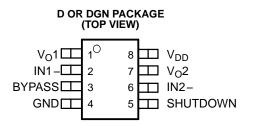




### 150-mW STEREO AUDIO POWER AMPLIFIER

#### **FEATURES**

- 150-mW Stereo Output
- PC Power Supply Compatible
  - Fully Specified for 3.3-V and 5-V Operation
  - Operation to 2.5 V
- Pop Reduction Circuitry
- Internal Midrail Generation
- Thermal and Short-Circuit Protection
- Surface-Mount Packaging
  - PowerPAD™ MSOP
  - SOIC
- Pin Compatible With LM4880 and LM4881 (SOIC)

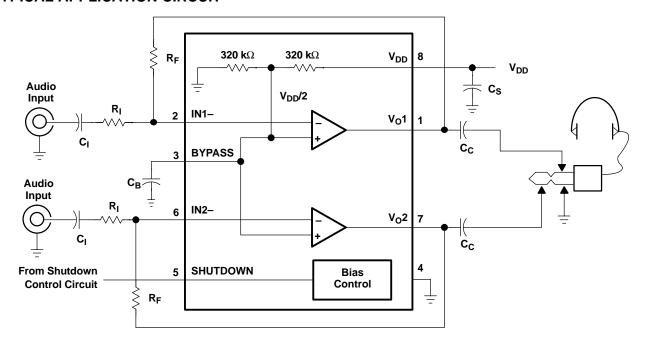


### **DESCRIPTION**

The TPA122 is a stereo audio power amplifier packaged in either an 8-pin SOIC, or an 8-pin PowerPAD<sup>TM</sup> MSOP package capable of delivering 150 mW of continuous RMS power per channel into 8- $\Omega$  loads. Amplifier gain is externally configured by means of two resistors per input channel and does not require external compensation for settings of 1 to 10.

THD+N when driving an 8- $\Omega$  load from 5 V is 0.1% at 1 kHz, and less than 2% across the audio band of 20 Hz to 20 kHz. For 32- $\Omega$  loads, the THD+N is reduced to less than 0.06% at 1 kHz, and is less than 1% across the audio band of 20 Hz to 20 kHz. For 10-k $\Omega$  loads, the THD+N performance is 0.01% at 1 kHz, and less than 0.02% across the audio band of 20 Hz to 20 kHz.

### TYPICAL APPLICATION CIRCUIT



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

PowerPAD is a trademark of Texas Instruments.





These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

#### **AVAILABLE OPTIONS**

	PACKAGED DEVIC	MSOP	
T <sub>A</sub>	T <sub>A</sub> SMALL OUTLINE <sup>(1)</sup> (D)		SYMBOLIZATION
-40°C to 85°C	TPA122D	TPA122DGN	TI AAE

(1) The D and DGN packages are available in left-ended tape and reel only (e.g., TPA122DR, TPA122DGNR).

#### **Terminal Functions**

TERMINA	AL	1/0	DESCRIPTION	
NAME	NO.	"	DESCRIPTION	
BYPASS	3	ı	Tap to voltage divider for internal mid-supply bias supply. Connect to a 0.1 $\mu$ F to 1 $\mu$ F low ESR capacitor for best performance.	
GND	4	ı	GND is the ground connection.	
IN1-	2	1	IN1- is the inverting input for channel 1.	
IN2-	6	ı	IN2- is the inverting input for channel 2.	
SHUTDOWN	5	- 1	Puts the device in a low quiescent current mode when held high	
$V_{DD}$	8	1	V <sub>DD</sub> is the supply voltage terminal.	
V <sub>O</sub> 1	1	0	V <sub>O</sub> 1 is the audio output for channel 1.	
V <sub>O</sub> 2	7	0	V <sub>O</sub> 2 is the audio output for channel 2.	

### **ABSOLUTE MAXIMUM RATINGS**

over operating free-air temperature range (unless otherwise noted)(1)

		UNIT
$V_{DD}$	Supply voltage	6 V
VI	Input voltage	–0.3 V to V <sub>DD</sub> + 0.3 V
	Continuous total power dissipation	Internally limited
TJ	Operating junction temperature range	-40°C to 150°C
T <sub>stg</sub>	Storage temperature range	−65°C to 150°C
	Lead temperature 1,6 mm (1/16 inch) from case for 10 seconds	260°C

<sup>(1)</sup> Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

### **DISSIPATION RATING TABLE**

PACKAGE	$T_A \le 25^{\circ}C$ POWER RATING	DERATING FACTOR ABOVE T <sub>A</sub> = 25°C	T <sub>A</sub> = 70°C POWER RATING	T <sub>A</sub> = 85°C POWER RATING
D	725 mW	5.8 mW/°C	464 mW	377 mW
DGN	2.14 W <sup>(1)</sup>	17.1 mW/°C	1.37 W	1.11 W

(1) See the Texas Instruments document, PowerPAD Thermally Enhanced Package Application Report (SLMA002), for more information on the PowerPAD package. The thermal data was measured on a PCB layout based on the information in the section entitled Texas Instruments Recommended Board for PowerPAD of that document.



### **RECOMMENDED OPERATING CONDITIONS**

		MIN	MAX	UNIT
$V_{DD}$	Supply voltage	2.5	5.5	V
T <sub>A</sub>	Operating free-air temperature	-40	85	°C
V <sub>IH</sub>	High-level input voltage, (SHUTDOWN)	$0.80 \times V_{DD}$		V
V <sub>IL</sub>	Low-level input voltage, (SHUTDOWN)		$0.40 \times V_{DD}$	V

### DC ELECTRICAL CHARACTERISTICS

at  $T_A = 25$ °C,  $V_{DD} = 3.3$  V (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
Voo	Output offset voltage				10	mV
PSRR	Power supply rejection ratio	V <sub>DD</sub> = 3.2 V to 3.4 V		83		dB
I <sub>DD</sub>	Supply current	V <sub>DD</sub> = 2.5, SHUTDOWN = 0 V		1.5	3	mA
I <sub>DD(SD)</sub>	Supply current in SHUTDOWN mode	V <sub>DD</sub> = 2.5, SHUTDOWN = V <sub>DD</sub>		10	50	μA
Z <sub>I</sub>	Input impedance			> 1		ΜΩ

### **AC OPERATING CHARACTERISTICS**

 $V_{DD}$  = 3.3 V,  $T_A$  = 25°C,  $R_L$  = 8  $\Omega$ 

	PARAMETER	TEST CONDITIONS	MIN TYP N	MAX UNIT
Po	Output power (each channel)	THD≤ 0.1%	70 <sup>(1)</sup>	mW
THD+N	Total harmonic distortion + noise	P <sub>O</sub> = 70 mW, 20 Hz–20 kHz	2%	
B <sub>OM</sub>	Maximum output power BW	G = 10, THD < 5%	> 20	kHz
	Phase margin	Open loop	58°	
	Supply ripple rejection	f = 1 kHz	68	dB
	Channel/channel output separation	f = 1 kHz	86	dB
SNR	Signal-to-noise ratio	P <sub>O</sub> = 100 mW	100	dB
V <sub>n</sub>	Noise output voltage		9.5	μV(rms)

<sup>(1)</sup> Measured at 1 kHz

### DC ELECTRICAL CHARACTERISTICS

at  $T_A = 25$ °C,  $V_{DD} = 5.5$  V (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
Voo	Output offset voltage				10	mV
PSRR	Power supply rejection ratio	V <sub>DD</sub> = 4.9 V to 5.1 V		76		dB
I <sub>DD</sub>	Supply current	SHUTDOWN = 0 V		1.5	3	mA
I <sub>DD(SD)</sub>	Supply current in SHUTDOWN mode	SHUTDOWN = V <sub>DD</sub>		60	100	μΑ
I <sub>IH</sub>	High-level input current (SHUTDOWN)	$V_{DD} = 5.5 \text{ V}, V_{I} = V_{DD}$			1	μΑ
$ I_{IL} $	Low-level input current (SHUTDOWN)	$V_{DD} = 5.5 \text{ V}, V_{I} = 0 \text{ V}$			1	μΑ
Z <sub>I</sub>	Input impedance			> 1		$M\Omega$



### **AC OPERATING CHARACTERISTICS**

 $V_{DD} = 5 \text{ V}, T_A = 25^{\circ}\text{C}, R_L = 8 \Omega$ 

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
Po	Output power (each channel)	THD≤ 0.1%		70(1)		mW
THD+N	Total harmonic distortion + noise	$P_{O} = 150 \text{ mW}, 20 \text{ Hz}-20 \text{ kHz}$		2%		
B <sub>OM</sub>	Maximum output power BW	G = 10, THD < 5%		> 20		kHz
	Phase margin	Open loop		56°		
	Supply ripple rejection ratio	f = 1 kHz		68		dB
	Channel/channel output separation	f = 1 kHz		86		dB
SNR	Signal-to-noise ratio	P <sub>O</sub> = 150 mW		100		dB
V <sub>n</sub>	Noise output voltage			9.5		μV(rms)

<sup>(1)</sup> Measured at 1 kHz

### **AC OPERATING CHARACTERISTICS**

 $V_{DD} = 3.3 \text{ V}, T_A = 25^{\circ}\text{C}, R_L = 32 \Omega$ 

	PARAMETER	TEST CONDITIONS	MIN TYP	MAX	UNIT
Po	Output power (each channel)	THD≤ 0.1%	40(1)		mW
THD+N	Total harmonic distortion + noise	P <sub>O</sub> = 30 mW, 20 Hz–20 kHz	0.5%		
B <sub>OM</sub>	Maximum output power BW	G = 10, THD < 2%	> 20		kHz
	Phase margin	Open loop	58°		
	Supply ripple rejection	f = 1 kHz	68		dB
	Channel/channel output separation	f = 1 kHz	86		dB
SNR	Signal-to-noise ratio	P <sub>O</sub> = 100 mW	100		dB
V <sub>n</sub>	Noise output voltage		9.5		μV(rms)

<sup>(1)</sup> Measured at 1 kHz

### **AC OPERATING CHARACTERISTICS**

 $\mathrm{V_{DD}} = 5~\mathrm{V},~\mathrm{T_A} = 25^{\circ}\mathrm{C},~\mathrm{R_L} = 32~\Omega$ 

	PARAMETER	TEST CONDITIONS	MIN TYP	MAX	UNIT
Po	Output power (each channel)	THD≤ 0.1%	40 <sup>(1)</sup>		mW
THD+N	Total harmonic distortion + noise	P <sub>O</sub> = 60 mW, 20 Hz–20 kHz	0.4%		
B <sub>OM</sub>	Maximum output power BW	G = 10, THD < 2%	> 20		kHz
	Phase margin	Open loop	56°		
	Supply ripple rejection	f = 1 kHz	68		dB
	Channel/channel output separation	f = 1 kHz	86		dB
SNR	Signal-to-noise ratio	P <sub>O</sub> = 150 mW	100		dB
V <sub>n</sub>	Noise output voltage		9.5		μV(rms)

<sup>(1)</sup> Measured at 1 kHz

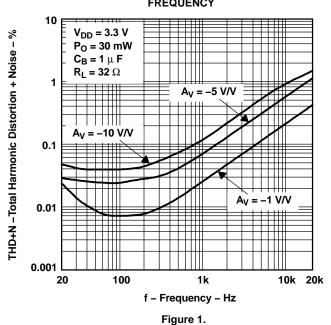


### **TYPICAL CHARACTERISTICS**

### **Table of Graphs**

			FIGURE
THD+N	Total harmonic distortion plus noise	vs Frequency	1, 2, 4, 5, 7, 8, 10, 11, 13, 14, 16, 17, 34, 36
	•	vs Output power	3, 6, 9, 12, 15, 18
	Supply ripple rejection	vs Frequency	19, 20
V <sub>n</sub>	Output noise voltage	vs Frequency	21, 22
	Crosstalk	vs Frequency	23-26, 37, 38
	Mute attenuation	vs Frequency	27, 28
	Open-loop gain and phase margin	vs Frequency	29, 30
	Output power	vs Load resistance	31, 32
	Phase	vs Frequency	39-44
I <sub>DD</sub>	Supply current	vs Supply voltage	33
SNR	Signal-to-noise ratio	vs Voltage gain	35
	Closed-loop gain	vs Frequency	39-44
	Power dissipation/amplifier	vs Output power	45, 46

## TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY



### TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY

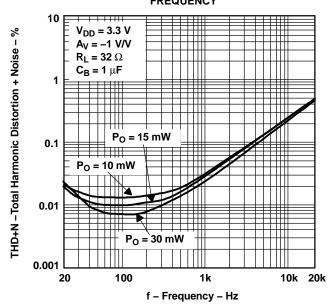
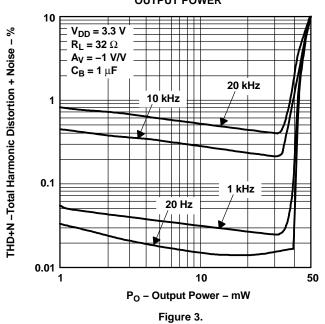


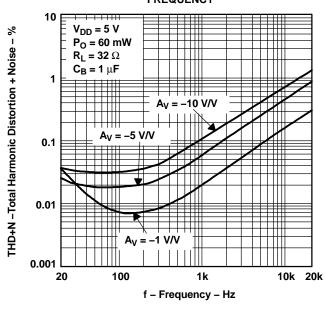
Figure 2.



## TOTAL HARMONIC DISTORTION + NOISE vs OUTPUT POWER

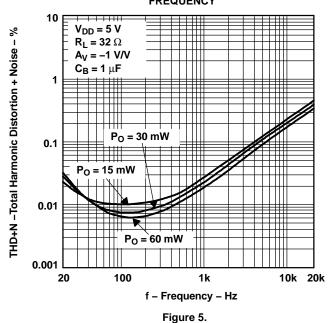


### TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY



#### Figure 4.

## TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY



### TOTAL HARMONIC DISTORTION + NOISE vs OUTPUT POWER

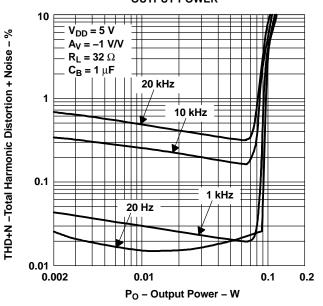


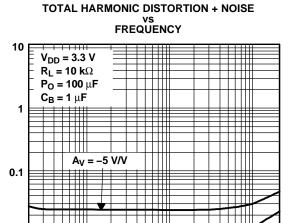
Figure 6.



THD+N -Total Harmonic Distortion + Noise - %

0.01

0.001



# 20 100 1k 10k 20k f - Frequency - Hz Figure 7.

TOTAL HARMONIC DISTORTION + NOISE vs OUTPUT POWER

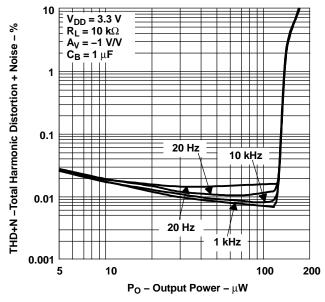


Figure 9.

### TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY

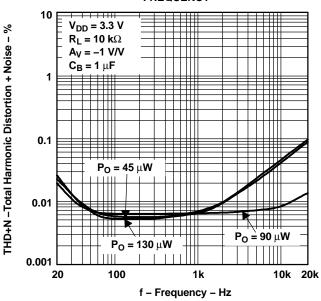


Figure 8.

### TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY

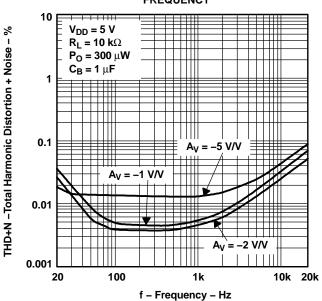


Figure 10.



## TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY

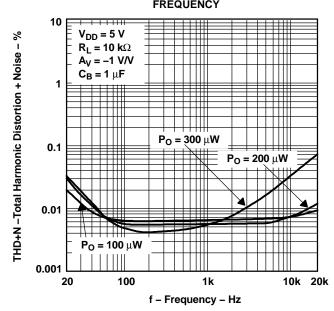


Figure 11.

### TOTAL HARMONIC DISTORTION + NOISE vs OUTPUT POWER

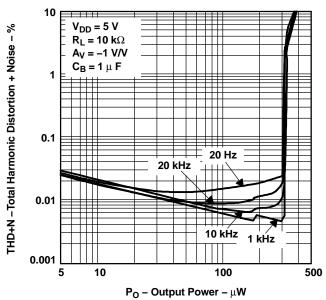


Figure 12.

## TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY

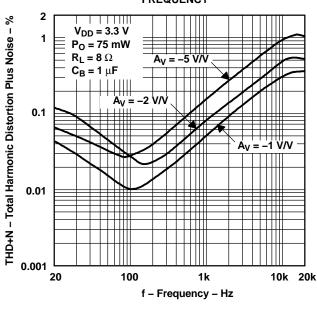


Figure 13.

## TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY

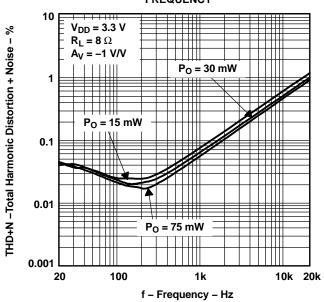
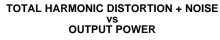


Figure 14.





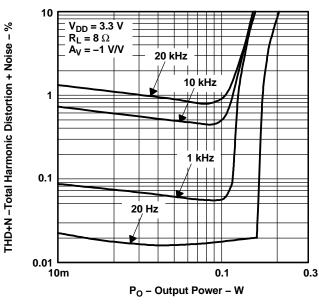


Figure 15.

## TOTAL HARMONIC DISTORTION + NOISE VS FREQUENCY

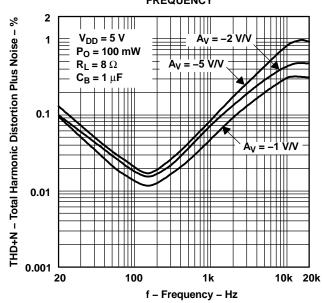


Figure 16.

## TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY

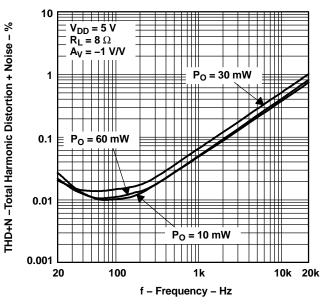


Figure 17.

### TOTAL HARMONIC DISTORTION + NOISE vs OUTPUT POWER

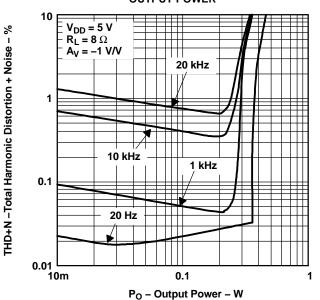


Figure 18.



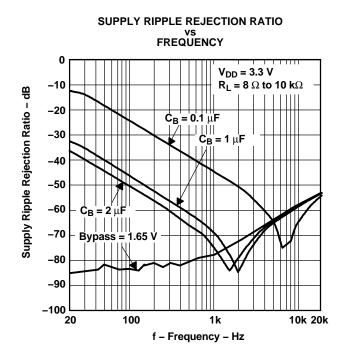
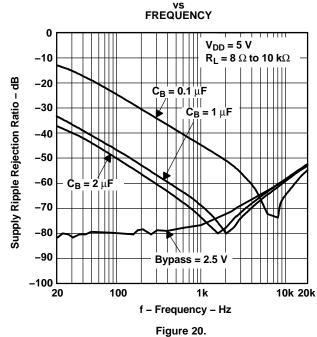
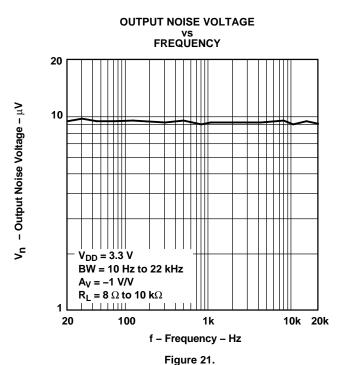
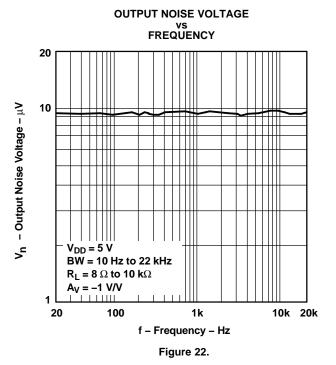


Figure 19.

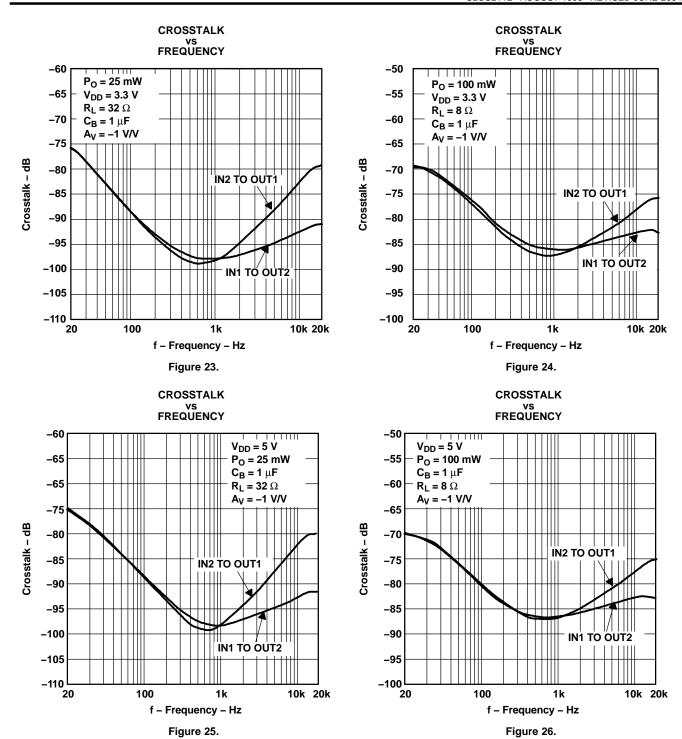


**SUPPLY RIPPLE REJECTION RATIO** 

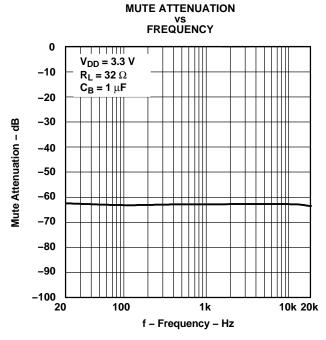












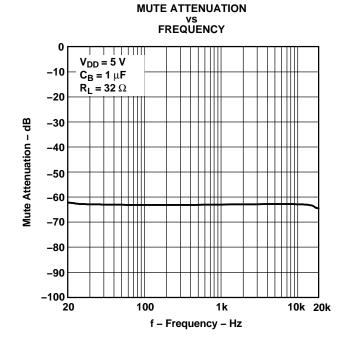
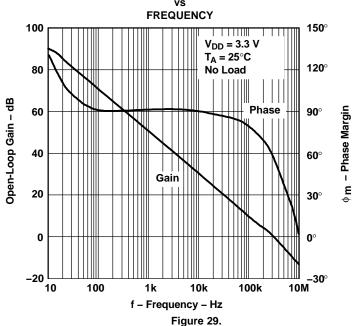


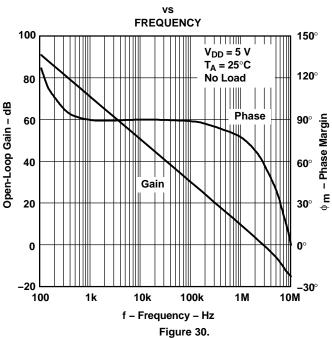
Figure 27. Figure 28.

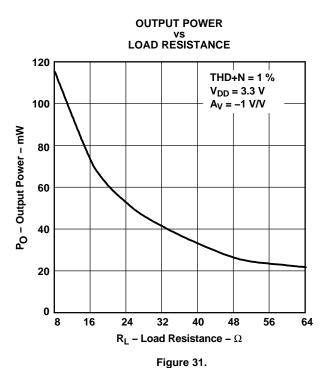
### OPEN-LOOP GAIN AND PHASE MARGIN vs





### **OPEN-LOOP GAIN AND PHASE MARGIN**





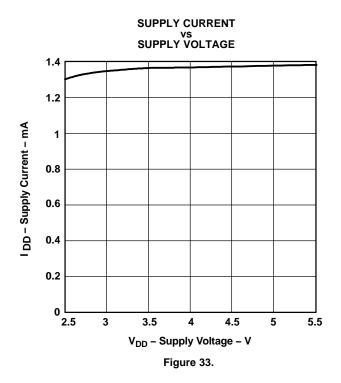
### OUTPUT POWER vs LOAD RESISTANCE 300 THD+N = 1 % $V_{DD} = 5 V$ 250 $A_V = -1 \text{ V/V}$ Po - Output Power - mW 200 150 100 50 16 40 32 $\mbox{R}_{\mbox{\scriptsize L}}$ – Load Resistance – $\Omega$

56

Figure 32.

64





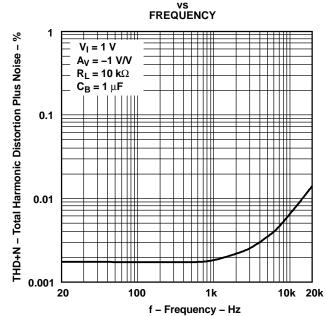
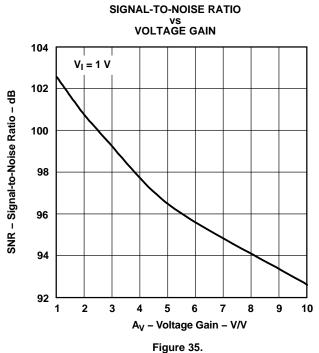
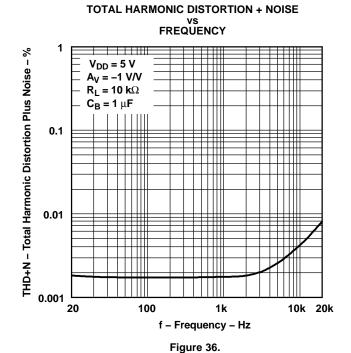


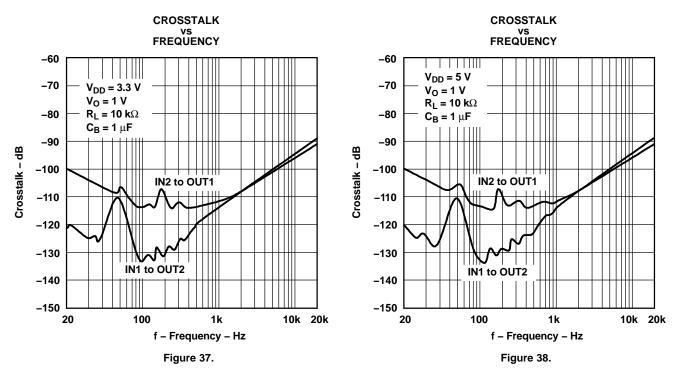
Figure 34.

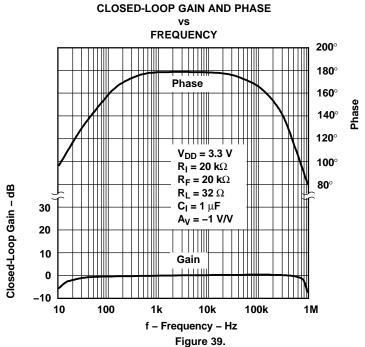
**TOTAL HARMONIC DISTORTION + NOISE** 





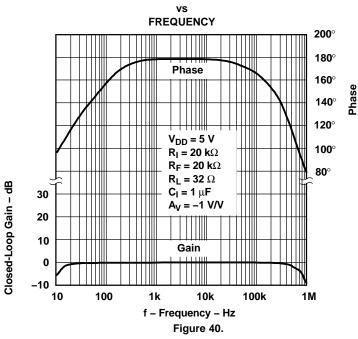




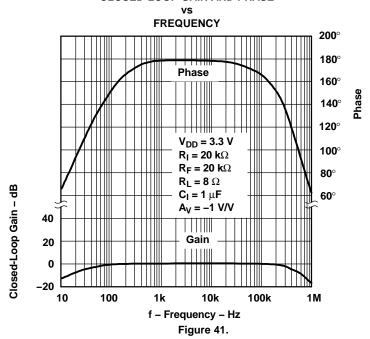




### **CLOSED-LOOP GAIN AND PHASE**

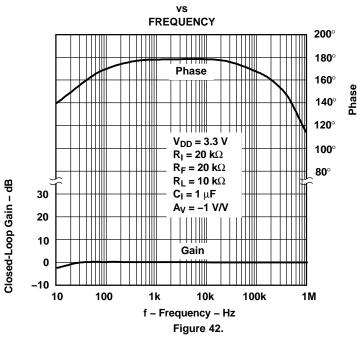


### **CLOSED-LOOP GAIN AND PHASE**

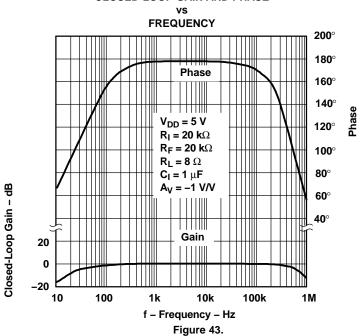








### **CLOSED-LOOP GAIN AND PHASE**





### **CLOSED-LOOP GAIN AND PHASE** vs **FREQUENCY 200**° 180° Phase 160° 140° 120° $V_{DD} = 5 V$ $R_I = 20 \text{ k}\Omega$ 100° $R_F = 20 \text{ k}\Omega$ $R_L = 10 \text{ k}\Omega$ 80° Closed-Loop Gain - dB $C_I = 1 \mu F$ 30 $A_V = -1 \text{ V/V}$ 20 10 Gain

### POWER DISSIPATION/AMPLIFIER vs OUTPUT POWER 80 $V_{DD} = 3.3 V$ 8 Ω 70 60 Amplifier Power - mW 50 40 16 Ω 30 $32^{\prime}\Omega$ 20 **64** Ω 10 20 40 80 100 120 140 160 180 0 60 200 Load Power - mW Figure 45.

0 -10 10

100

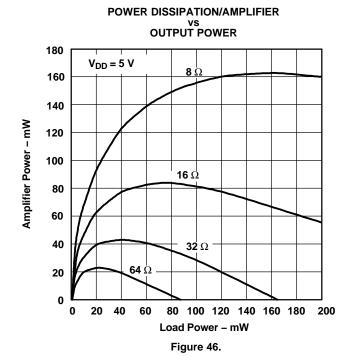
1k

10k

f - Frequency - Hz Figure 44.

100k

1M





#### APPLICATION INFORMATION

### GAIN SETTING RESISTORS, R<sub>F</sub> and R<sub>I</sub>

The gain for the TPA122 is set by resistors  $R_F$  and  $R_I$  according to Equation 1.

$$Gain = -\left(\frac{R_F}{R_I}\right) \tag{1}$$

Given that the TPA122 is an MOS amplifier, the input impedance is high. Consequently, input leakage currents are not generally a concern, although noise in the circuit increases as the value of  $R_F$  increases. In addition, a certain range of  $R_F$  values is required for proper start-up operation of the amplifier. Taken together, it is recommended that the effective impedance seen by the inverting node of the amplifier be set between 5 k $\Omega$  and 20 k $\Omega$ . The effective impedance is calculated in Equation 2.

Effective Impedance = 
$$\frac{R_F R_I}{R_F + R_I}$$
 (2)

As an example, consider an input resistance of 20 k $\Omega$  and a feedback resistor of 20 k $\Omega$ . The gain of the amplifier would be -1 and the effective impedance at the inverting terminal would be 10 k $\Omega$ , which is within the recommended range.

For high-performance applications, metal film resistors are recommended because they tend to have lower noise levels than carbon resistors. For values of  $R_F$  above 50  $k\Omega$ , the amplifier tends to become unstable due to a pole formed from  $R_F$  and the inherent input capacitance of the MOS input structure. For this reason, a small compensation capacitor of approximately 5 pF should be placed in parallel with  $R_F$ . In effect, this creates a low-pass filter network with the cutoff frequency defined in Equation 3.

$$f_{c(lowpass)} = \frac{1}{2\pi R_F C_F}$$
 (3)

For example, if  $R_F$  is 100 k $\Omega$  and  $C_F$  is 5 pF, then  $f_{c(lowpass)}$  is 318 kHz, which is well outside the audio range.

### INPUT CAPACITOR C

In the typical application, an input capacitor,  $C_I$ , is required to allow the amplifier to bias the input signal to the proper dc level for optimum operation. In this case,  $C_I$  and  $R_I$  form a high-pass filter with the corner frequency determined in Equation 4.

$$f_{c(highpass)} = \frac{1}{2\pi R_{I}C_{I}}$$
 (4)

The value of  $C_l$  is important to consider, as it directly affects the bass (low-frequency) performance of the circuit. Consider the example where  $R_l$  is 20 k $\Omega$  and the specification calls for a flat bass response down to 20 Hz. Equation 4 is reconfigured as Equation 5.

$$C_{I} = \frac{1}{2\pi R_{I} f_{c(highpass)}}$$
 (5)

In this example,  $C_l$  is 0.4  $\mu F$ , so one would likely choose a value in the range of 0.47  $\mu F$  to 1  $\mu F$ . A further consideration for this capacitor is the leakage path from the input source through the input network  $(R_l, C_l)$  and the feedback resistor  $(R_F)$  to the load. This leakage current creates a dc offset voltage at the input to the amplifier that reduces useful headroom, especially in high-gain applications (> 10). For this reason a low-leakage tantalum or ceramic capacitor is the best choice. When polarized capacitors are used, the positive side of the capacitor should face the amplifier input in most applications, as the dc level there is held at  $V_{DD}/2$ , which is likely higher than the source dc level. Note that it is important to confirm the capacitor polarity in the application.



### **APPLICATION INFORMATION (continued)**

### POWER SUPPLY DECOUPLING, C<sub>S</sub>

The TPA122 is a high-performance CMOS audio amplifier that requires adequate power supply decoupling to ensure that the output total harmonic distortion (THD) is as low as possible. Power supply decoupling also prevents oscillations for long lead lengths between the amplifier and the speaker. The optimum decoupling is achieved by using two capacitors of different types that target different types of noise on the power supply leads. For higher frequency transients, spikes, or digital hash on the line, a good low equivalent-series-resistance (ESR) ceramic capacitor, typically 0.1  $\mu$ F, placed as close as possible to the device  $V_{DD}$  lead, works best. For filtering lower frequency noise signals, a larger aluminum electrolytic capacitor of 10  $\mu$ F or greater placed near the power amplifier is recommended.

### MIDRAIL BYPASS CAPACITOR, CR

The midrail bypass capacitor,  $C_B$ , serves several important functions. During start-up,  $C_B$  determines the rate at which the amplifier starts up. This helps to push the start-up pop noise into the subaudible range (so low it can not be heard). The second function is to reduce noise produced by the power supply caused by coupling into the output drive signal. This noise is from the midrail generation circuit internal to the amplifier. The capacitor is fed from a 160-k $\Omega$  source inside the amplifier. To keep the start-up pop as low as possible, the relationship shown in Equation 6 should be maintained.

$$\frac{1}{\left(\mathsf{C}_{\mathsf{B}} \times 160 \,\mathsf{k}\Omega\right)} \le \frac{1}{\left(\mathsf{C}_{\mathsf{I}}\mathsf{R}_{\mathsf{I}}\right)} \tag{6}$$

As an example, consider a circuit where  $C_B$  is 1  $\mu F$ ,  $C_I$  is 1  $\mu F$ , and  $R_I$  is 20  $k\Omega$ . Inserting these values into Equation 6 results in:  $6.25 \le 50$  which satisfies the rule. Bypass capacitor,  $C_B$ , values of 0.1- $\mu F$  to 1- $\mu F$  ceramic or tantalum low-ESR capacitors are recommended for the best THD and noise performance.

### **OUTPUT COUPLING CAPACITOR, Cc**

In the typical single-supply, single-ended (SE) configuration, an output coupling capacitor ( $C_{\rm C}$ ) is required to block the dc bias at the output of the amplifier, thus preventing dc currents in the load. As with the input coupling capacitor, the output coupling capacitor and impedance of the load form a high-pass filter governed by Equation 7.

$$f_{C} = \frac{1}{2\pi R_{L} C_{C}} \tag{7}$$

The main disadvantage, from a performance standpoint, is that the typically small load impedances drive the low-frequency corner higher. Large values of  $C_C$  are required to pass low frequencies into the load. Consider the example where a  $C_C$  of 68  $\mu F$  is chosen and loads vary from 32  $\Omega$  to 47  $k\Omega$ . Table 1 summarizes the frequency response characteristics of each configuration.

Table 1. Common Load Impedances vs Low Frequency Output Characteristics in SE Mode

$R_L$	C <sub>C</sub>	LOWEST FREQUENCY
32 Ω	68 µF	73 Hz
10,000 Ω	68 µF	0.23 Hz
47,000 Ω	68 µF	0.05 Hz

As Table 1 indicates, headphone response is adequate and drive into line level inputs (a home stereo for example) is good.

The output coupling capacitor required in single-supply, SE mode also places additional constraints on the selection of other components in the amplifier circuit. With the rules described earlier still valid, add the following relationship:



$$\frac{1}{\left(C_{\mathsf{B}} \times 160 \,\mathrm{k}\Omega\right)} \le \frac{1}{\left(C_{\mathsf{I}} \mathsf{R}_{\mathsf{I}}\right)} \ll \frac{1}{\mathsf{R}_{\mathsf{L}} C_{\mathsf{C}}} \tag{8}$$

### **USING LOW-ESR CAPACITORS**

Low-ESR capacitors are recommended throughout this application. A real capacitor can be modeled simply as a resistor in series with an ideal capacitor. The voltage drop across this resistor minimizes the beneficial effects of the capacitor in the circuit. The lower the equivalent value of this resistance, the more the real capacitor behaves like an ideal capacitor.

#### **5-V VERSUS 3.3-V OPERATION**

The TPA122 was designed for operation over a supply range of 2.5 V to 5.5 V. This data sheet provides full specifications for 5-V and 3.3-V operation because these are considered to be the two most common standard voltages. There are no special considerations for 3.3-V versus 5-V operation as far as supply bypassing, gain setting, or stability. The most important consideration is that of output power. Each amplifier in the TPA122 can produce a maximum voltage swing of  $V_{DD}-1$  V. This means, for 3.3-V operation, clipping starts to occur when  $V_{O(PP)}=2.3$  V, as opposed to  $V_{O(PP)}=4$  V for 5-V operation. The reduced voltage swing subsequently reduces maximum output power into the load before distortion begins to become significant.

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#### PACKAGING INFORMATION

Orderable part number	Status	Material type	Package   Pins	Package qty   Carrier	RoHS	Lead finish/	MSL rating/	Op temp (°C)	Part marking
	(1)	(2)			(3)	Ball material	Peak reflow		(6)
						(4)	(5)		
TPA122D	Active	Production	SOIC (D)   8	75   TUBE	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	TPA122
TPA122D.A	Active	Production	SOIC (D)   8	75   TUBE	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	TPA122
TPA122DGN	Active	Production	HVSSOP (DGN)   8	80   TUBE	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	AAE
TPA122DGN.A	Active	Production	HVSSOP (DGN)   8	80   TUBE	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	AAE
TPA122DGNR	Active	Production	HVSSOP (DGN)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	AAE
TPA122DGNR.A	Active	Production	HVSSOP (DGN)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	AAE
TPA122DR	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	TPA122
TPA122DR.A	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	TPA122

<sup>(1)</sup> Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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<sup>(2)</sup> Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

<sup>(3)</sup> RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

<sup>(4)</sup> Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

<sup>(5)</sup> MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

### **PACKAGE OPTION ADDENDUM**

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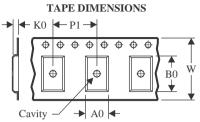
In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

### **PACKAGE MATERIALS INFORMATION**

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### TAPE AND REEL INFORMATION





A0	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

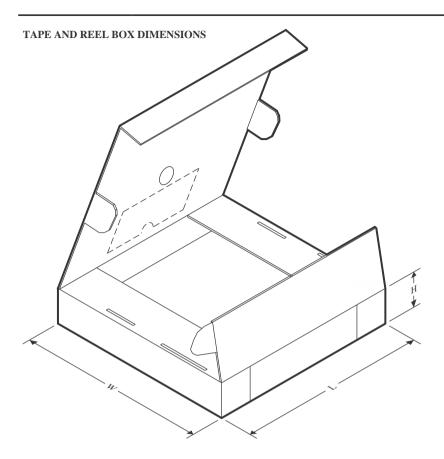


#### \*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPA122DGNR	HVSSOP	DGN	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
TPA122DR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1

### **PACKAGE MATERIALS INFORMATION**

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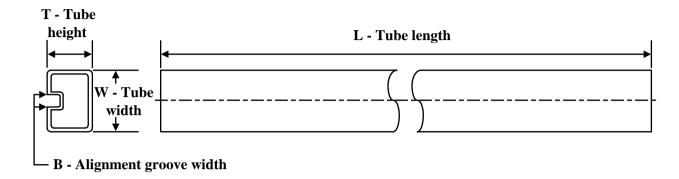
### \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPA122DGNR	HVSSOP	DGN	8	2500	358.0	335.0	35.0
TPA122DR	SOIC	D	8	2500	350.0	350.0	43.0

### **PACKAGE MATERIALS INFORMATION**

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### **TUBE**



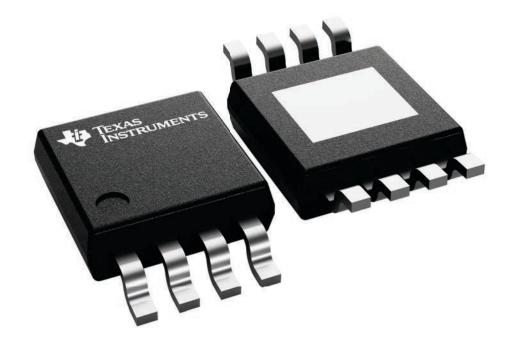
### \*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (µm)	B (mm)
TPA122D	D	SOIC	8	75	505.46	6.76	3810	4
TPA122D.A	D	SOIC	8	75	505.46	6.76	3810	4

3 x 3, 0.65 mm pitch

SMALL OUTLINE PACKAGE

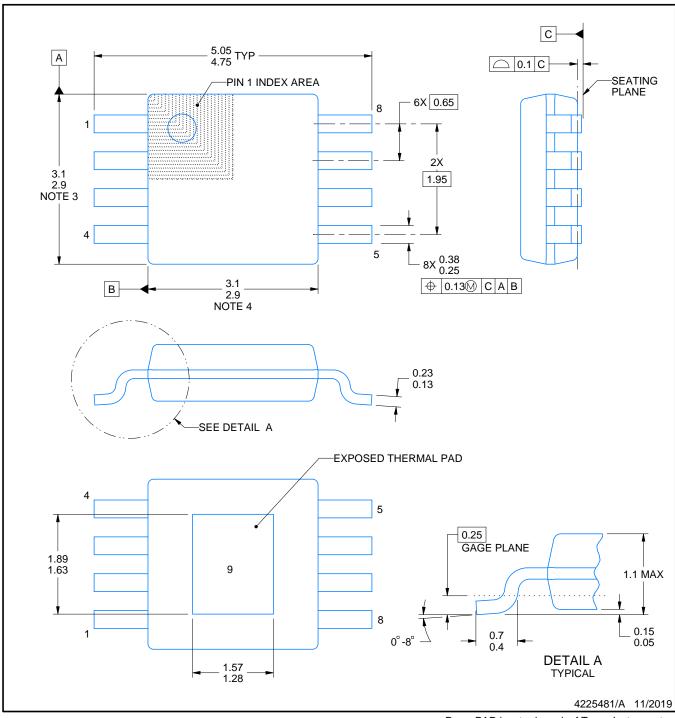
This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.



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## $\textbf{PowerPAD}^{^{\text{\tiny{TM}}}}\,\textbf{VSSOP - 1.1 mm max height}$

SMALL OUTLINE PACKAGE



### NOTES:

PowerPAD is a trademark of Texas Instruments.

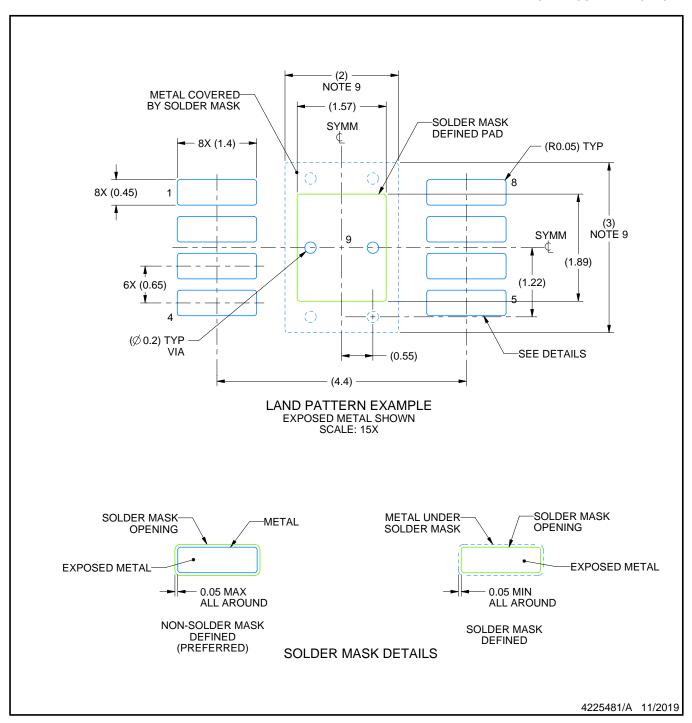
- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

  2. This drawing is subject to change without notice.

  3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-187.



SMALL OUTLINE PACKAGE

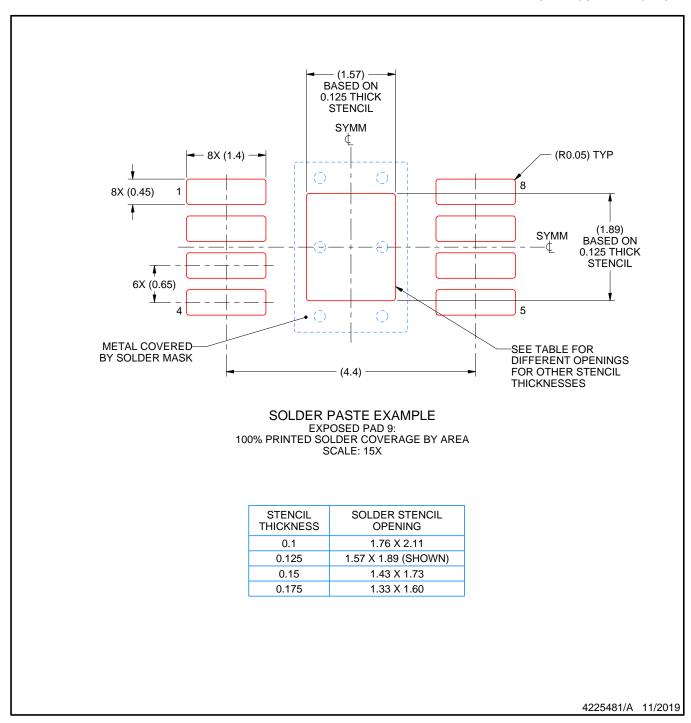


### NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
- 9. Size of metal pad may vary due to creepage requirement.



SMALL OUTLINE PACKAGE



NOTES: (continued)

- 10. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 11. Board assembly site may have different recommendations for stencil design.





SMALL OUTLINE INTEGRATED CIRCUIT



### NOTES:

- 1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.



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