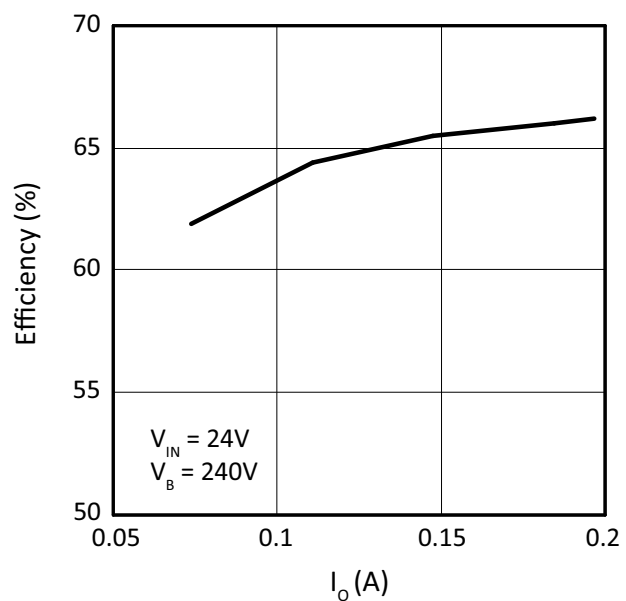


Figure 12: Efficiency vs. SMPS Current

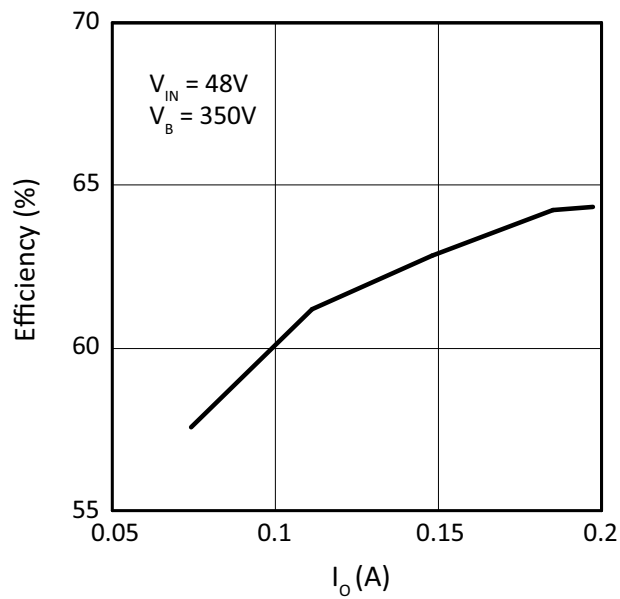


Figure 13: SMPS Current vs. SMPS Voltage

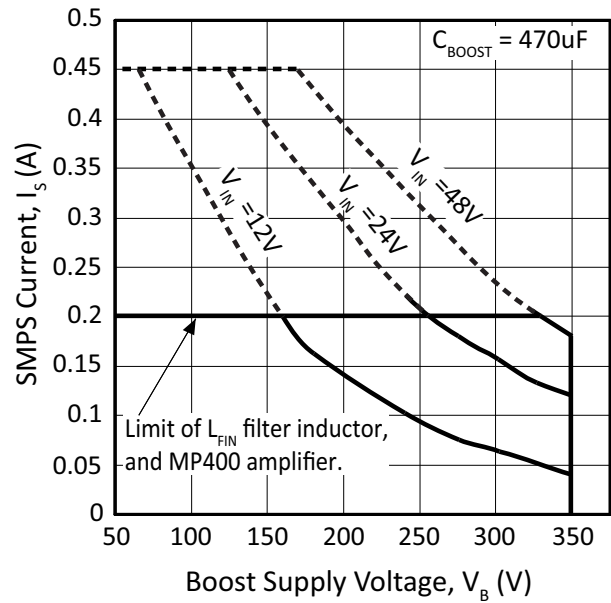


Figure 14: SMPS Power Derating

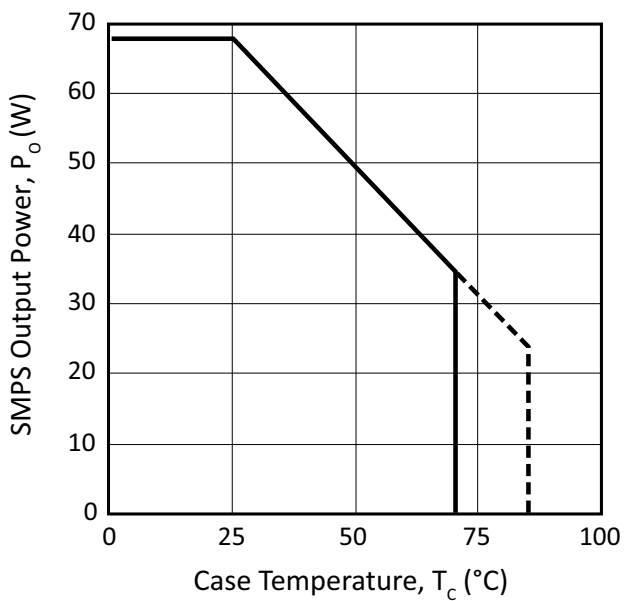


Figure 15: Pulse Response vs. Cap Load

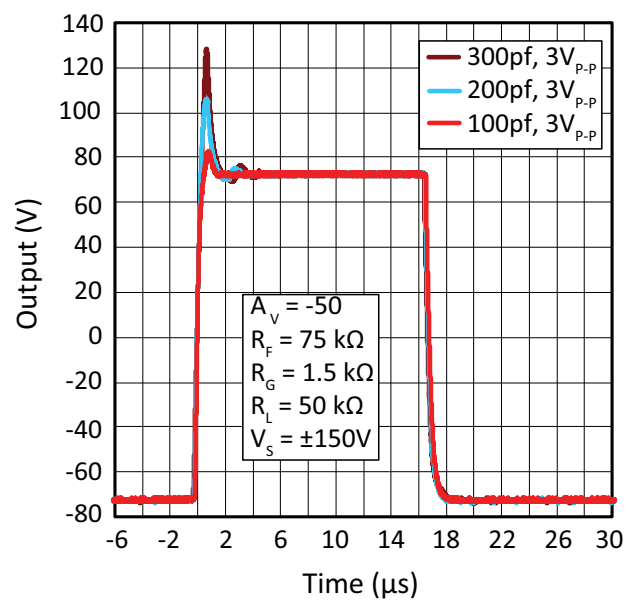


Figure 16: Pulse Response vs. Cap Load

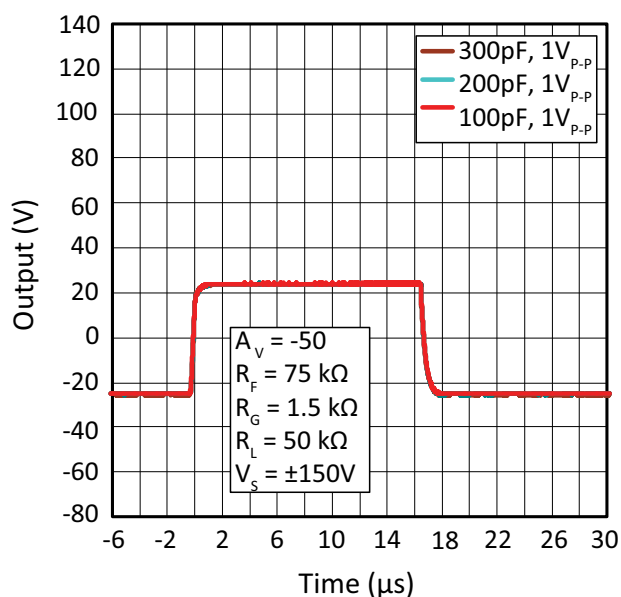


Figure 17: Pulse Response vs. Cap Load

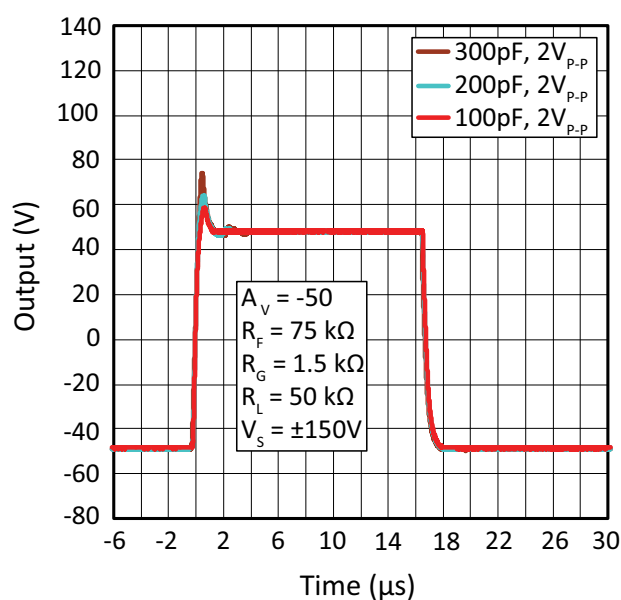


Figure 18: Small Signal Open Loop Gain

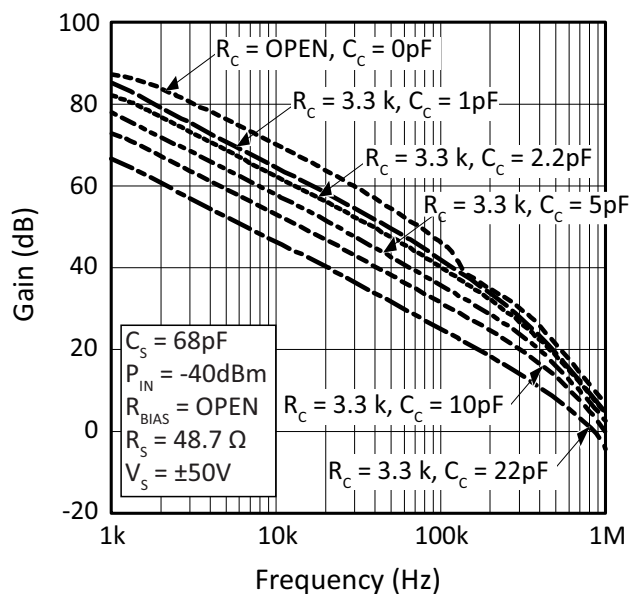


Figure 19: Small Signal Open Loop Phase, $V_O = 250 \text{ mV}_{p-p}$

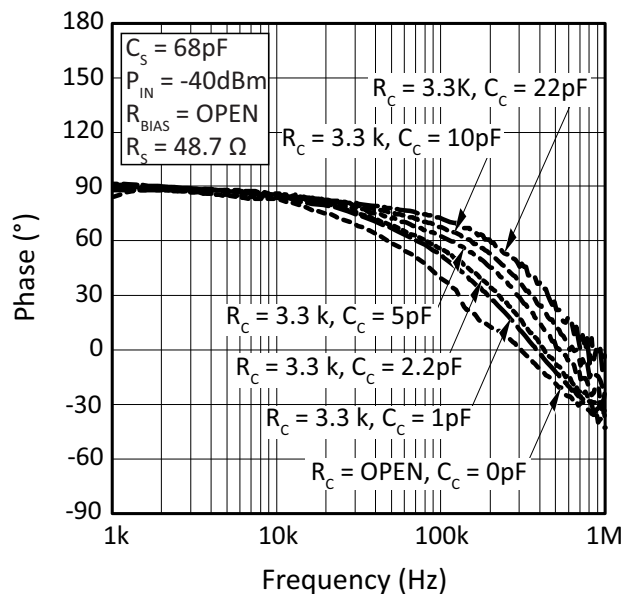


Figure 20: Small Signal Open Loop Phase

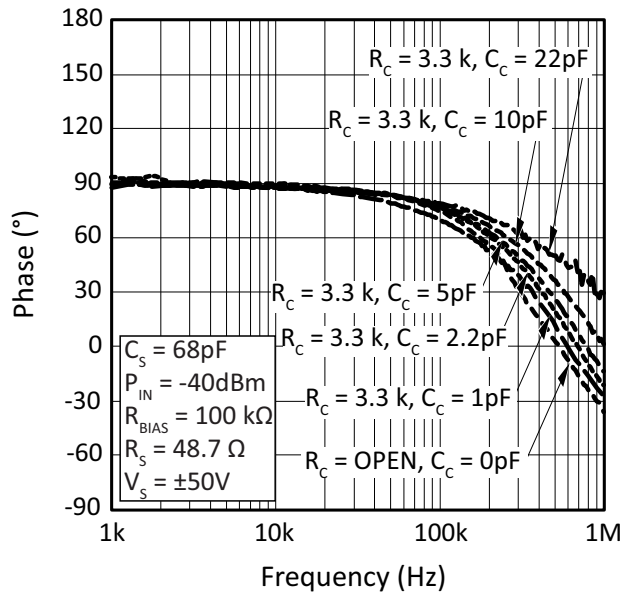


Figure 21: Gain vs. Input/Output Signal Level

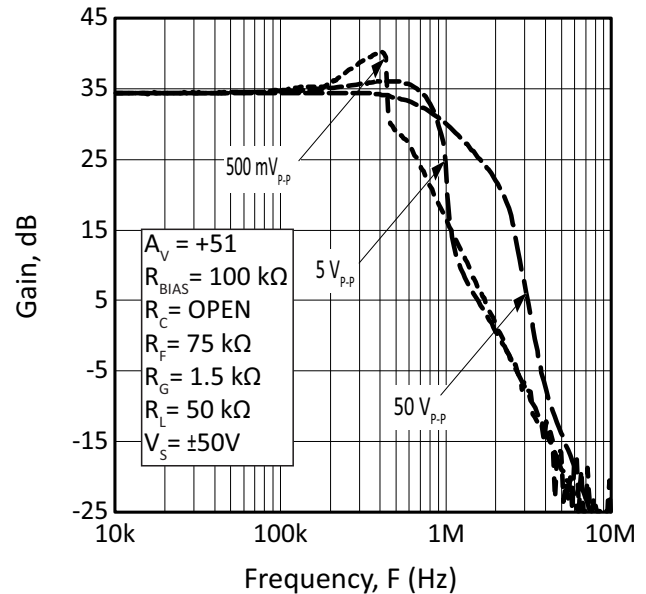


Figure 22: Small Signal Gain vs. Compensation, $V_O=5\text{V}_{p-p}$

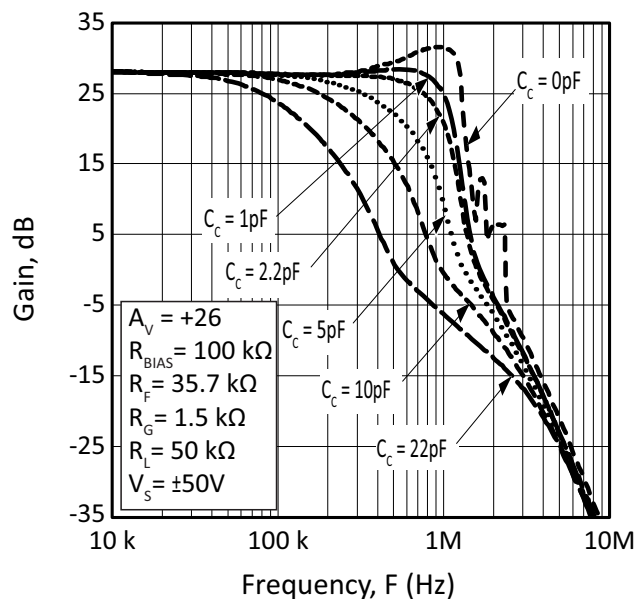


Figure 23: Small Signal Gain vs. Compensation, $V_O=500\text{mV}_{p-p}$

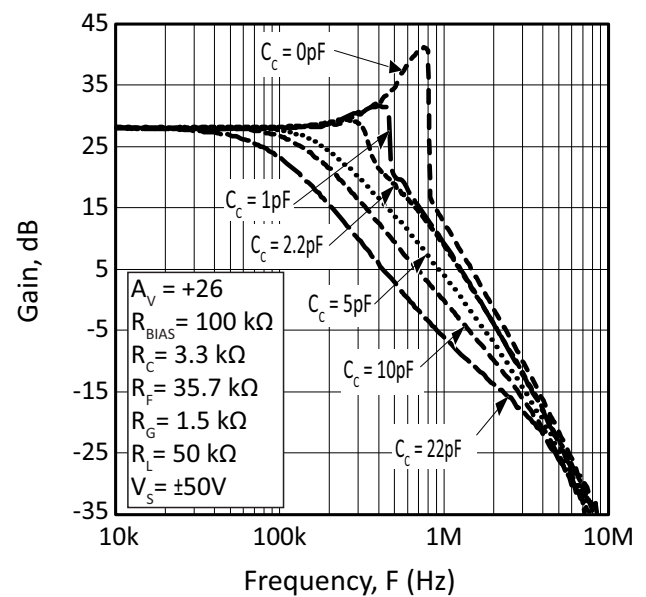


Figure 24: Large Signal Gain vs. Compensation, $V_O=50V_{p-p}$

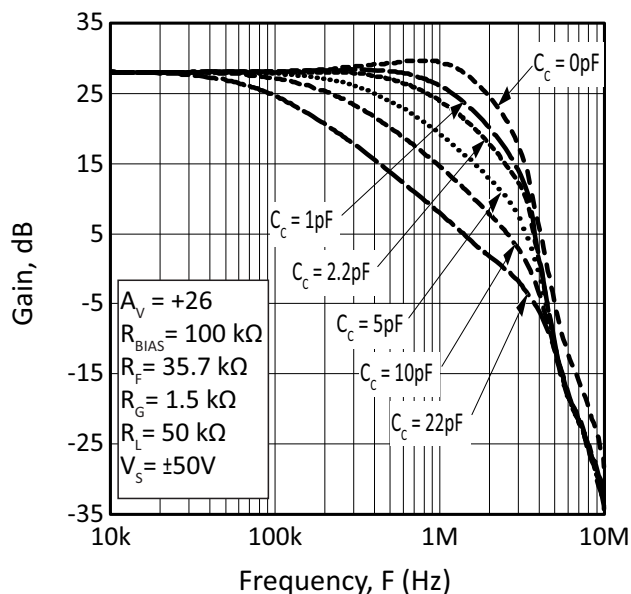


Figure 25: SR+/SR- (25% - 75%)

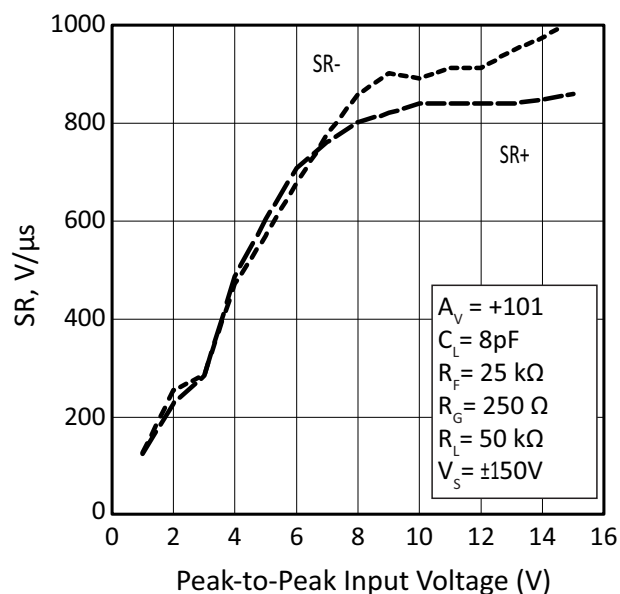


Figure 26: SR+/SR- (25% - 75%)

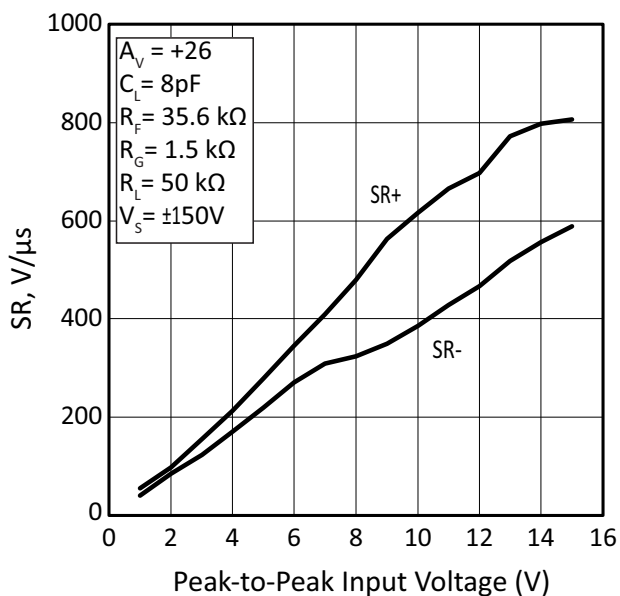


Figure 27: SR+/SR- (25% - 75%)

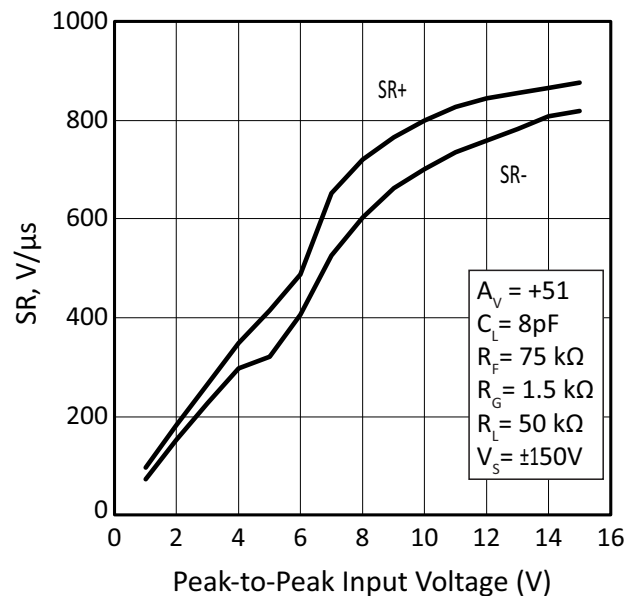


Figure 28: Rise and Fall Time (10% - 90%)

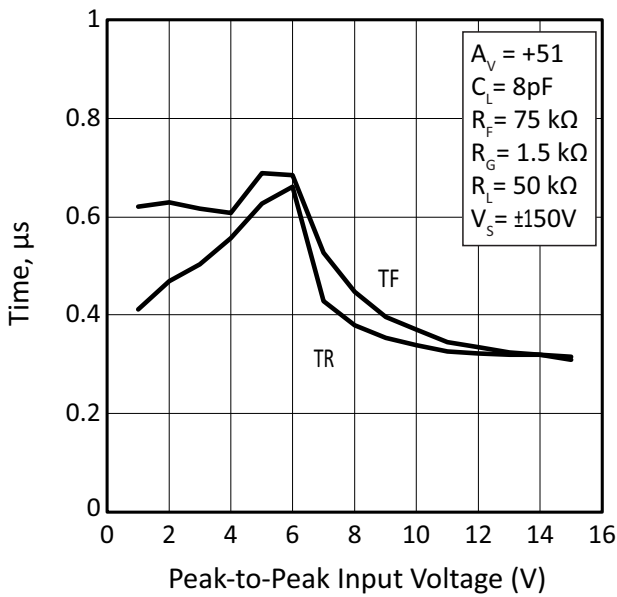


Figure 29: Transient Response

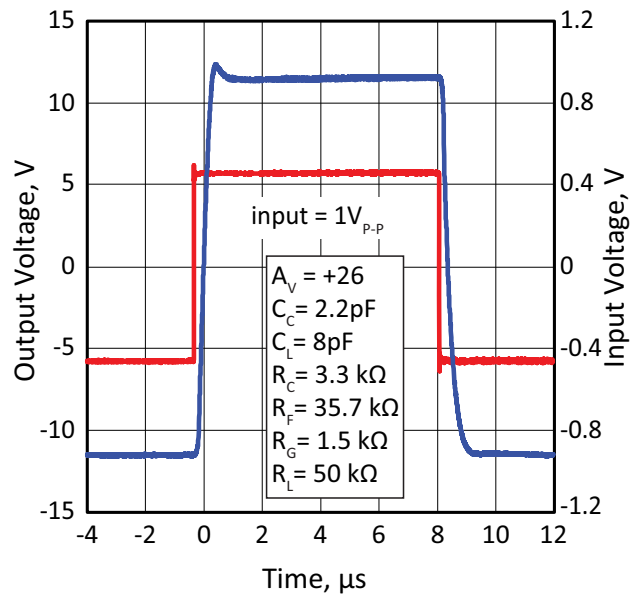


Figure 30: Transient Response

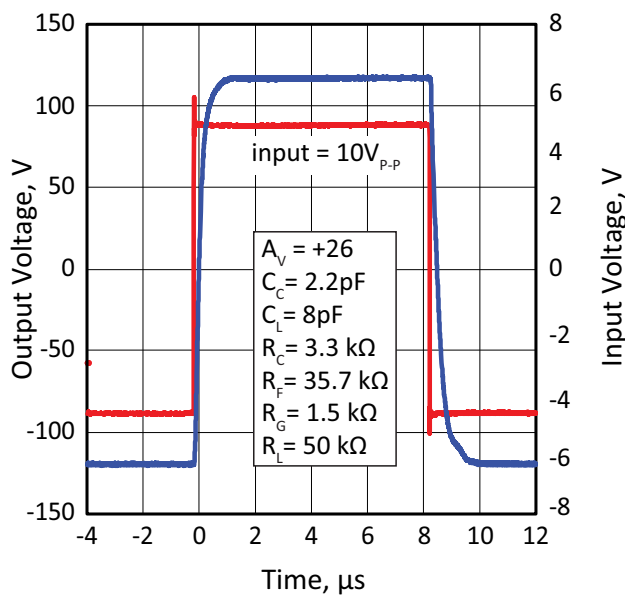


Figure 31: Transient Response

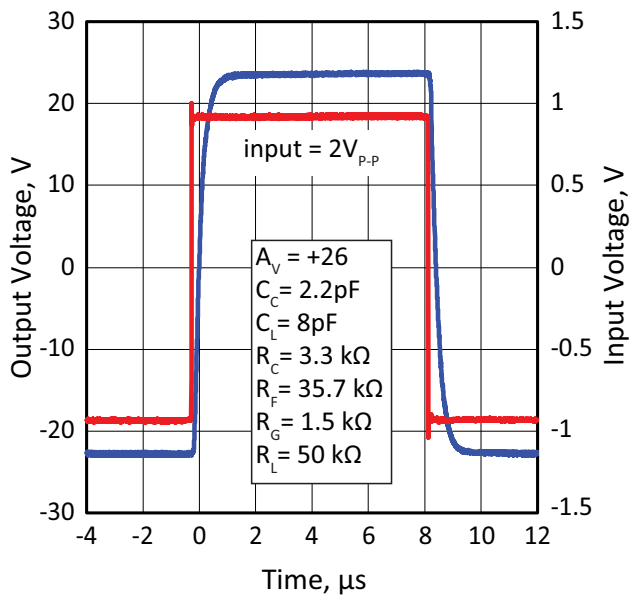


Figure 32: Pulse Response vs. C_C and R_C

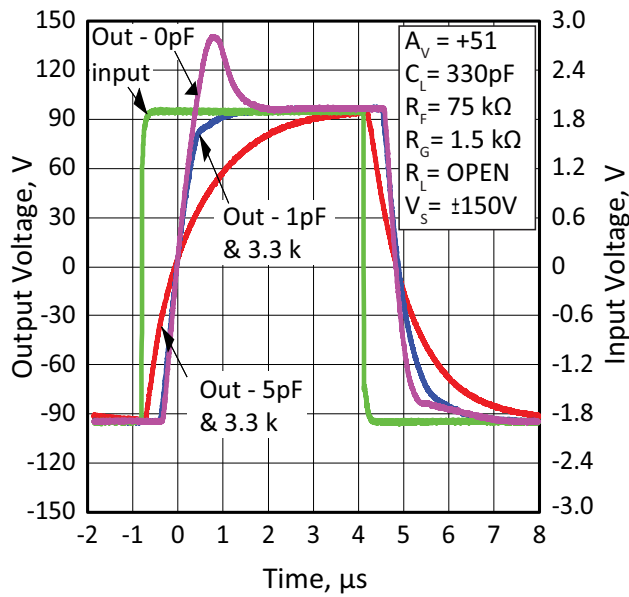


Figure 33: Pulse Response

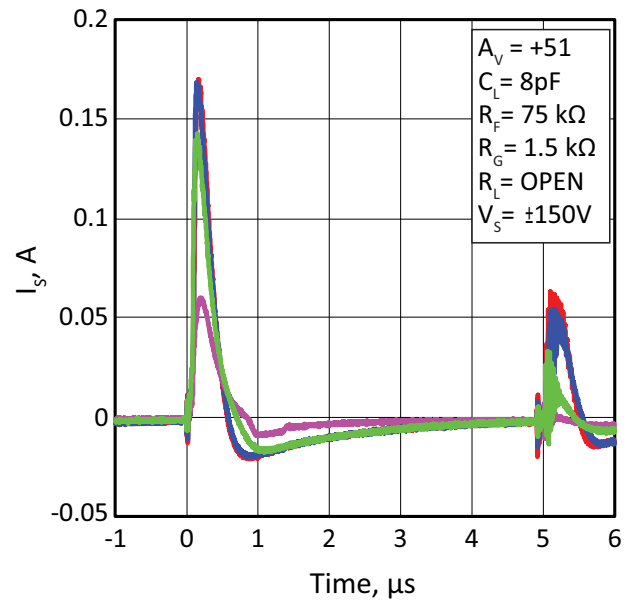


Figure 34: Overdrive Recovery

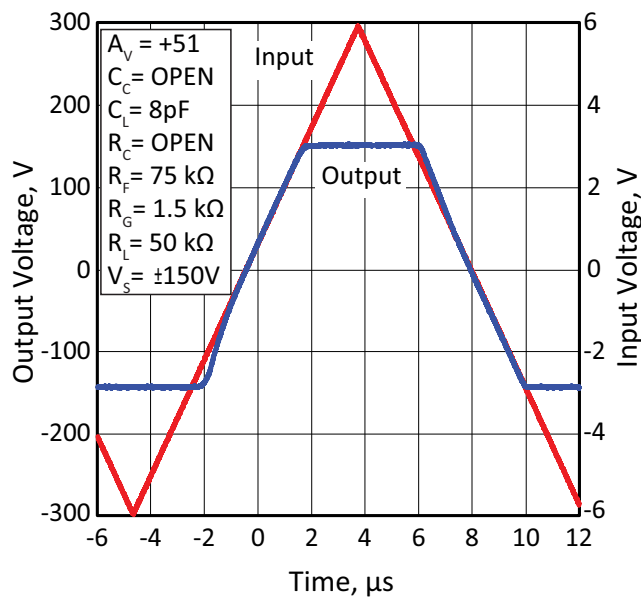


Figure 35: I_S vs. V_{IN}

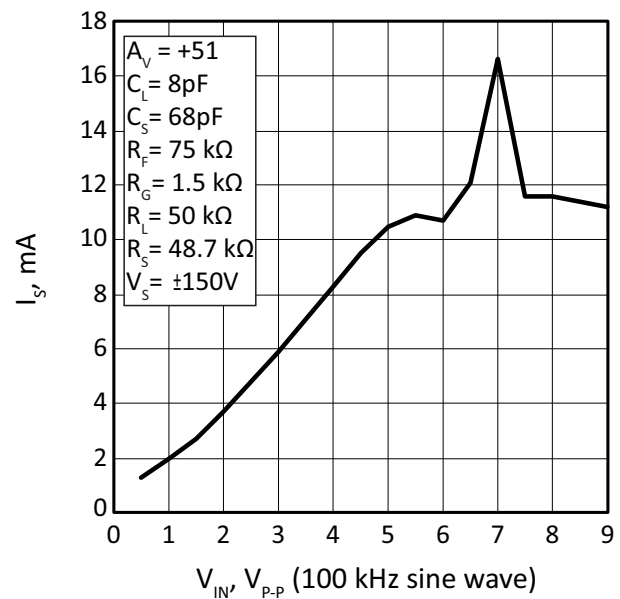


Figure 36: Supply Current vs. Frequency

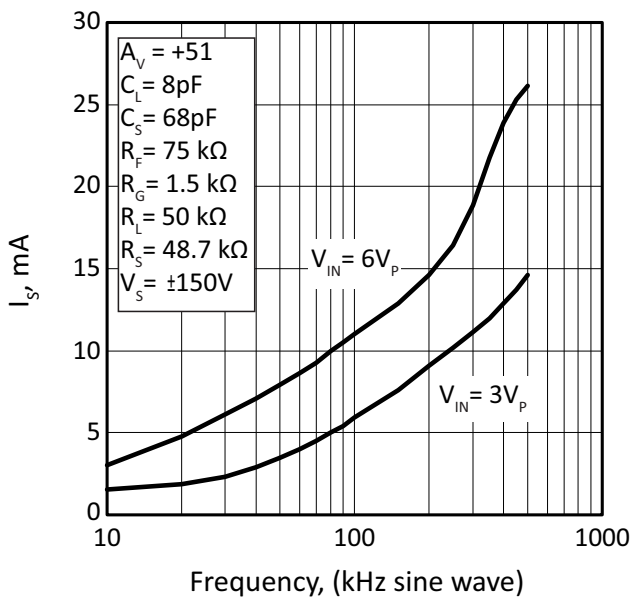


Figure 37: SR+/SR- (25% - 75%)

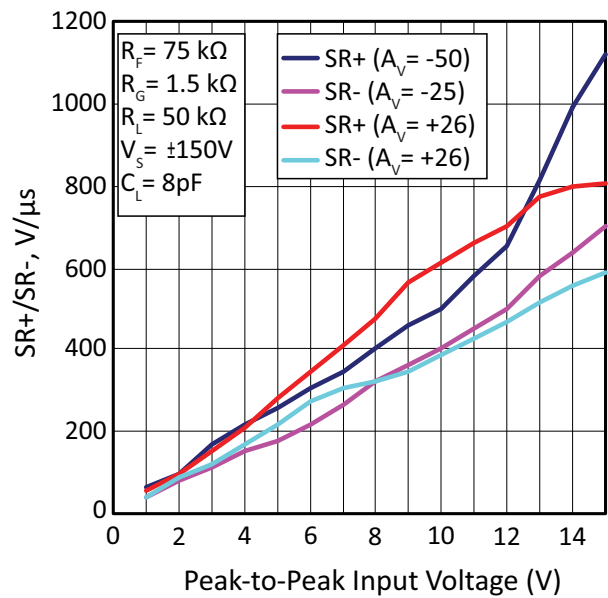
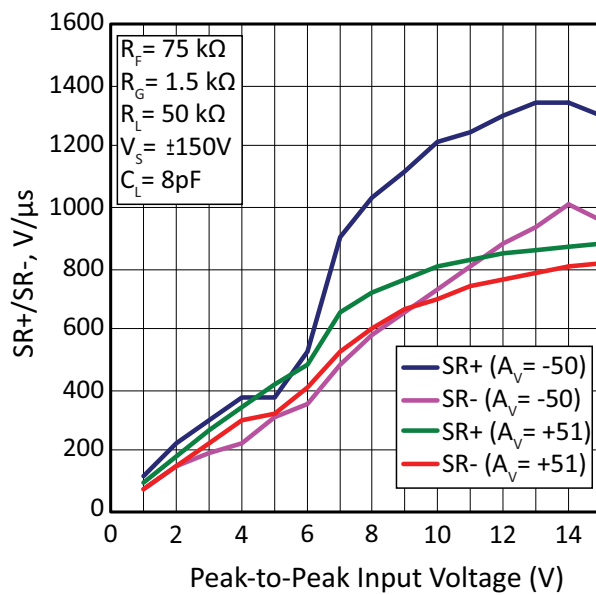


Figure 38: SR+/SR- (25% - 75%)

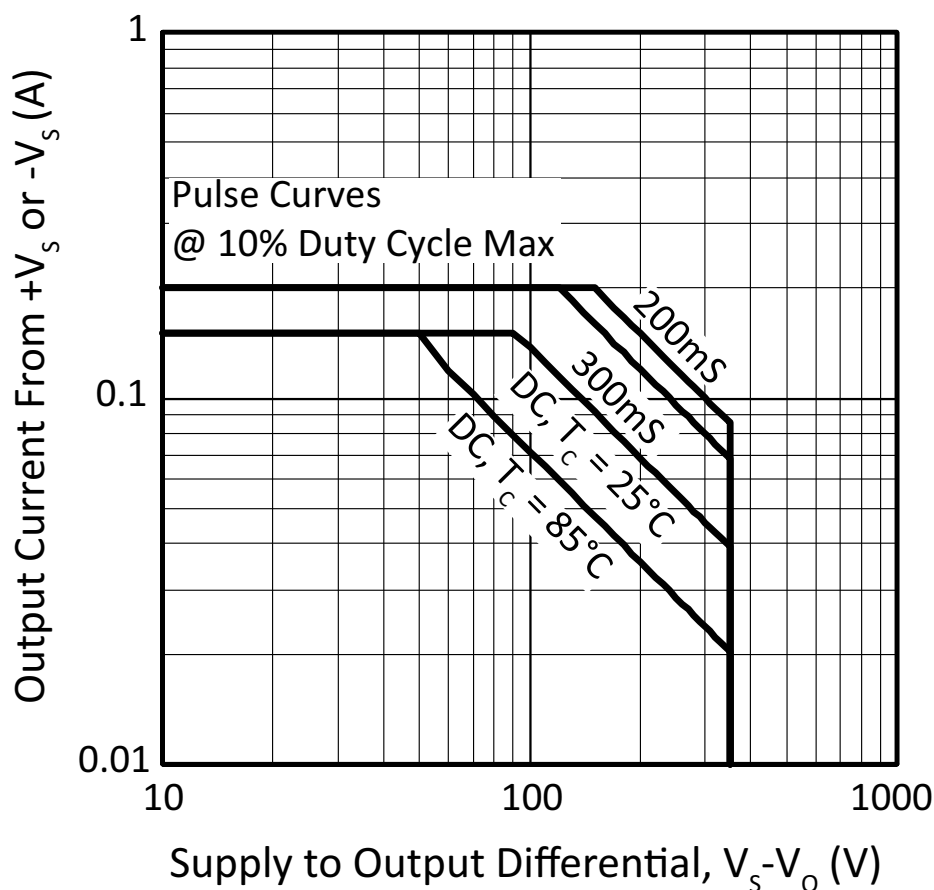


SAFE OPERATING AREA (SOA)

The MOSFET output stage of the MP400FC is not limited by second breakdown considerations as in bipolar output stages. Only thermal considerations of the package and current handling capabilities limit the Safe Operating Area. The SOA plots include power dissipation limitations which are dependent upon case temperature. Keep in mind that the dynamic current sources which drive high slew rates can increase the operating temperature of the amplifier during periods of repeated slewing. The plot of supply current vs. input signal amplitude for a 100 kHz signal provides an indication of the supply current with repeated slewing conditions. This application dependent condition must be considered carefully.

The output stage is self-protected against transient flyback by the parasitic body diodes of the output stage. However, for protection against sustained high energy flyback, external, fast recovery diodes must be used.

Figure 39: SOA



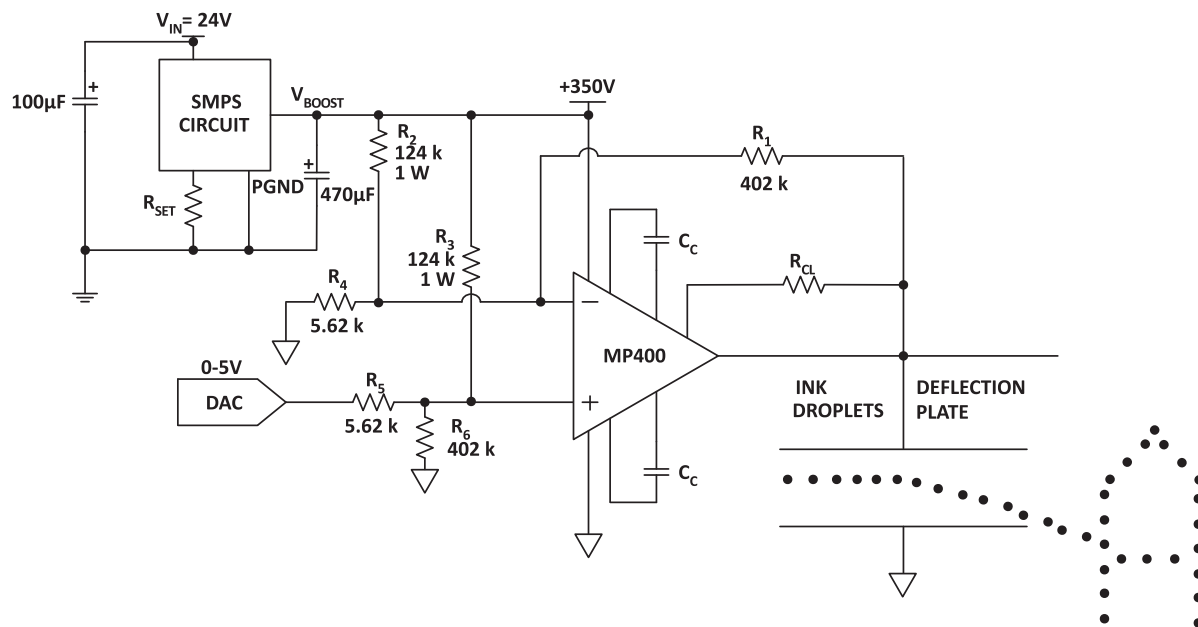
GENERAL

Please read Application Note 1 “General Operating Considerations” which covers stability, supplies, heat sinking, mounting, current limit, SOA interpretation, and specification interpretation. Visit www.apexanalog.com for Apex Microtechnology’s complete Application Notes library, Technical Seminar Workbook, and Evaluation Kits.

TYPICAL APPLICATION

The MP400FC is ideally suited to driving both piezo actuation and deflection applications off of a single low voltage supply. The circuit in figure 40 boosts a system 24 V bus to 350 V to drive an ink jet print head. The MP400FCs high speed deflection amplifier is biased for single supply operation by external resistors R2 – R6, so that a 0 to 5 V DAC can be used as the input to the amplifier to drive the print head from 0 to >300 V. Refer to Apex Application Note 21.

Figure 40: Typical Application



THEORY OF OPERATION

The MP400 is designed specifically as a high speed pulse amplifier. In order to achieve high slew rates with low idle current, the internal design is quite different from traditional voltage feedback amplifiers. Basic op amp behaviors like high input impedance and high open loop gain still apply. But there are some notable differences, such as signal dependent supply current, bandwidth and output impedance, among others. The impact of these differences varies depending on application performance requirements and circumstances. These different behaviors are ideal for some applications but can make designs more challenging in other circumstances.

SUPPLY CURRENT AND BYPASS CAPACITANCE

A traditional voltage feedback amplifier relies on fixed current sources in each stage to drive the parasitic capacitances of the next stage. These currents combine to define the idle or quiescent current of the amplifier. By design, these fixed currents are often the limiting parameter for slew rate and bandwidth of the amplifier. Amplifiers which are high voltage and have fast slew rates typically have high idle currents and dissipate notable power with no signal applied to the load. At the heart of the MP400 design is a signal dependent current source which strikes a new balance between supply current and dynamic performance. With small input signals, the supply current of the MP400 is very low, idling at less than 1 mA. With large transient input signals, the supply currents increase dramatically to allow the amplifier stages to respond quickly. The Pulse Response plot in the typical performance section of this datasheet describes the dynamic nature of the supply current with various input transients.

Choosing proper bypass capacitance requires careful consideration of the dynamic supply currents. High frequency ceramic capacitors of 0.1 μF or more should be placed as close as possible to the amplifier supply pins. The inductance of the routing from the supply pins to these ceramic capacitors will limit the supply of peak current during transients, thus reducing the slew rate of the MP400. The high frequency capacitance should be supplemented by additional bypass capacitance not more than a few centimeters from the amplifier. This additional bypass can be a slower capacitor technology, such as electrolytic, and is necessary to keep the supplies stable during sustained output currents. Generally, a few microfarads is sufficient.

SMALL SIGNAL PERFORMANCE

The small signal performance plots in the typical performance section of this datasheet describe the behavior when the dynamic current sources described previously are near the idle state. The selection of compensation capacitor directly affects the open loop gain and phase performance.

Depending on the configuration of the amplifier, these plots show that the phase margin can diminish to very low levels when left uncompensated. This is due to the amount of bias current in the input stage when the part is in standby. An increase in the idle current in the output stage of the amplifier will improve phase margin for small signals although will increase the overall supply current.

Current can be injected into the output stage by adding a resistor, R_{BIAS} , between pins 42 and 4. The size of R_{BIAS} will depend upon the application but 500 μA (50 V V_{+} supply/100K) of added bias current shows significant improvement in the small signal phase plots. Adding this resistor has little to no impact on small signal gain or large signal performance as under these conditions the current in the input stage is elevated over its idle value. It should also be noted that connecting a resistor to the upper supply only injects a fixed current and if the upper supply is fixed and well bypassed. If the application includes variable or adjustable supplies, a current source diode could also be used. These two terminal components combine a JFET and resistor connected within the package to behave like a current source.

As a second stability measure, the MP400 is externally compensated and performance can be optimized to the application. Unlike the R_{BIAS} technique, external phase compensation maintains the low idle current but does affect the large signal response of the amplifier. Refer to the small and large signal response plots as a guide in making the tradeoffs between bandwidth and stability. Due to the unique design of the MP400, two symmetric compensation networks are required. The compensation capacitor C_c must be rated for a working voltage of the full operating supply voltage ($+V_S$ to $-V_S$). NPO capacitors are recommended to maintain the desired level of compensation over temperature.

LARGE SIGNAL PERFORMANCE

As the amplitude of the input signal increases, the internal dynamic current sources increase the operation bandwidth of the amplifier. This unique performance is apparent in its slew rate, pulse response, and large signal performance plots. Recall the previous discussion about the relationships between signal amplitude, supply current, and slew rate. As the amplitude of the input amplitude increases from 1 V_{p-p} to 15 V_{p-p}, the slew rate increases from 50 V/μs to well over 350 V/μs.

Notice the knee in the Rise and Fall times plot, at approximately 6 V_{p-p} input voltage. Beyond this point the output becomes clipped by the supply rails and the amplifier is no longer operating in a closed loop fashion. The rise and fall times become faster as the dynamic current sources are providing maximum current for slewing. The result of this amplifier architecture is that it slews fast, and allows good control of overshoot for large input signals. This can be seen clearly in the large signal Transient Response plots.

CURRENT LIMIT

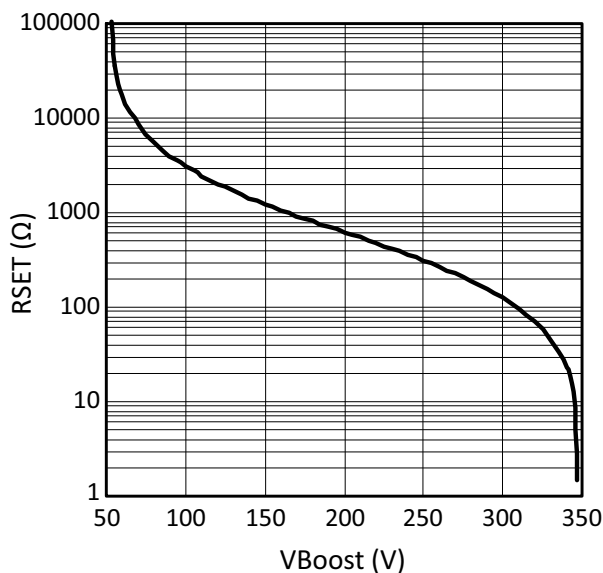
For proper operation, the current limit resistor, R_{LIM}, must be connected as shown in the typical connection diagram. For maximum reliability and protection, the largest resistor value should be used. The maximum practical value for R_{LIM} is about 12 Ω. However, refer to the SOA curve to assist in selecting the optimum value for R_{lim} in the intended application. Current limit may not protect against short circuit conditions with supply voltages over 200 V.

LAYOUT CONSIDERATIONS

Care should be taken to position the R_C / C_C compensation networks close to the amplifier compensation pins. Long loops in these paths pick up noise and increase the likelihood of LC interactions and oscillations.

SMPS OPERATION

Figure 41: SMPS Output vs. RSET



The MP400FC is designed to operate off of a standard voltage rail. Typical values include 12 V, 24 V, or 48 V. The addition of the on-board SMPS eliminates the need to design or purchase a high voltage power supply. The only inputs required by the SMPS are the V_{IN} source. Input and output filter capacitor, and boost voltage set resistor (R_{SET}).

The SMPS output can be adjusted between a minimum of 50 V to a maximum of 350 V. The voltage boost adjustment is independent of V_{IN} . Adjustment to the boost level is made through a resistor from the R_{SET} pin to ground. The resistor value is:

$$R_{SET} = \frac{1.85 \cdot 10^5}{V_{BOOST} - 49.95} - 615$$

Where V_{BOOST} = desired SMPS voltage.

Example:

1. Desired $V_{BOOST} = 160$ V
2. $R_{SET} = 1k$ (1066 by equation)

If R_{SET} is open, V_{BOOST} will be 50 V. If R_{SET} is shorted to ground V_{BOOST} will be limited to 350 V.

Note that while the MP400 SMPS generates a positive voltage from 50 V to 350 V, the amplifier may operate from a variety of supply voltages. Symmetric, asymmetrical and single supply configurations can be used so long as the total supply voltage from $+V_S$ to $-V_S$ does not exceed 350 V. The amplifier performance graphs in this datasheet include some plots taken with symmetrical supplies, but those plots generally apply to all supply configurations.

SMPS OUTPUT CAPACITOR

An external SMPS output filter capacitor is required for proper operation. ESR considerations prevail in the choice of the output filter capacitor. Select the highest value capacitor that meets the following ESR requirement. The minimum value for C_{BOOST} is 100 μ F.

$$ESR = \frac{dVo}{I_{LPK}}$$

Where:

dVo = The maximum acceptable output ripple voltage

I_{LPK} = Peak inductor current = $(1/L) \cdot V_{IN} \cdot t_{on}$

$L = 10^{-6}$ if the internal inductor is used.

V_{IN} = Input voltage of the application.

$t_{on} = \sqrt{2 \cdot I_o \cdot L \cdot ((V_{BOOST} + 0.6 - V_{IN}) / (F_{SW} \cdot V_{IN}^2))}$

V_{BOOST} = The boost supply voltage of the application.

I_o = The maximum continuous output current for the application.

F_{SW} = 100 kHz switching frequency of the MP400FC boost supply.

SMPS INPUT CAPACITOR

An external input capacitor is required. This capacitor should be at least 100 µF.

THERMAL CONSIDERATIONS

For reliable operation the MP400FC will require a heatsink for most applications. When choosing the heatsink the power dissipation in the op amp and the SMPS MOSFET switch (Q2) are both considered. The power dissipation of the op amp is determined in the same manner as any power op amp. The power dissipation of the MOSFET switch (Q2) is the sum of the power dissipation due to conduction and the switching power.

$$P_{D(Q2)} = (I_{IN(pk)}^2 \cdot R_{DS(ON)} \cdot D) + (I_{IN(pk)} \cdot V_{IN} \cdot t_r \cdot F_{SW})$$

Where:

V_{IN} = SMPS input voltage

V_B = SMPS output voltage

I_O = Total SMPS output current

F_{SW} = 100 kHz

$R_{DS(ON)}$ = 0.621 Ω

t_r = 82 x 10⁻⁹s

D = $t_1 \cdot F_{SW}$

$$t_1 = \sqrt{2 \cdot I_O \cdot 10 \times 10^{-6} \cdot \left(\frac{V_B - V_{IN}}{F_{SW} \cdot V_{IN}} \right)}$$

$$I_{IN(pk)} = \frac{V_B \cdot t_d}{10 \times 10^{-6}}$$

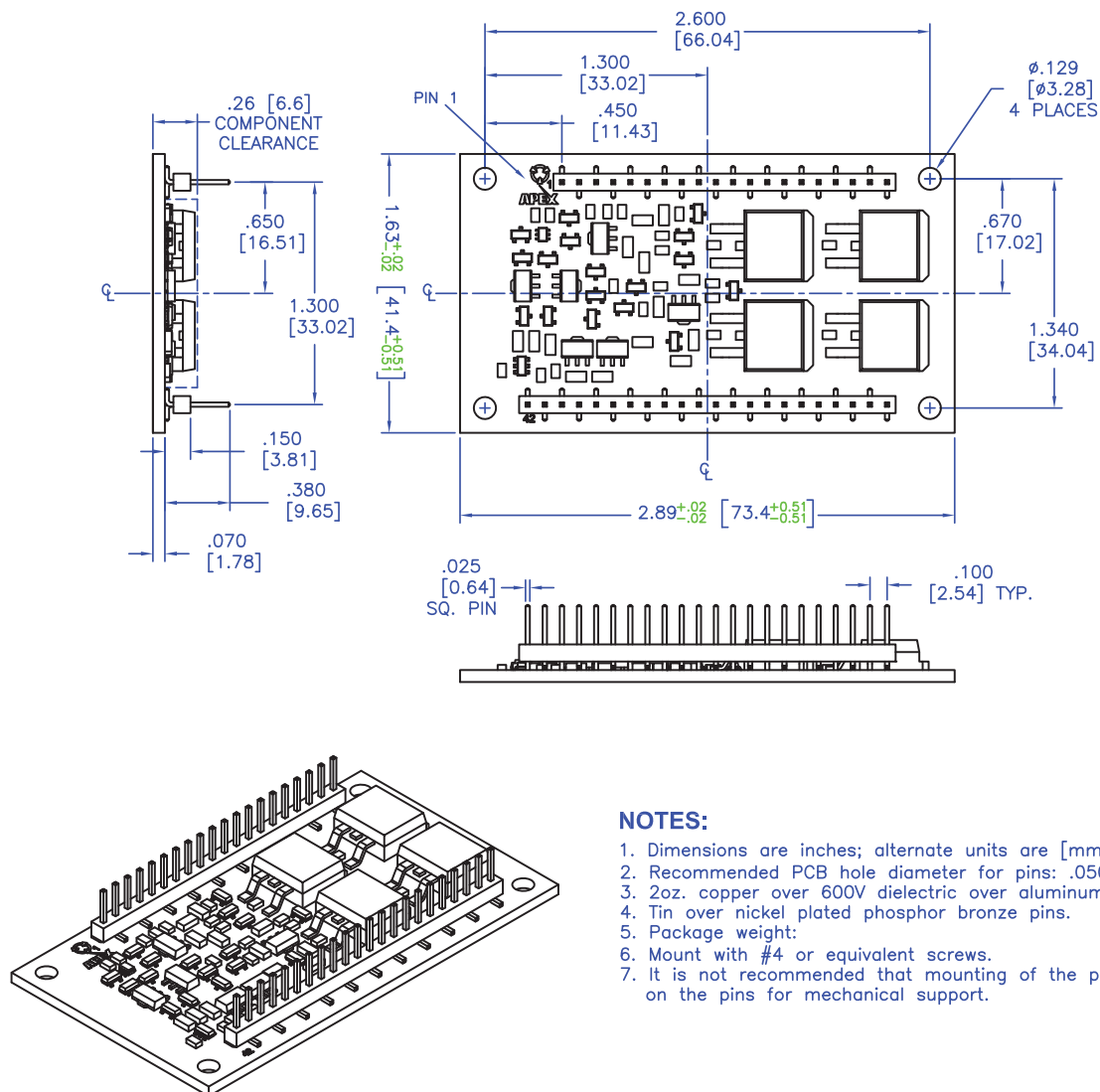
$$t_d = t_1 \cdot \left(\frac{V_B}{V_B - V_{IN}} \right) - t_1$$

MP400FC

PACKAGE OPTIONS

Part Number	Apex Package Style	Description
MP400FC	FC	42-pin DIP

PACKAGE STYLE FC



NOTES:

1. Dimensions are inches; alternate units are [mm].
2. Recommended PCB hole diameter for pins: .050 [1.27].
3. 2oz. copper over 600V dielectric over aluminum substrate.
4. Tin over nickel plated phosphor bronze pins.
5. Package weight:
6. Mount with #4 or equivalent screws.
7. It is not recommended that mounting of the package rely on the pins for mechanical support.

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