![ST logo]

# VB409
# VB409SP

## HIGH VOLTAGE REGULATOR POWER I.C.
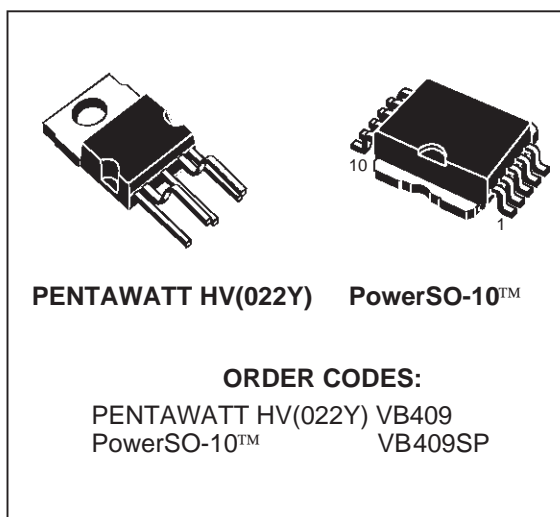
| TYPE | $I_{CL(in)}$ | $I_{CL(out)}$ | $V_{OUT}$ |
|------|---------|----------|---------|
| VB409 | 0.8 A | 70 mA | 5V ± 5% |
| VB409SP | | | |

■ NO HIGH VOLTAGE EXTERNAL CAPACITOR
■ 5 V DC REGULATED OUTPUT VOLTAGE
■ OUTPUT CURRENT LIMITED TO 70 mA
■ THERMAL SHUT-DOWN PROTECTION
■ INPUT OVERCURRENT PROTECTION
■ POWER DISSIPATION INTERNALLY LIMITED



**PENTAWATT HV(022Y)**     **PowerSO-10™**

### ORDER CODES:

PENTAWATT HV(022Y) VB409
PowerSO-10™                VB409SP

### DESCRIPTION

The VB409 VB409SP are fully protected positive voltage regulator designed in STMicroelectronics High Voltage VIPower™ technology. The devices can be connected directly to the rectified mains (110V/230V). The devices are well suited for applications powered from the AC mains and requiring a 5V DC regulated output voltage without galvanic insulation. VB409, VB409SP provides up to 70 mA output current (internally limited) at 5V. The included over current and thermal shutdown provide protection for the device.

### BLOCK DIAGRAM
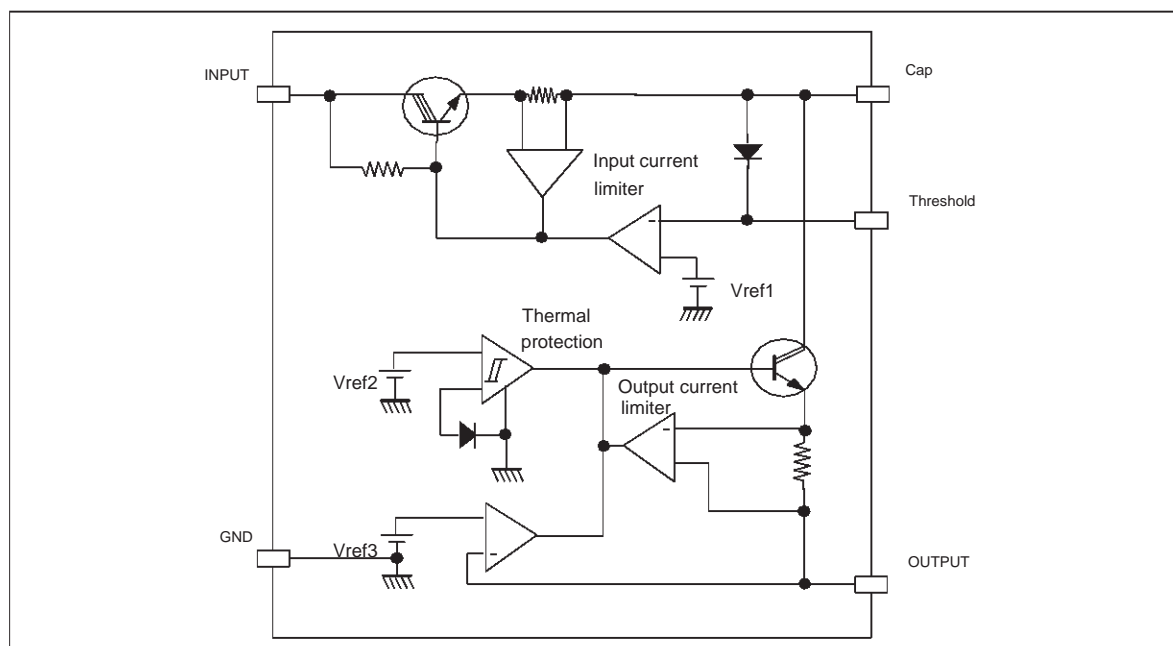
## ABSOLUTE MAXIMUM RATING

| Symbol | Parameter | Value | Unit |
|---|---|---|---|
| $\Delta V_{IN,OUT}$ | Input to output voltage | - 0.2 to 420 | V |
| $I_{OUT}$ | Output current | Internally limited | mA |
| $P_{TOT}$ | Power dissipation at $T_C$=25°C | Internally limited | W |
| $I_{IN}$ | Input current | Internally limited | mA |
| $T_j$ | Junction operating temperature | - 40 to 125 | °C |
| $T_{STG}$ | Storage temperature | - 55 to 150 | °C |

## THERMAL DATA

| Symbol | Parameter | | Value | | Unit |
|---|---|---|---|---|---|
| | | | PENTAWATT | POWERSO-10 | Unit |
| $R_{thj-amb}$ | Thermal resistance junction-ambient | (MAX) | 60 | 50 | °C/W |
| $R_{thj-case}$ | Thermal resistance junction-case | (MAX) | 1.1 | | °C/W |

## CONNECTION DIAGRAM (TOP VIEW)



POWERSO-10

PENTAWATT HV(022Y)
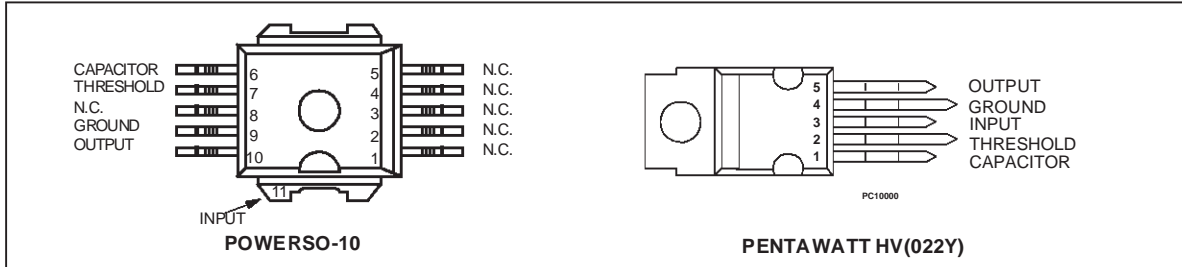
## ELECTRICAL CHARACTERISTICS ($V_{IN}$=230Vr.m.s.; 50Hz; $C_1$=100µF; $V_1$=50V (See Fig. 2); $I_{OUT}$ =25mA; $V_{OUT}$=5V; -25°C<$T_j$<125°C) (unless otherwise specified)

| Symbol | Parameter | Test Conditions | Min | Typ | Max | Unit |
|---|---|---|---|---|---|---|
| $V_{IN(ac)}$ | Input voltage a.c. | | 15 | | 230 | Vr.m.s. |
| $BV_{IN-GND}$ | Breakdown voltage input-ground in off state | | 650 | | | V |
| $f_{IN}$ | Input frequency | | 0 | | 1 | kHz |
| $V_{OUT}$ | Output voltage | | 4.75 | 5 | 5.25 | V |
| $\Delta V_{OUT}/\Delta V_{cap}$ | Cap regulation | $V_{cap}$=8 to 12V; $V_{IN}$=0V; $T_j$=25°C | | | 7 | mV/V |
| $\Delta V_{OUT}/\Delta I_{OUT}$ | Load regulation | $I_{OUT}$=1 to 40mA; $V_{cap}$=10V; $T_j$=25°C | | | 500 | µV/mA |
| $I_{CL(out)}$ | Output current limit | $T_j$=25°C | 70 | | 90 | mA |
| $T_{jsh}$ | Junction temperature shutdown limit | | | 140 | 150 | °C |
| $\Delta T_{jsh}$ | Junction temperature shutdown hysteresis | | | 35 | | °C |
| $I_d$ | Quiescent current | $T_j$=25°C; $I_{OUT}$=0A | | | 2 | mA |
| $V_d$ | Dropout voltage ($V_{cap}$ to $V_{OUT}$) | $T_j$=25°C | | | 3 | V |
| $I_{CL(in)}$ | Input clamp current | | 0.8 | | 2 | A |
| $\Delta V_{cap}/\Delta T$ | Drift of capacitor pin voltage in temperature | | | -15 | | mV/°C |
| $V_{cap(max)}$ | Max clamped voltage on cap pin | | 12 | | 14.5 | V |
| $V_{ref1}$ | Reference threshold Voltage | | 10 | 10.5 | 11 | V |
| $I_{th}$ | Current on threshold pin | | | 100 | | µA |

**OPERATION DESCRIPTION**

The VB409, VB409SP contain two separate stages, as shown in the block diagram. The first stage is a preregulator that translates the high rectified mains voltage to a low voltage and charges an external electrolytic capacitor. The second stage is a simple 5V regulator. The typical operating waveforms are shown in Figure 2. The device may be driven by a half wave (110 or 230 Vr.m.s.) or by a full wave using a bridge rectifier. Current flow through the preregulator stage is provided by the trilinton only during a conduction angle, at both the start and the end of each half cycle. This angle is set by adjusting the external resistor divider (R1 and R2), in order to set the time $t_1$ at which voltage at the threshold pin reaches the internal threshold $V_{ref1}$ (see Figure 2a). When the threshold pin voltage gets over $V_{ref1}$, the series trilinton is switched off and remains off until voltage at the threshold pin again drops below the internal threshold. Using this technique, energy is drawn from the AC mains only during the low voltage portions of each positive half cycle, thus reducing the dissipation in the first stage. During the conduction angle, current provided by the trilinton is used to supply the load and to charge the capacitor C1. In such a way, when the trilinton switches off, the load receives the required current by the capacitor discharge. For this reason it is important to set properly the conduction angle: during this period C1 has to reach a sufficient charge to guarantee that, at the end of discharging, the voltage drop

between the capacitor and the output pin is over 2V. Assuming that conduction angle has been set, two different possibilities can occur:

1) C1 value is such to reach $V_{cap(max)}$ within the conduction angle. As the comparator also senses C1 voltage, when $V_{cap}$ gets over $V_{ref1}$, the trilinton would switch off. But doing this, the capacitor would discharge through the load so reducing its voltage. As soon as $V_{cap}$ drops below $V_{ref1}$, the trilinton switches on. As consequence the trilinton reaches a stable condition limiting the current to a value sufficient to supply the load and hold the capacitor voltage just below $V_{cap(max)}$ (see figures 2b and 2c).

2) C1 value is such to reach $V_{cap(max)}$ outside the conduction angle. In this case the trilinton doesn't reduce the current, but hold it to a constant value ($I_{CL(in)}$) during the whole conduction angle (see figures 3a and 3b).

As there are two conduction angles for each half cycle, the capacitor is recharged twice during each period. In such a way the capacitor voltage has a small ripple and, consequently, it needs a small current to regenerate its charge. The device has integrated current limit and thermal shutdown protections. The thermal shutdown turns the low voltage stage off, if the die temperature exceeds a predetermined value. Hysteresis in the thermal sense circuit holds the device off until the die temperature cools down.
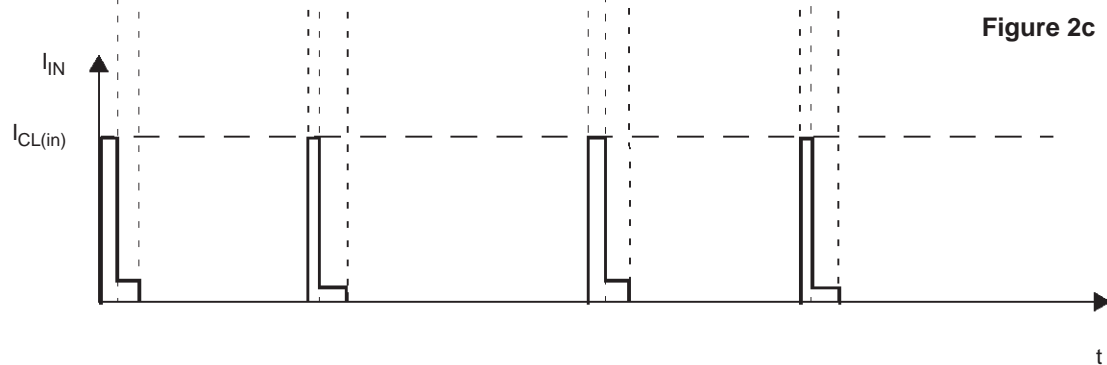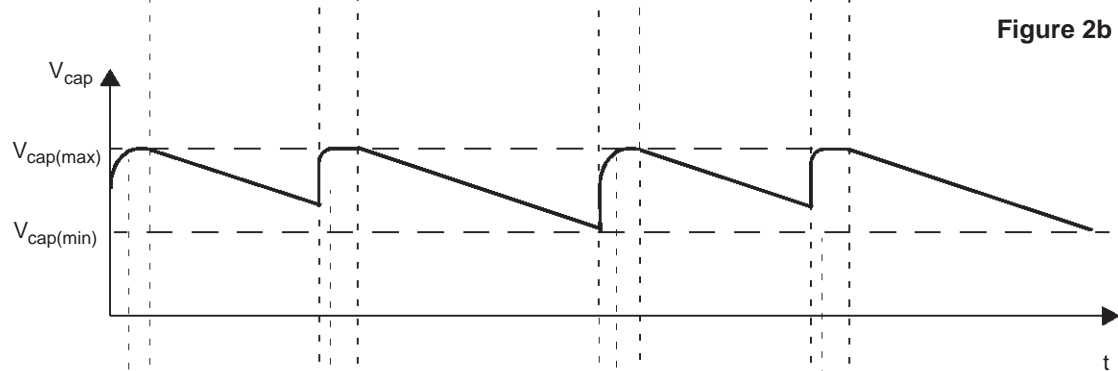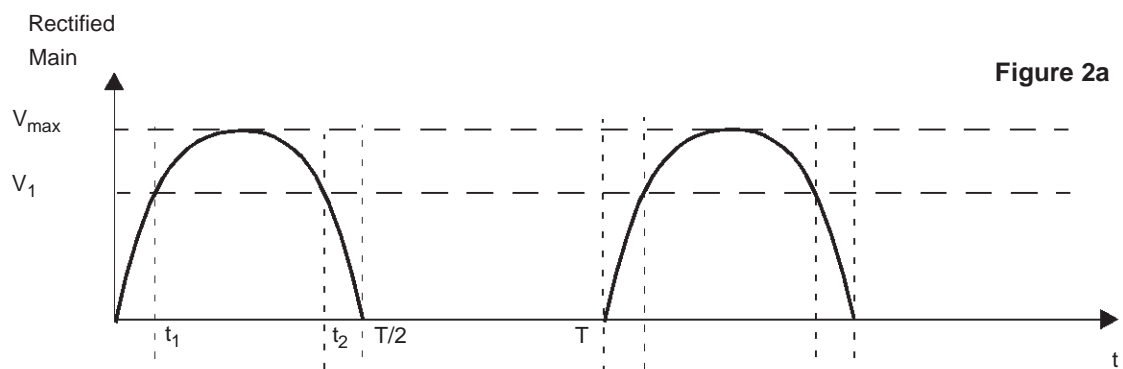
**Figure 1:** Application scheme
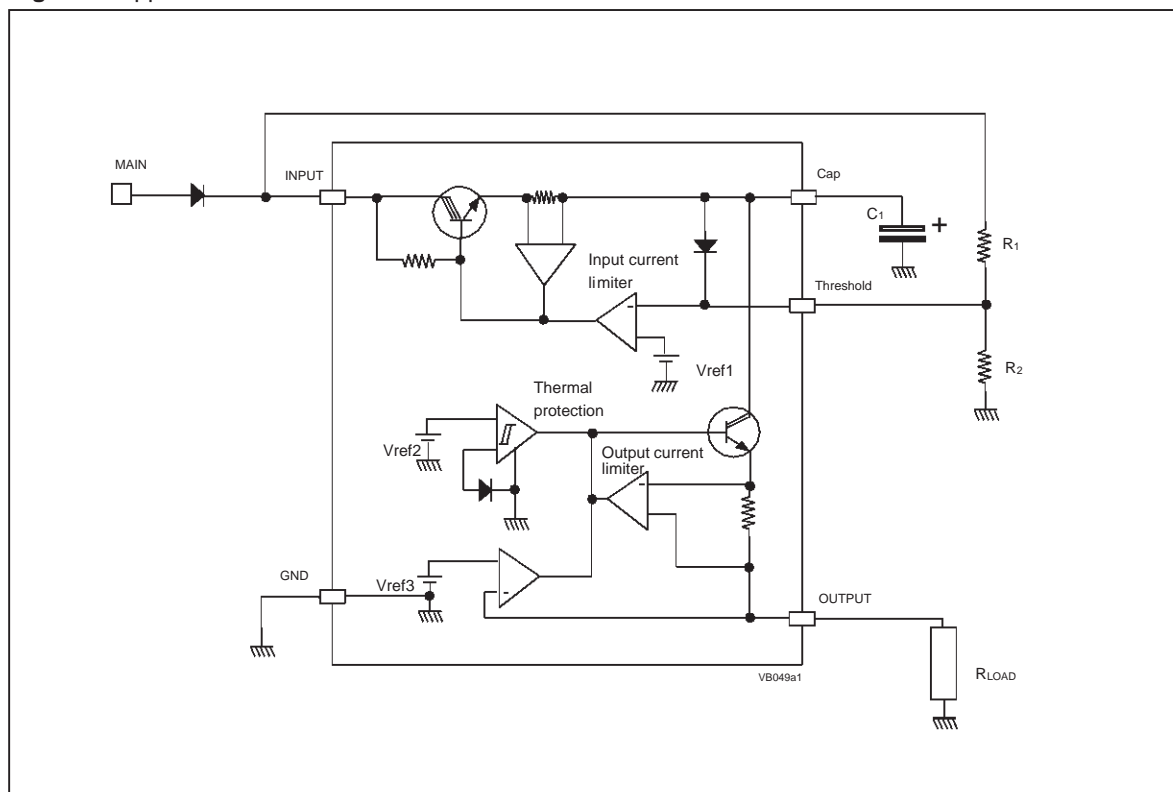


## APPLICATION EXAMPLE

(without heatsink; R1=1M$\Omega$; C1=47$\mu$F)

| $I_{OUT}$ | R2 | $P_{AV}$ |
|---|---|---|
| 10 mA | 560 K$\Omega$ | 0.32 W |
| 15 mA | 470 K$\Omega$ | 0.49 W |
| 20 mA | 390 K$\Omega$ | 0.67 W |

(without heatsink; R1=1M$\Omega$; C1=100$\mu$F)

| $I_{OUT}$ | R2 | $P_{AV}$ |
|---|---|---|
| 20mA | 390 K$\Omega$ | 0.70 W |
| 25mA | 330 K$\Omega$ | 0.92 W |
| 30mA | 270 K$\Omega$ | 1.20 W |
| 35mA | 220 K$\Omega$ | 1.53 W |
| 40mA | 180 K$\Omega$ | 1.92 W |

**Figure 2:** typical waveforms



**Figure 2a**

Rectified Main

$V_{max}$

$V_1$

$t_1$   $t_2$   T/2   T   t

**Figure 2b**

$V_{cap}$

$V_{cap(max)}$

$V_{cap(min)}$

t

**Figure 2c**

$I_{IN}$

$I_{CL(in)}$

t

**Figure 2d**

$I_{OUT}$

t

## AVERAGE POWER CALCULATION IN WORST CASE

As before explained, the device also senses the preregulator voltage ($V_{cap}$), so that as soon as the capacitor reaches its maximum voltage, the trilinton reduces the current so limiting furtherly power dissipation. On the contrary if the capacitor doesn't reach the maximum value, the trilinton supplies current at a steady value ($I_{max}$) during the whole conduction angle. This is obviously the worst case, in which the average power dissipation is maximum.



**Figure 3a**

**Figure 3b**
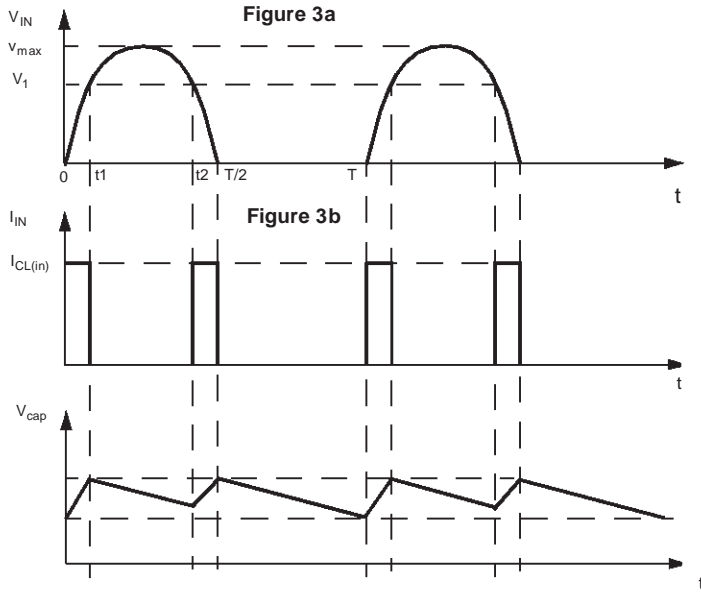
$$V_{IN} = \begin{cases} V_{max} \cdot \sin\left(\frac{2\pi}{T} \cdot t\right) & 0 \leq t \leq \frac{T}{2} \\ 0 & \frac{T}{2} \leq t \leq T \end{cases}$$

$$I_{IN} = \begin{cases} I_{CL(in)} \cdot & \begin{array}{l} 0 \leq t \leq t1 \\ t2 \leq t \leq \frac{T}{2} \end{array} \\ 0 & \text{elsewhere} \end{cases}$$

Assuming that

$$[0,t1] = [t2,\tfrac{T}{2}]$$

are the conduction angles, it results:

$$P_{AV} = \frac{1}{T} \cdot \int_0^T (V_{IN} \cdot I_{IN})dt = \frac{1}{T} \cdot \left[ \int_0^{t1} (V_{IN} \cdot I_{CL(in)})dt + \int_{t2}^{\frac{T}{2}} (V_{IN} \cdot I_{CL(in)})dt \right] =$$

$$= \frac{I_{CL(in)} \cdot V_{max}}{T} \cdot \left[ \int_0^{t1} \sin\left(\frac{2\pi}{T} \cdot t\right)dt + \int_{t2}^{\frac{T}{2}} \sin\left(\frac{2\pi}{T} \cdot t\right)dt \right] = \frac{I_{CL(in)} \cdot V_{max}}{T} \cdot \left[ 2\int_0^{t1} \sin\left(\frac{2\pi}{T} \cdot t\right)dt \right] =$$

$$= 2\frac{I_{CL(in)} \cdot V_{max}}{T} \cdot \frac{T}{2\pi} \cdot \left[ -\cos\left(\frac{2\pi}{T} \cdot t1\right) + \cos 0 \right] = \frac{I_{CL(in)} \cdot V_{max}}{\pi}\left[ 1 - \sqrt{1 - \sin^2\left(\frac{2\pi}{T} \cdot t1\right)} \right] =$$

As for t1:

$$\frac{V_1}{V_{max}} = \sin\left(\frac{2\pi}{T} \cdot t1\right)$$

it follows:

$$\boxed{P_{AV} = \frac{I_{CL(in)} \cdot V_{max}}{\pi} \cdot \left[ 1 - \sqrt{1 - \left(\frac{V_1}{V_{max}}\right)^2} \right]}$$

Where

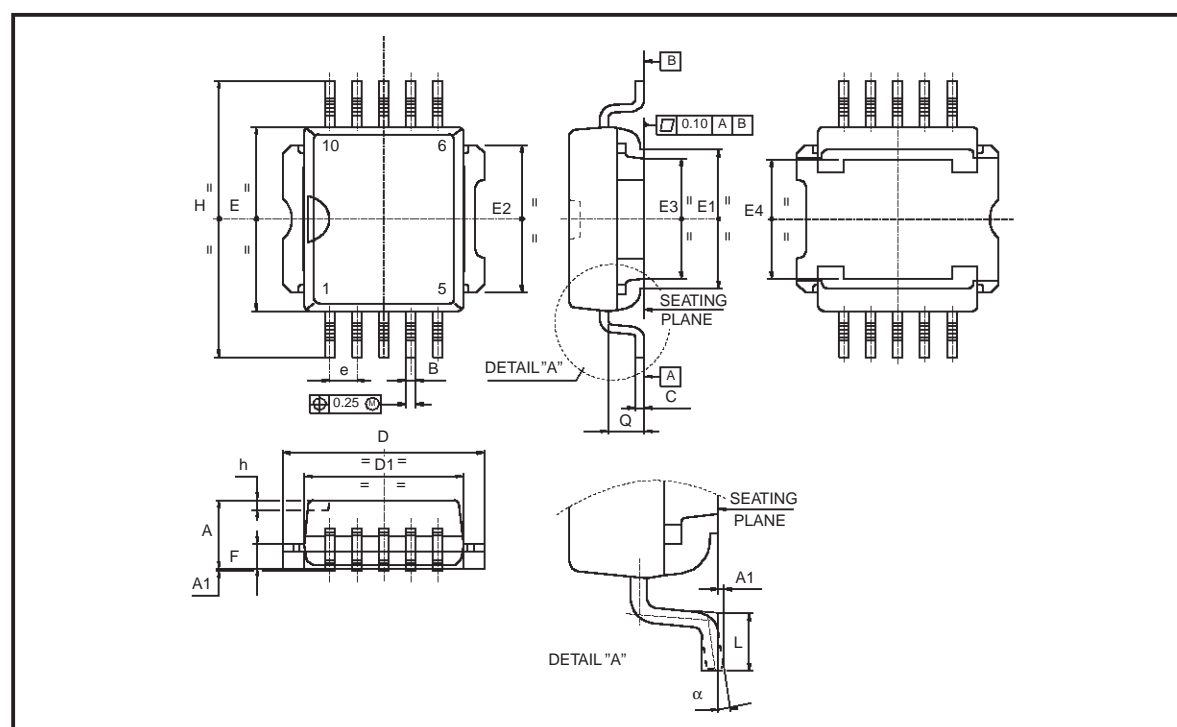$$V_1 = V_{ref1} \cdot \left(1 + \frac{R1}{R2}\right)$$

## PENTAWATT HV 022Y (VERTICAL HIGH PITCH) MECHANICAL DATA

| DIM. | mm. | | | inch | | |
|------|------|-----|------|------|------|------|
| | MIN. | TYP | MAX. | MIN. | TYP. | MAX. |
| A | 4.30 | | 4.80 | 0.169 | | 0.189 |
| C | 1.17 | | 1.37 | 0.046 | | 0.054 |
| D | 2.40 | | 2.80 | 0.094 | | 0.110 |
| E | 0.35 | | 0.55 | 0.014 | | 0.022 |
| F | 0.60 | | 0.80 | 0.024 | | 0.031 |
| G1 | 4.91 | | 5.21 | 0.193 | | 0.205 |
| G2 | 7.49 | | 7.80 | 0.295 | | 0.307 |
| H1 | 9.30 | | 9.70 | 0.366 | | 0.382 |
| H2 | | | 10.40 | | | 0.409 |
| H3 | 10.05 | | 10.40 | 0.396 | | 0.409 |
| L | 16.42 | | 17.42 | 0.646 | | 0.686 |
| L1 | 14.60 | | 15.22 | 0.575 | | 0.599 |
| L3 | 20.52 | | 21.52 | 0.808 | | 0.847 |
| L5 | 2.60 | | 3.00 | 0.102 | | 0.118 |
| L6 | 15.10 | | 15.80 | 0.594 | | 0.622 |
| L7 | 6.00 | | 6.60 | 0.236 | | 0.260 |
| M | 2.50 | | 3.10 | 0.098 | | 0.122 |
| M1 | 5.00 | | 5.70 | 0.197 | | 0.224 |
| R | | 0.50 | | | 0.020 | |
| V4 | | 90° | | | 90° | |
| Diam. | 3.70 | | 3.90 | 0.146 | | 0.154 |
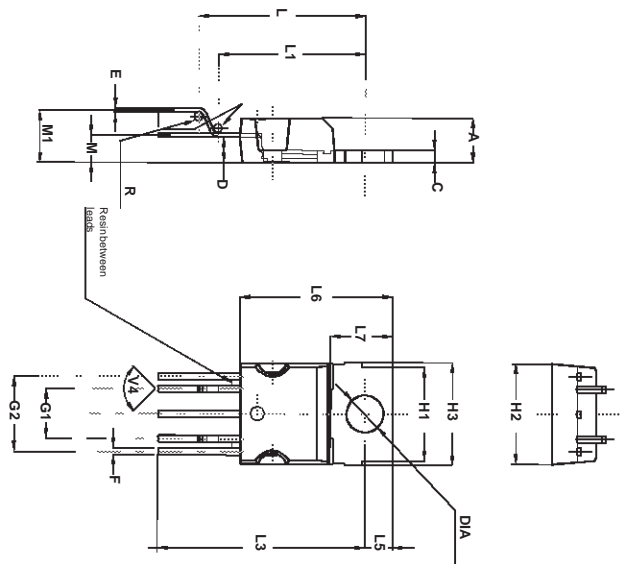
## PowerSO-10™ MECHANICAL DATA

| DIM. | mm. | | | inch | | |
|------|-----|-----|------|------|------|------|
| | MIN. | TYP | MAX. | MIN. | TYP. | MAX. |
| A | 3.35 | | 3.65 | 0.132 | | 0.144 |
| A1 | 0.00 | | 0.10 | 0.000 | | 0.004 |
| B | 0.40 | | 0.60 | 0.016 | | 0.024 |
| c | 0.35 | | 0.55 | 0.013 | | 0.022 |
| D | 9.40 | | 9.60 | 0.370 | | 0.378 |
| D1 | 7.40 | | 7.60 | 0.291 | | 0.300 |
| E | 9.30 | | 9.50 | 0.366 | | 0.374 |
| E1 | 7.20 | | 7.40 | 0.283 | | 0.291 |
| E2 | 7.20 | | 7.60 | 0.283 | | 300 |
| E3 | 6.10 | | 6.35 | 0.240 | | 0.250 |
| E4 | 5.90 | | 6.10 | 0.232 | | 0.240 |
| e | | 1.27 | | | 0.050 | |
| F | 1.25 | | 1.35 | 0.049 | | 0.053 |
| H | 13.80 | | 14.40 | 0.543 | | 0.567 |
| h | | 0.50 | | | 0.002 | |
| L | 1.20 | | 1.80 | 0.047 | | 0.070 |
| Q | | 1.70 | | | 0.067 | |
| $\alpha$ | 0º | | 8º | | | |