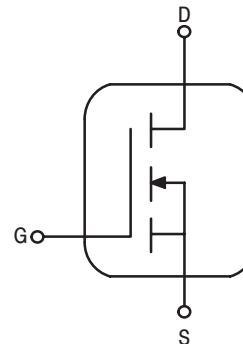


**The RF MOSFET Line**

**RF Power Field Effect Transistor**  
**N-Channel Enhancement-Mode Lateral MOSFETs**

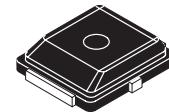
The MRF1517T1 is designed for broadband commercial and industrial applications at frequencies to 520 MHz. The high gain and broadband performance of this device makes it ideal for large-signal, common source amplifier applications in 7.5 volt portable FM equipment.

- Specified Performance @ 520 MHz, 7.5 Volts
  - Output Power — 8 Watts
  - Power Gain — 11 dB
  - Efficiency — 55%
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- Excellent Thermal Stability
- Capable of Handling 20:1 VSWR, @ 9.5 Vdc, 520 MHz, 2 dB Overdrive
- Broadband UHF/VHF Demonstration Amplifier Information Available Upon Request
- RF Power Plastic Surface Mount Package
- Available in Tape and Reel.  
T1 Suffix = 1,000 Units per 12 mm, 7 Inch Reel.



**MRF1517T1**

**520 MHz, 8 W, 7.5 V  
LATERAL N-CHANNEL  
BROADBAND  
RF POWER MOSFET**



**CASE 466-02, STYLE 1  
(PLD-1.5)**  
**PLASTIC**

**MAXIMUM RATINGS**

Rating	Symbol	Value	Unit
Drain-Source Voltage (1)	$V_{DSS}$	25	Vdc
Gate-Source Voltage	$V_{GS}$	$\pm 20$	Vdc
Drain Current — Continuous	$I_D$	4	Adc
Total Device Dissipation @ $T_C = 25^\circ\text{C}$ (2) Derate above $25^\circ\text{C}$	$P_D$	62.5 0.50	Watts W/ $^\circ\text{C}$
Storage Temperature Range	$T_{stg}$	-65 to +150	$^\circ\text{C}$
Operating Junction Temperature	$T_J$	150	$^\circ\text{C}$

**THERMAL CHARACTERISTICS**

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	2	$^\circ\text{C}/\text{W}$

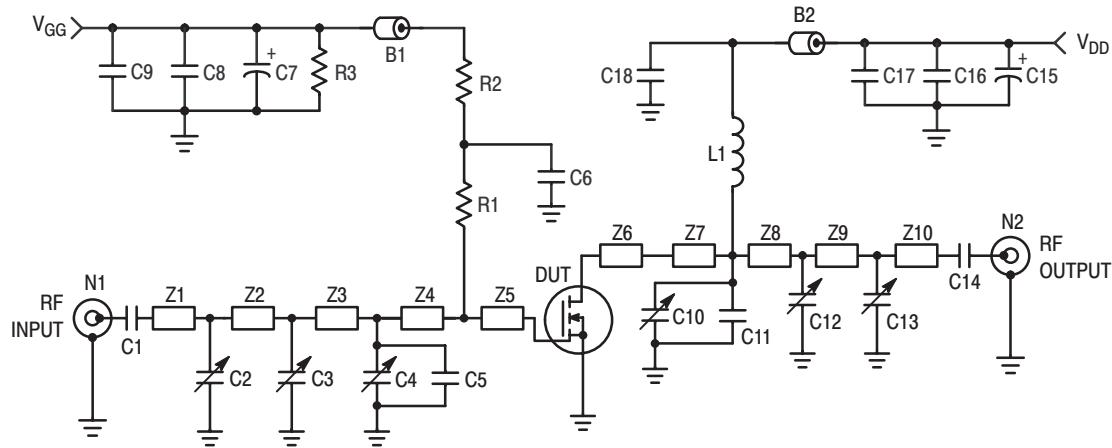
(1) Not designed for 12.5 volt applications.

(2) Calculated based on the formula  $P_D = \frac{T_J - T_C}{R_{\theta JC}}$

**NOTE — CAUTION —** MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.

**ELECTRICAL CHARACTERISTICS** ( $T_C = 25^\circ\text{C}$  unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
<b>OFF CHARACTERISTICS</b>					
Zero Gate Voltage Drain Current ( $V_{DS} = 35$ Vdc, $V_{GS} = 0$ )	$I_{DSS}$	—	—	1	$\mu\text{A}$
Gate-Source Leakage Current ( $V_{GS} = 10$ Vdc, $V_{DS} = 0$ )	$I_{GSS}$	—	—	1	$\mu\text{A}$
<b>ON CHARACTERISTICS</b>					
Gate Threshold Voltage ( $V_{DS} = 7.5$ Vdc, $I_D = 120 \mu\text{A}$ )	$V_{GS(\text{th})}$	1.0	1.7	2.1	Vdc
Drain-Source On-Voltage ( $V_{GS} = 10$ Vdc, $I_D = 1$ Adc)	$V_{DS(\text{on})}$	—	0.5	—	Vdc
Forward Transconductance ( $V_{DS} = 10$ Vdc, $I_D = 2$ Adc)	$g_{fs}$	0.9	—	—	S
<b>DYNAMIC CHARACTERISTICS</b>					
Input Capacitance ( $V_{DS} = 7.5$ Vdc, $V_{GS} = 0$ , $f = 1$ MHz)	$C_{iss}$	—	66	—	pF
Output Capacitance ( $V_{DS} = 7.5$ Vdc, $V_{GS} = 0$ , $f = 1$ MHz)	$C_{oss}$	—	38	—	pF
Reverse Transfer Capacitance ( $V_{DS} = 7.5$ Vdc, $V_{GS} = 0$ , $f = 1$ MHz)	$C_{rss}$	—	6	—	pF
<b>FUNCTIONAL TESTS</b> (In Motorola Test Fixture)					
Common-Source Amplifier Power Gain ( $V_{DD} = 7.5$ Vdc, $P_{out} = 8$ Watts, $I_{DQ} = 150$ mA, $f = 520$ MHz)	$G_{ps}$	10	11	—	dB
Drain Efficiency ( $V_{DD} = 7.5$ Vdc, $P_{out} = 8$ Watts, $I_{DQ} = 150$ mA, $f = 520$ MHz)	$\eta$	50	55	—	%



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	R1	15 $\Omega$ , 0805 Chip Resistor
C1	300 pF, 100 mil Chip Capacitor	R2	1.0 k $\Omega$ , 1/8 W Resistor
C2, C3, C4, C10, C12, C13	0 to 20 pF, Trimmer Capacitor	R3	33 k $\Omega$ , 1/2 W Resistor
C5, C11	43 pF, 100 mil Chip Capacitor	Z1	0.315" x 0.080" Microstrip
C6, C18	120 pF, 100 mil Chip Capacitor	Z2	1.415" x 0.080" Microstrip
C7, C15	10 $\mu$ F, 50 V Electrolytic Capacitor	Z3	0.322" x 0.080" Microstrip
C8, C16	0.1 $\mu$ F, 100 mil Chip Capacitor	Z4	0.022" x 0.080" Microstrip
C9, C17	1,000 pF, 100 mil Chip Capacitor	Z5, Z6	0.260" x 0.223" Microstrip
C14	330 pF, 100 mil Chip Capacitor	Z7	0.050" x 0.080" Microstrip
L1	55.5 nH, 5 Turn, Coilcraft	Z8	0.625" x 0.080" Microstrip
N1, N2	Type N Flange Mount	Z9	0.800" x 0.080" Microstrip
		Z10	0.589" x 0.080" Microstrip
		Board	Glass Teflon®, 31 mils, 2 oz. Copper

Figure 1. 480 – 520 MHz Broadband Test Circuit

#### TYPICAL CHARACTERISTICS, 480 – 520 MHz

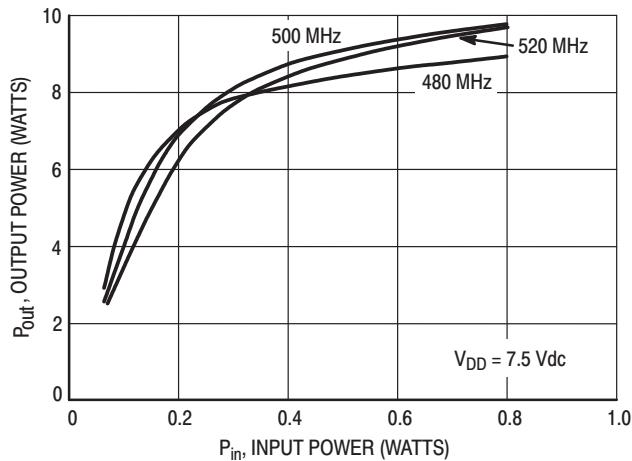


Figure 2. Output Power versus Input Power

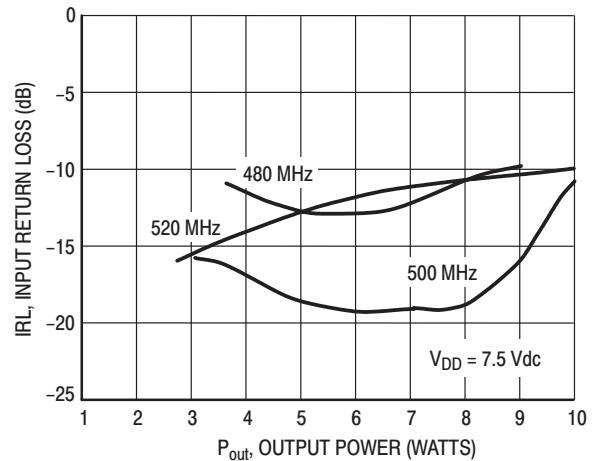
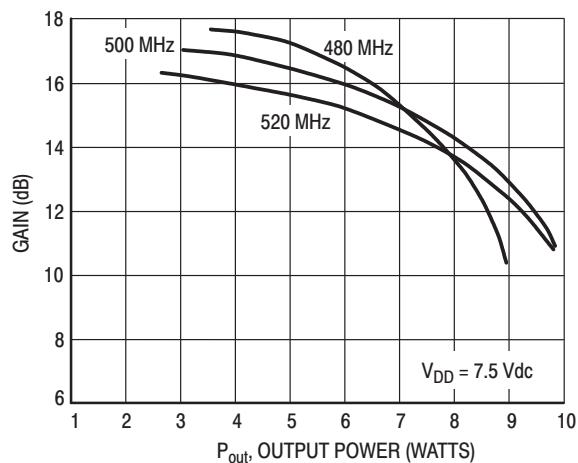
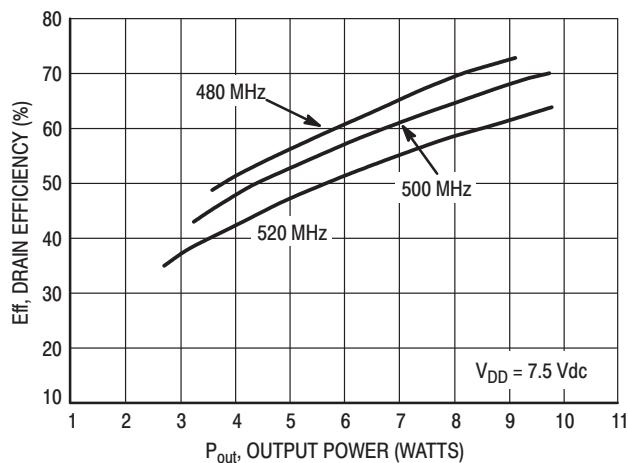


Figure 3. Input Return Loss versus Output Power

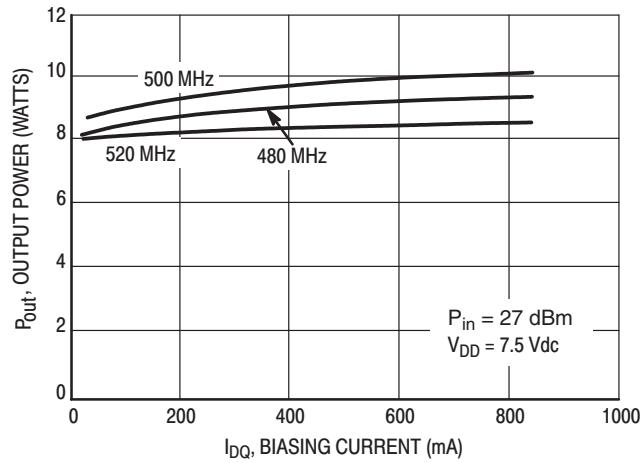
## TYPICAL CHARACTERISTICS, 480 – 520 MHz



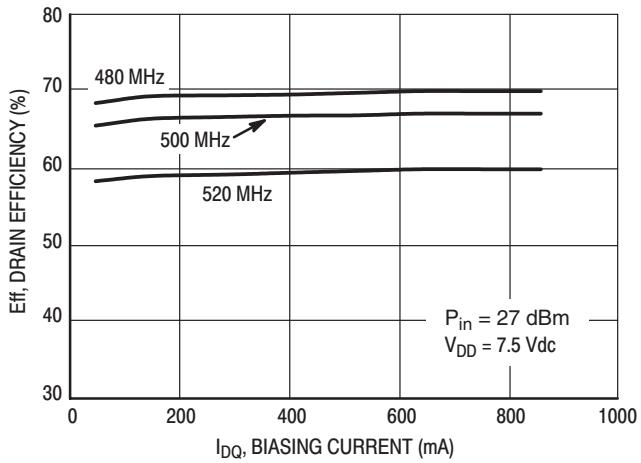
**Figure 4. Gain versus Output Power**



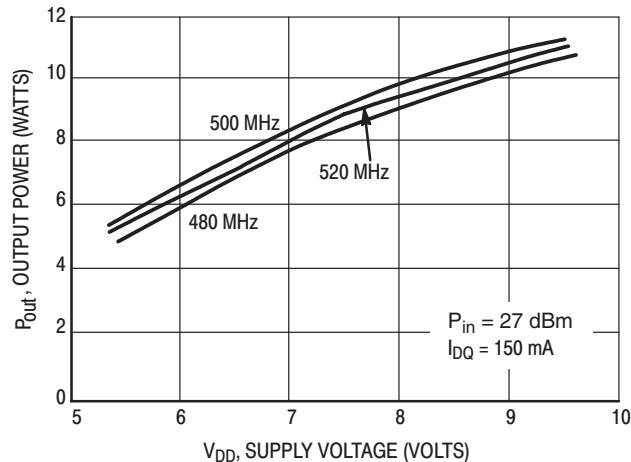
**Figure 5. Drain Efficiency versus Output Power**



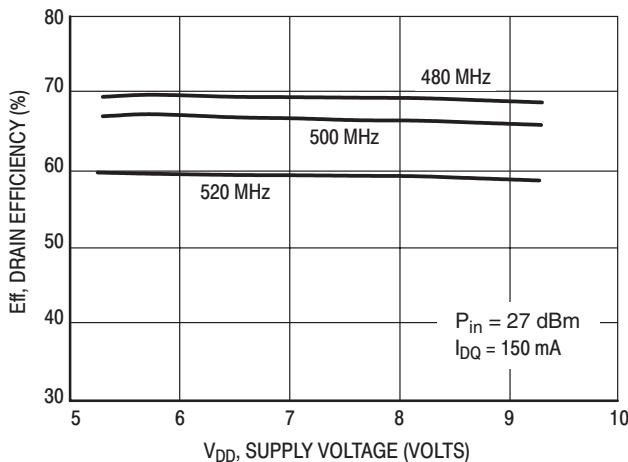
**Figure 6. Output Power versus Biasing Current**



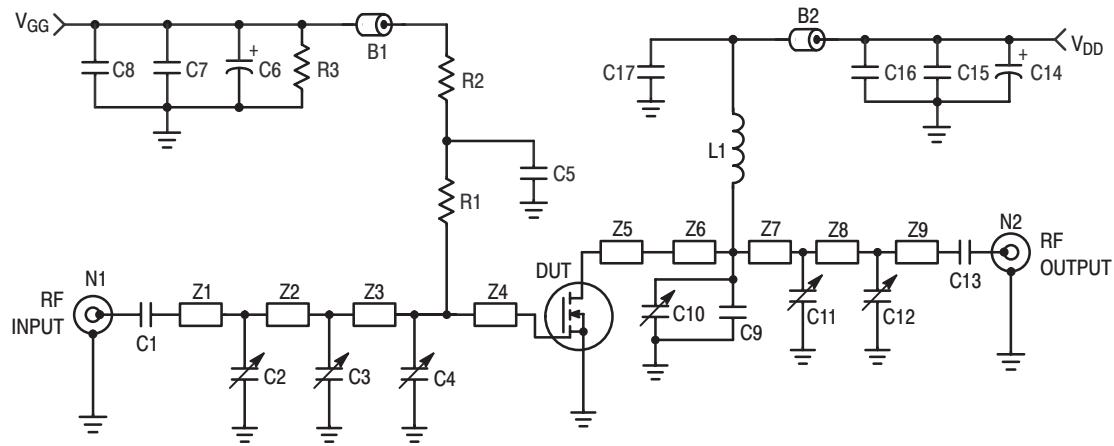
**Figure 7. Drain Efficiency versus Biasing Current**



**Figure 8. Output Power versus Supply Voltage**



**Figure 9. Drain Efficiency versus Supply Voltage**



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	R1	12 $\Omega$ , 0805 Chip Resistor
C1, C13	300 pF, 100 mil Chip Capacitor	R2	1.0 k $\Omega$ , 1/8 W Resistor
C2, C3, C4, C10, C11, C12	0 to 20 pF, Trimmer Capacitor	R3	33 k $\Omega$ , 1/2 W Resistor
C5, C17	130 pF, 100 mil Chip Capacitor	Z1	0.617" x 0.080" Microstrip
C6, C14	10 $\mu$ F, 50 V Electrolytic Capacitor	Z2	0.723" x 0.080" Microstrip
C7, C15	0.1 $\mu$ F, 100 mil Chip Capacitor	Z3	0.513" x 0.080" Microstrip
C8, C16	1,000 pF, 100 mil Chip Capacitor	Z4, Z5	0.260" x 0.223" Microstrip
C9	33 pF, 100 mil Chip Capacitor	Z6	0.048" x 0.080" Microstrip
L1	55.5 nH, 5 Turn, Coilcraft	Z7	0.577" x 0.080" Microstrip
N1, N2	Type N Flange Mount	Z8	1.135" x 0.080" Microstrip
		Z9	0.076" x 0.080" Microstrip
		Board	Glass Teflon®, 31 mils, 2 oz. Copper

Figure 10. 400 – 440 MHz Broadband Test Circuit

#### TYPICAL CHARACTERISTICS, 400 – 440 MHz

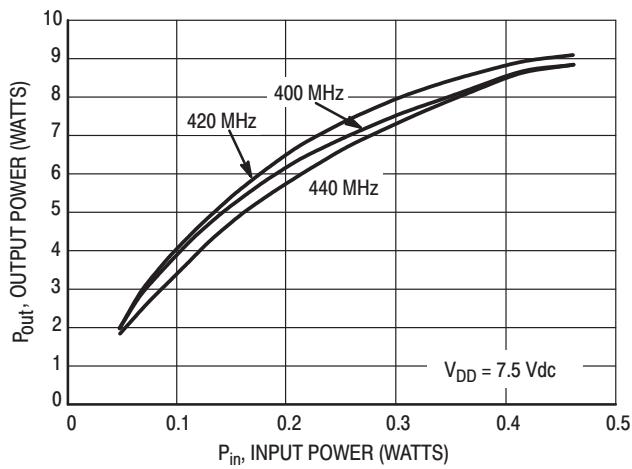


Figure 11. Output Power versus Input Power

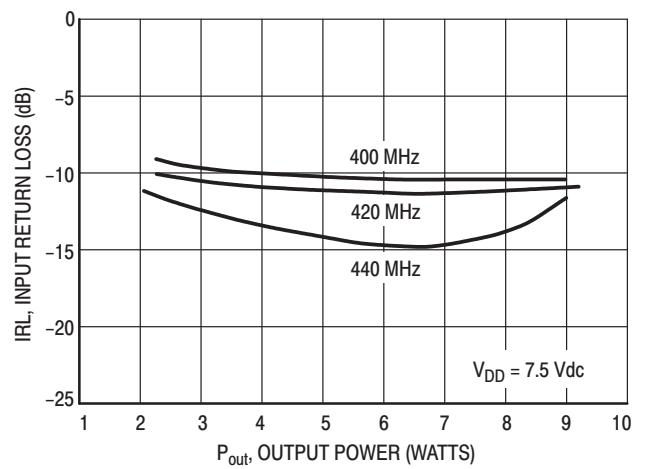


Figure 12. Input Return Loss versus Output Power

## TYPICAL CHARACTERISTICS, 400 – 440 MHz

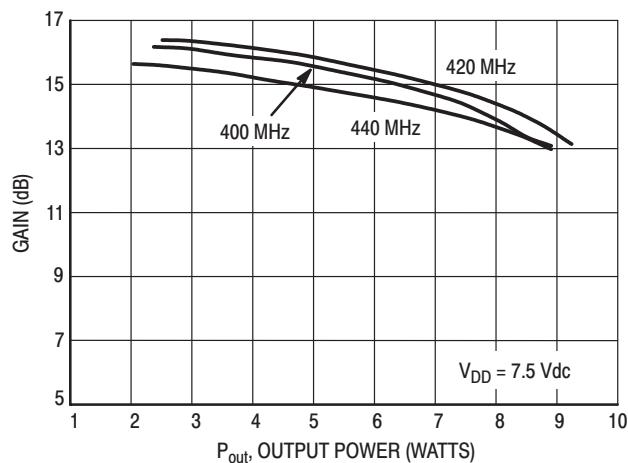


Figure 13. Gain versus Output Power

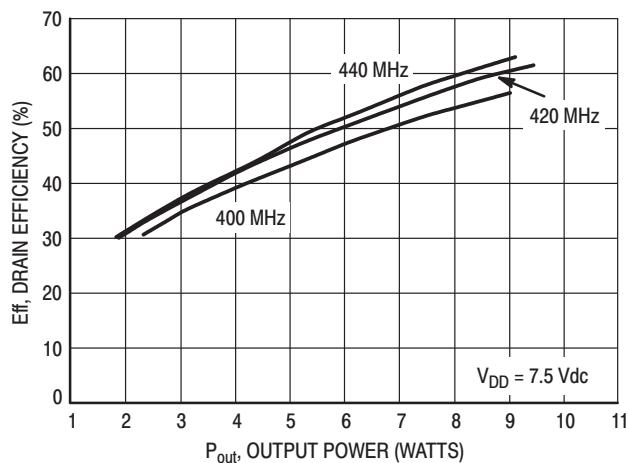


Figure 14. Drain Efficiency versus Output Power

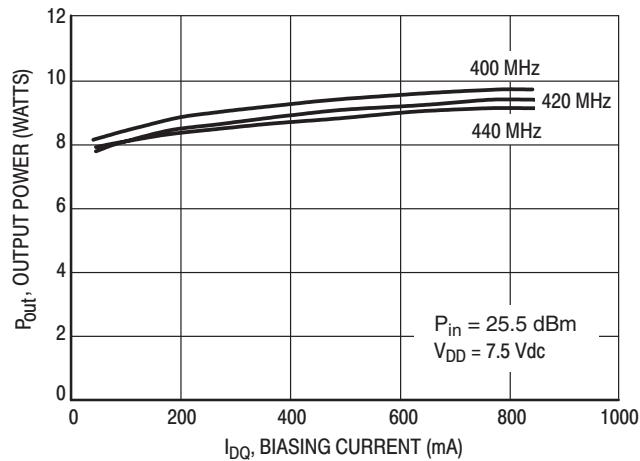


Figure 15. Output Power versus Biasing Current

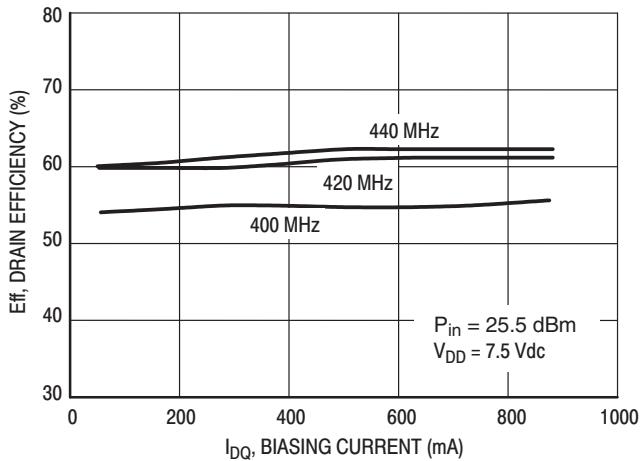


Figure 16. Drain Efficiency versus Biasing Current

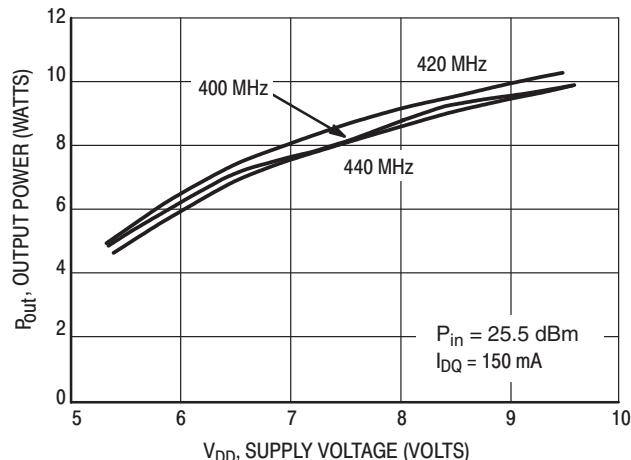


Figure 17. Output Power versus Supply Voltage

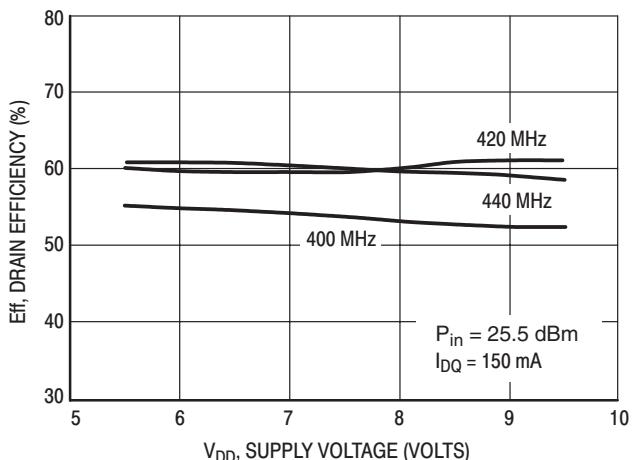
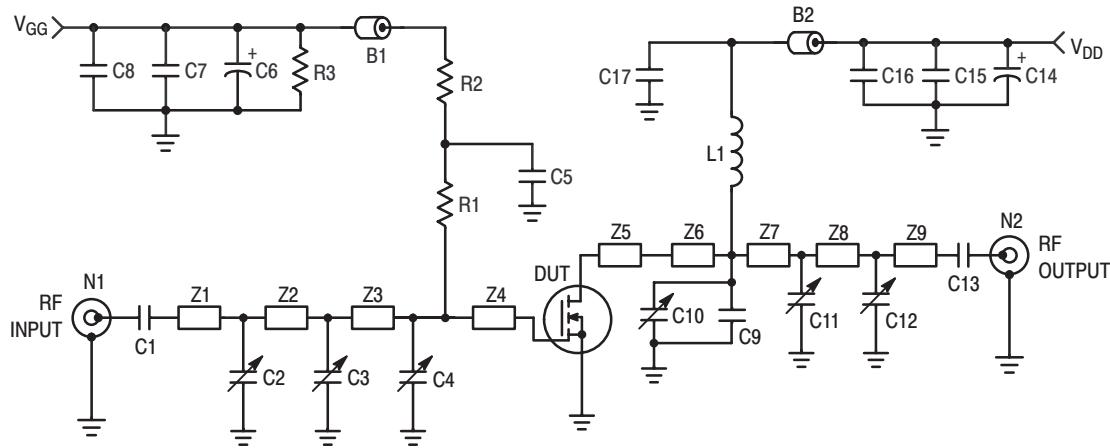


Figure 18. Drain Efficiency versus Supply Voltage



B1, B2	Short Ferrite Bead, Fair Rite Products (2743021446)	R1	15 $\Omega$ , 0805 Chip Resistor
C1	240 pF, 100 mil Chip Capacitor	R2	1.0 k $\Omega$ , 1/8 W Resistor
C2, C3, C4, C10, C11, C12	0 to 20 pF, Trimmer Capacitor	R3	33 k $\Omega$ , 1/2 W Resistor
C5, C17	130 pF, 100 mil Chip Capacitor	Z1	0.471" x 0.080" Microstrip
C6, C14	10 mF, 50 V Electrolytic Capacitor	Z2	1.082" x 0.080" Microstrip
C7, C15	0.1 mF, 100 mil Chip Capacitor	Z3	0.372" x 0.080" Microstrip
C8, C16	1,000 pF, 100 mil Chip Capacitor	Z4, Z5	0.260" x 0.223" Microstrip
C9	39 pF, 100 mil Chip Capacitor	Z6	0.050" x 0.080" Microstrip
C13	330 pF, 100 mil Chip Capacitor	Z7	0.551" x 0.080" Microstrip
L1	55.5 nH, 5 Turn, Coilcraft	Z8	0.825" x 0.080" Microstrip
N1, N2	Type N Flange Mount	Z9	0.489" x 0.080" Microstrip
		Board	Glass Teflon <sup>®</sup> , 31 mils, 2 oz. Copper

Figure 19. 440 – 480 MHz Broadband Test Circuit

#### TYPICAL CHARACTERISTICS, 440 – 480 MHz

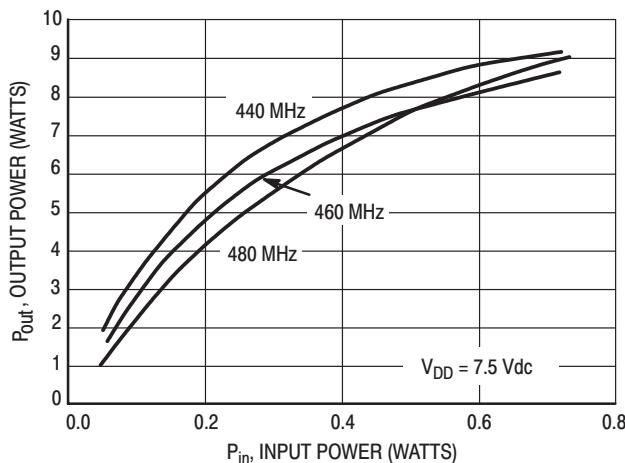


Figure 20. Output Power versus Input Power

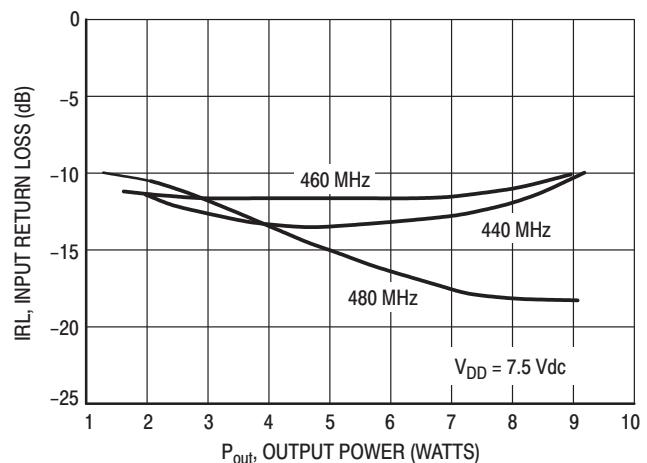


Figure 21. Input Return Loss versus Output Power

## TYPICAL CHARACTERISTICS, 440 – 480 MHz

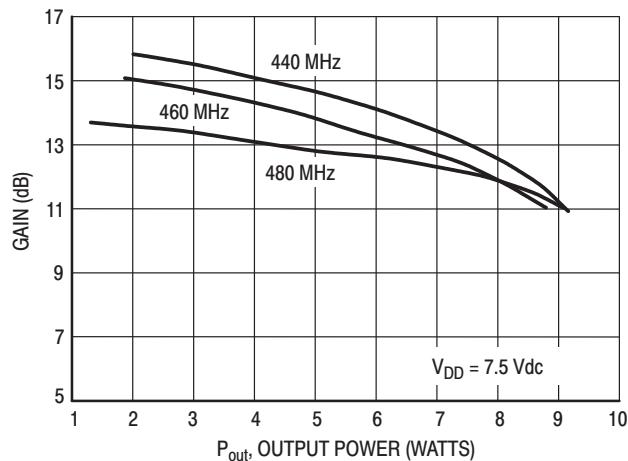


Figure 22. Gain versus Output Power

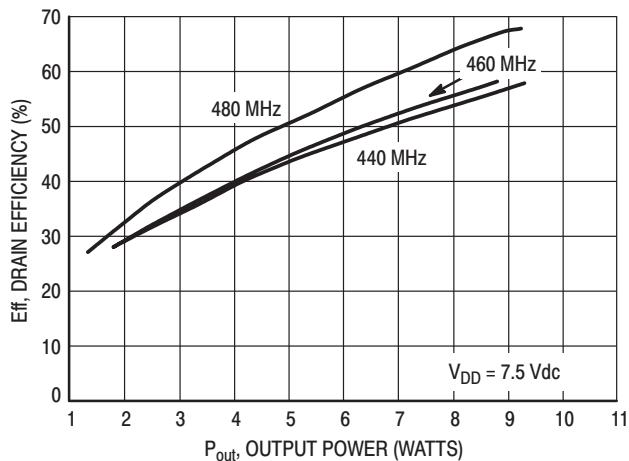


Figure 23. Drain Efficiency versus Output Power

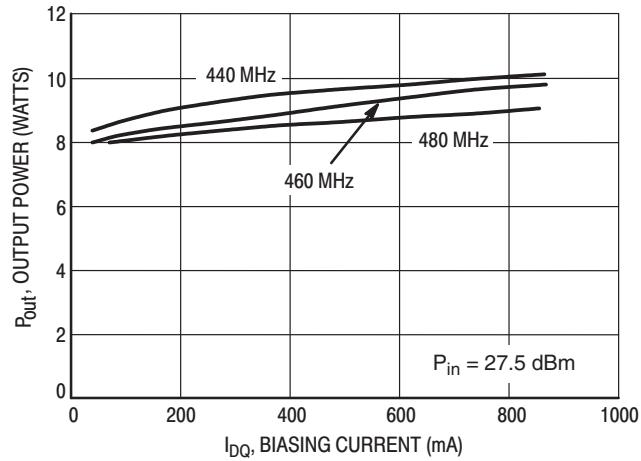


Figure 24. Output Power versus Biasing Current

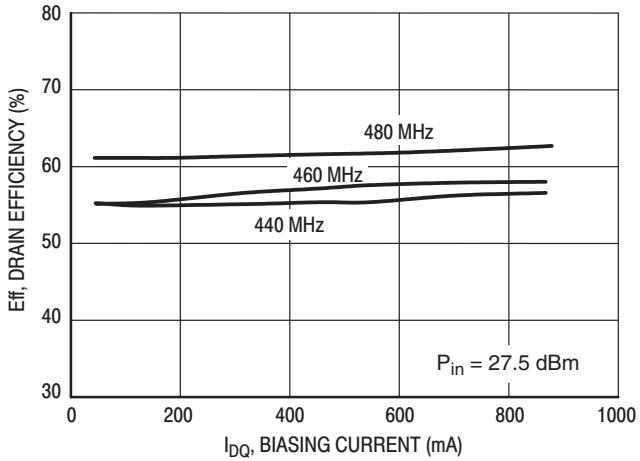


Figure 25. Drain Efficiency versus Biasing Current

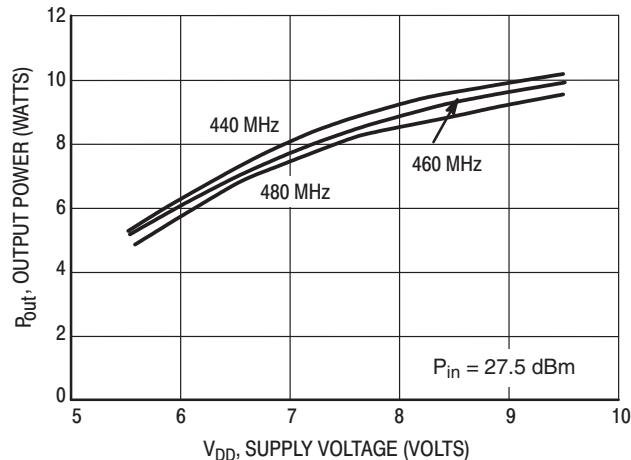


Figure 26. Output Power versus Supply Voltage

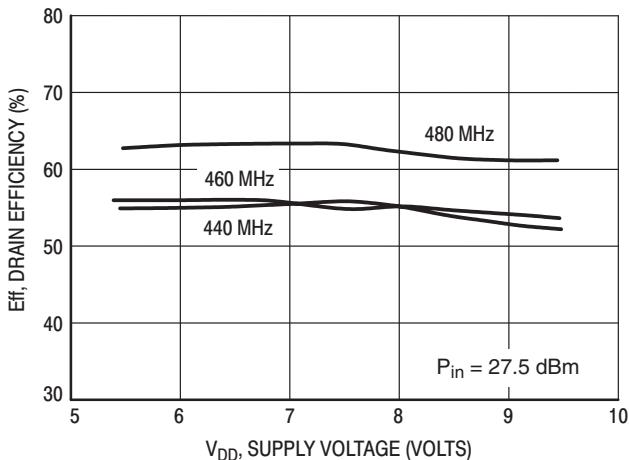
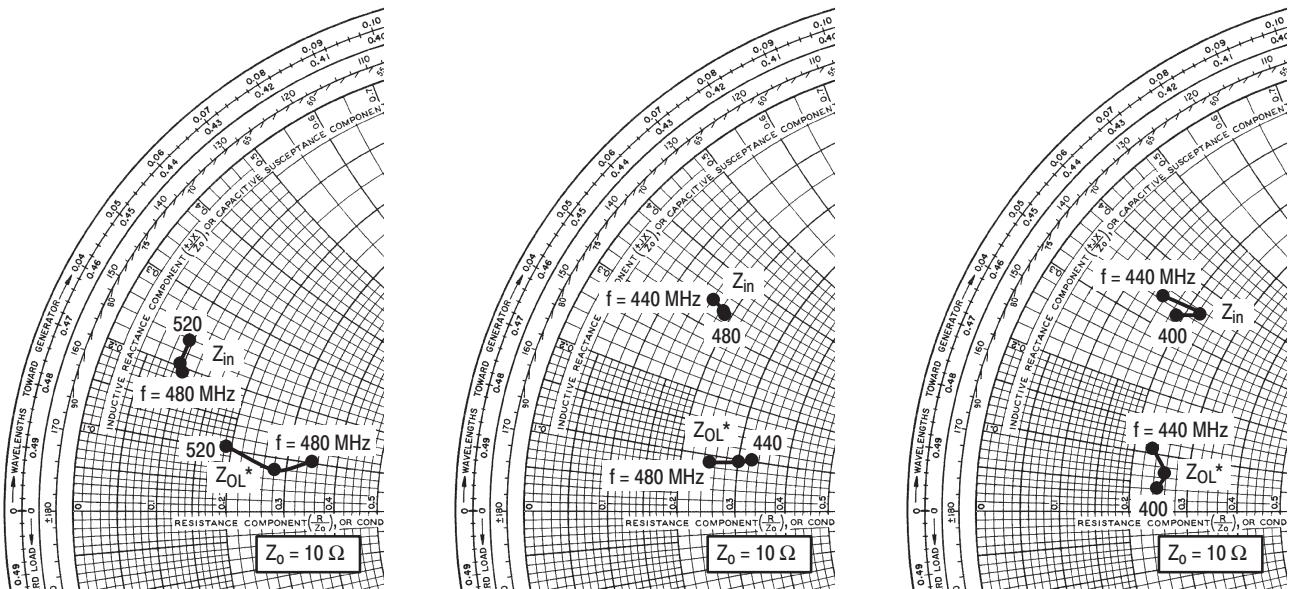


Figure 27. Drain Efficiency versus Supply Voltage



$V_{DD} = 7.5 \text{ V}$ ,  $I_{DQ} = 150 \text{ mA}$ ,  $P_{out} = 8 \text{ W}$

$f$ MHz	$Z_{in}$ $\Omega$	$Z_{OL}^*$ $\Omega$
480	$1.06 + j1.82$	$3.51 + j0.99$
500	$0.97 + j2.01$	$2.82 + j0.75$
520	$0.975 + j2.37$	$1.87 + j1.03$

$Z_{in}$  = Complex conjugate of source impedance.

$Z_{OL}^*$  = Complex conjugate of the load impedance at given output power, voltage, frequency, and  $\eta_D > 50\%$ .

$V_{DD} = 7.5 \text{ V}$ ,  $I_{DQ} = 150 \text{ mA}$ ,  $P_{out} = 8 \text{ W}$

$f$ MHz	$Z_{in}$ $\Omega$	$Z_{OL}^*$ $\Omega$
440	$1.62 + j3.41$	$3.25 + j0.98$
460	$1.85 + j3.35$	$3.05 + j0.93$
480	$1.91 + j3.31$	$2.54 + j0.84$

$Z_{in}$  = Complex conjugate of source impedance.

$Z_{OL}^*$  = Complex conjugate of the load impedance at given output power, voltage, frequency, and  $\eta_D > 50\%$ .

$V_{DD} = 7.5 \text{ V}$ ,  $I_{DQ} = 150 \text{ mA}$ ,  $P_{out} = 8 \text{ W}$

$f$ MHz	$Z_{in}$ $\Omega$	$Z_{OL}^*$ $\Omega$
400	$1.96 + j3.32$	$2.52 + j0.39$
420	$2.31 + j3.56$	$2.61 + j0.64$
440	$1.60 + j3.45$	$2.37 + j1.04$

$Z_{in}$  = Complex conjugate of source impedance.

$Z_{OL}^*$  = Complex conjugate of the load impedance at given output power, voltage, frequency, and  $\eta_D > 50\%$ .

Note:  $Z_{OL}^*$  was chosen based on tradeoffs between gain, drain efficiency, and device stability.

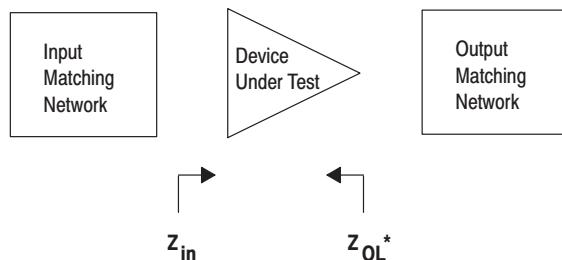


Figure 28. Series Equivalent Input and Output Impedance

Table 1. Common Source Scattering Parameters ( $V_{DD} = 7.5$  Vdc)

f MHz		$S_{11}$		$S_{21}$		$S_{12}$		$S_{22}$	
		$ S_{11} $	$\angle \phi$	$ S_{21} $	$\angle \phi$	$ S_{12} $	$\angle \phi$	$ S_{22} $	$\angle \phi$
50	0.84	-152	17.66	97	0.016	0	0.77	-167	
100	0.84	-164	8.86	85	0.016	5	0.78	-172	
200	0.86	-170	4.17	72	0.015	-5	0.79	-173	
300	0.88	-171	2.54	62	0.014	-8	0.80	-172	
400	0.90	-172	1.72	55	0.013	-25	0.83	-172	
500	0.92	-172	1.28	50	0.013	-10	0.84	-172	
600	0.94	-173	0.98	46	0.014	-22	0.86	-171	
700	0.95	-173	0.76	41	0.010	-30	0.86	-172	
800	0.96	-174	0.61	38	0.011	-14	0.86	-171	
900	0.96	-175	0.50	33	0.011	-31	0.85	-172	
1000	0.97	-175	0.40	31	0.006	55	0.88	-171	

f MHz		$S_{11}$		$S_{21}$		$S_{12}$		$S_{22}$	
		$ S_{11} $	$\angle \phi$	$ S_{21} $	$\angle \phi$	$ S_{12} $	$\angle \phi$	$ S_{22} $	$\angle \phi$
50	0.90	-165	20.42	94	0.018	1	0.76	-164	
100	0.89	-172	10.20	87	0.015	-7	0.77	-170	
200	0.90	-175	4.96	79	0.015	-12	0.77	-172	
300	0.90	-176	3.17	73	0.017	-2	0.80	-171	
400	0.91	-176	2.26	67	0.013	1	0.82	-172	
500	0.92	-176	1.75	63	0.011	-6	0.83	-171	
600	0.93	-176	1.39	59	0.012	-31	0.85	-171	
700	0.94	-176	1.14	55	0.015	-34	0.88	-171	
800	0.94	-176	0.93	51	0.008	-22	0.87	-171	
900	0.95	-177	0.78	45	0.007	2	0.87	-172	
1000	0.96	-177	0.65	43	0.008	-40	0.90	-170	

f MHz		$S_{11}$		$S_{21}$		$S_{12}$		$S_{22}$	
		$ S_{11} $	$\angle \phi$	$ S_{21} $	$\angle \phi$	$ S_{12} $	$\angle \phi$	$ S_{22} $	$\angle \phi$
50	0.92	-165	19.90	95	0.017	3	0.76	-164	
100	0.90	-172	9.93	88	0.018	2	0.77	-170	
200	0.91	-176	4.84	80	0.016	-4	0.77	-172	
300	0.91	-176	3.10	74	0.014	-11	0.80	-172	
400	0.92	-176	2.22	68	0.014	-14	0.81	-172	
500	0.93	-176	1.73	64	0.016	-8	0.83	-171	
600	0.94	-176	1.39	61	0.013	-24	0.85	-171	
700	0.94	-176	1.12	56	0.013	-24	0.87	-171	
800	0.95	-176	0.93	52	0.009	-12	0.87	-171	
900	0.96	-177	0.78	46	0.008	10	0.87	-173	
1000	0.97	-177	0.64	44	0.012	4	0.89	-169	

## APPLICATIONS INFORMATION

### DESIGN CONSIDERATIONS

This device is a common-source, RF power, N-Channel enhancement mode, Lateral Metal-Oxide Semiconductor Field-Effect Transistor (MOSFET). Motorola Application Note AN211A, "FETs in Theory and Practice", is suggested reading for those not familiar with the construction and characteristics of FETs.

This surface mount packaged device was designed primarily for VHF and UHF portable power amplifier applications. Manufacturability is improved by utilizing the tape and reel capability for fully automated pick and placement of parts. However, care should be taken in the design process to insure proper heat sinking of the device.

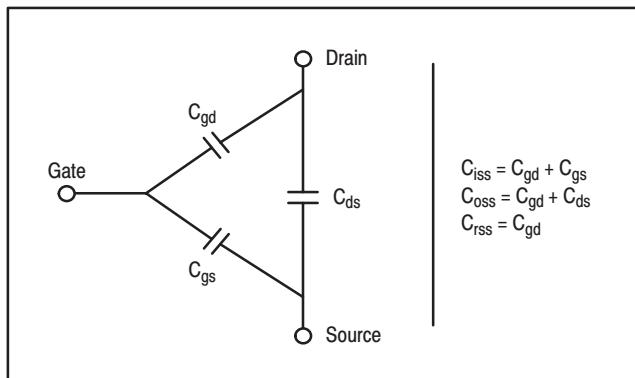
The major advantages of Lateral RF power MOSFETs include high gain, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage.

### MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between all three terminals. The metal oxide gate structure determines the capacitors from gate-to-drain ( $C_{gd}$ ), and gate-to-source ( $C_{gs}$ ). The PN junction formed during fabrication of the RF MOSFET results in a junction capacitance from drain-to-source ( $C_{ds}$ ). These capacitances are characterized as input ( $C_{iss}$ ), output ( $C_{oss}$ ) and reverse transfer ( $C_{rss}$ ) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The  $C_{iss}$  can be specified in two ways:

1. Drain shorted to source and positive voltage at the gate.
2. Positive voltage of the drain in respect to source and zero volts at the gate.

In the latter case, the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



### DRAIN CHARACTERISTICS

One critical figure of merit for a FET is its static resistance in the full-on condition. This on-resistance,  $R_{DS(on)}$ , occurs in the linear region of the output characteristic and is specified at a specific gate-source voltage and drain current. The

drain-source voltage under these conditions is termed  $V_{DS(on)}$ . For MOSFETs,  $V_{DS(on)}$  has a positive temperature coefficient at high temperatures because it contributes to the power dissipation within the device.

$BV_{DSS}$  values for this device are higher than normally required for typical applications. Measurement of  $BV_{DSS}$  is not recommended and may result in possible damage to the device.

### GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The DC input resistance is very high – on the order of  $10^9 \Omega$  – resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage to the gate greater than the gate-to-source threshold voltage,  $V_{GS(th)}$ .

**Gate Voltage Rating** — Never exceed the gate voltage rating. Exceeding the rated  $V_{GS}$  can result in permanent damage to the oxide layer in the gate region.

**Gate Termination** — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

**Gate Protection** — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended. Using a resistor to keep the gate-to-source impedance low also helps dampen transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

### DC BIAS

Since this device is an enhancement mode FET, drain current flows only when the gate is at a higher potential than the source. RF power FETs operate optimally with a quiescent drain current ( $I_{DQ}$ ), whose value is application dependent. This device was characterized at  $I_{DQ} = 150$  mA, which is the suggested value of bias current for typical applications. For special applications such as linear amplification,  $I_{DQ}$  may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

### GAIN CONTROL

Power output of this device may be controlled to some degree with a low power dc control signal applied to the gate, thus facilitating applications such as manual gain control, ALC/AGC and modulation systems. This characteristic is very dependent on frequency and load line.

## **MOUNTING**

The specified maximum thermal resistance of  $2^{\circ}\text{C}/\text{W}$  assumes a majority of the  $0.065'' \times 0.180''$  source contact on the back side of the package is in good contact with an appropriate heat sink. As with all RF power devices, the goal of the thermal design should be to minimize the temperature at the back side of the package. Refer to Motorola Application Note AN4005/D, "Thermal Management and Mounting Method for the PLD-1.5 RF Power Surface Mount Package," and Engineering Bulletin EB209/D, "Mounting Method for RF Power Leadless Surface Mount Transistor" for additional information.

## **AMPLIFIER DESIGN**

Impedance matching networks similar to those used with bipolar transistors are suitable for this device. For examples see Motorola Application Note AN721, "Impedance Matching Networks Applied to RF Power Transistors." Large-signal

impedances are provided, and will yield a good first pass approximation.

Since RF power MOSFETs are triode devices, they are not unilateral. This coupled with the very high gain of this device yields a device capable of self oscillation. Stability may be achieved by techniques such as drain loading, input shunt resistive loading, or output to input feedback. The RF test fixture implements a parallel resistor and capacitor in series with the gate, and has a load line selected for a higher efficiency, lower gain, and more stable operating region.

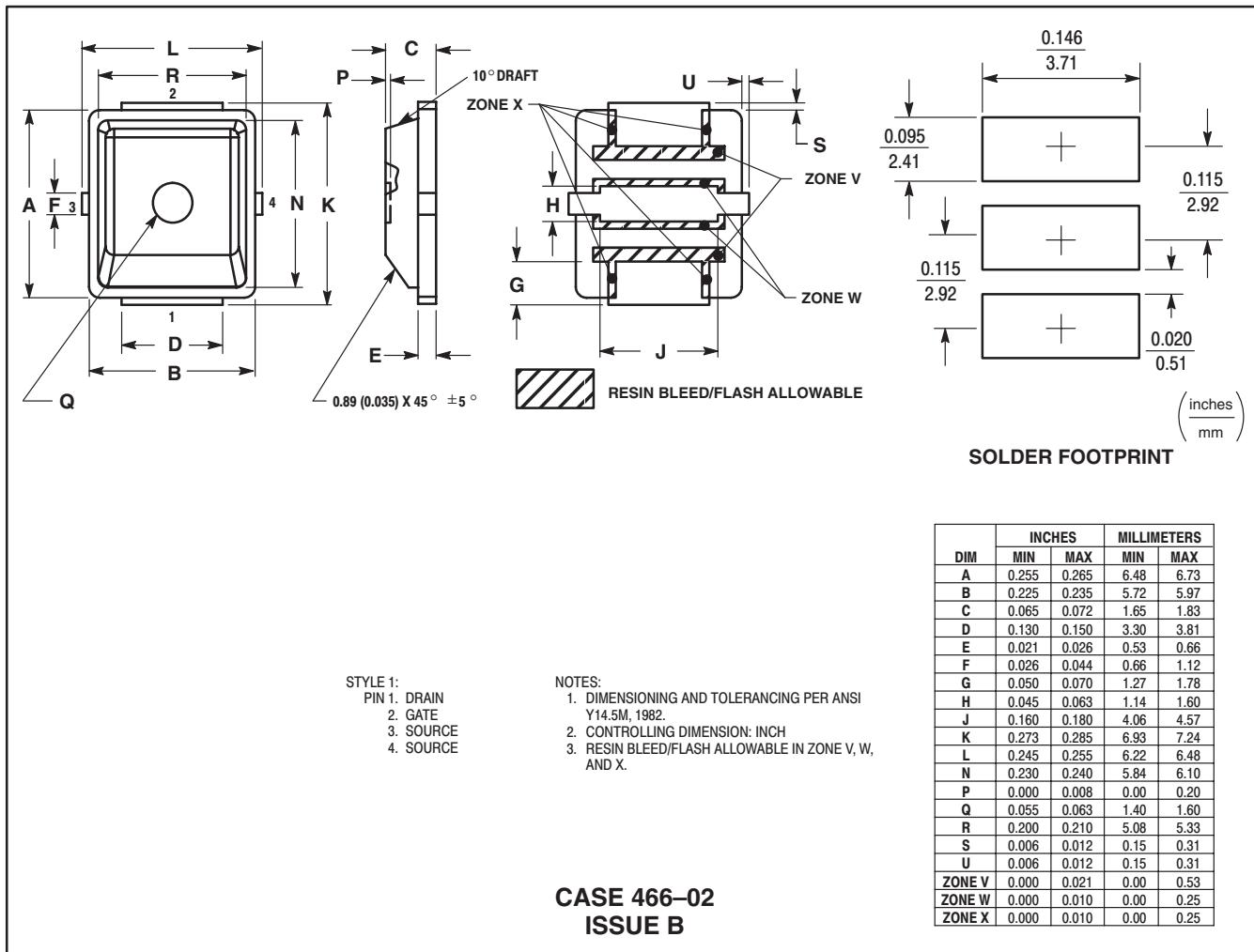
Two-port stability analysis with this device's S-parameters provides a useful tool for selection of loading or feedback circuitry to assure stable operation. See Motorola Application Note AN215A, "RF Small-Signal Design Using Two-Port Parameters" for a discussion of two port network theory and stability.

## NOTES

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## PACKAGE DIMENSIONS



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