


**SANYO Semiconductors**
**DATA SHEET**

An ON Semiconductor Company

# Bi-CMOS IC

## LV5028TT — LED Driver IC

### Overview

LV5028TT is a High Voltage LED drive controller which drives LED current up to 3A with external MOSFET. LV5028TT is realized very simple LED circuits with a few external parts. It corresponds various wide dimming controls including the TRIAC dimming control.

### Functions

- High Voltage LED Controller
- Various Dimming Control
  - TRIAC & Analog input
- Switching frequency 50kHz
- Low noise switching system
  - 5 stages skip mode Frequency
  - Soft driving
- Selectable Reference voltage
  - Internal 0.605V & External input voltage
- Short Protection Circuit
- Built-in stabilized function

### Specifications

#### Maximum Ratings at Ta = 25°C

Parameter	Symbol	Conditions	Ratings	Unit
Maximum Input voltage	V <sub>IN</sub> max		-0.3 to 42	V
REF_OUT,REF_IN,CS,ACS			-0.3 to 7	V
OUT	V <sub>OUT_abs</sub>		-0.3 to 42	V
OUT2	V <sub>OUT2_abs</sub>		-0.3 to 42	V
Allowable power dissipation	P <sub>d</sub> max	With specified board*	1.0	W
Junction temperature	T <sub>jmax</sub>		150	°C
Operating temperature	T <sub>opr</sub>		-30 to +125	°C
Storage temperature	T <sub>stg</sub>		-40 to +150	°C

\*Specified board: 58.0×54.0×1.6mm (glass epoxy board)

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## Recommended Operating Conditions at $T_a = 25^\circ\text{C}$

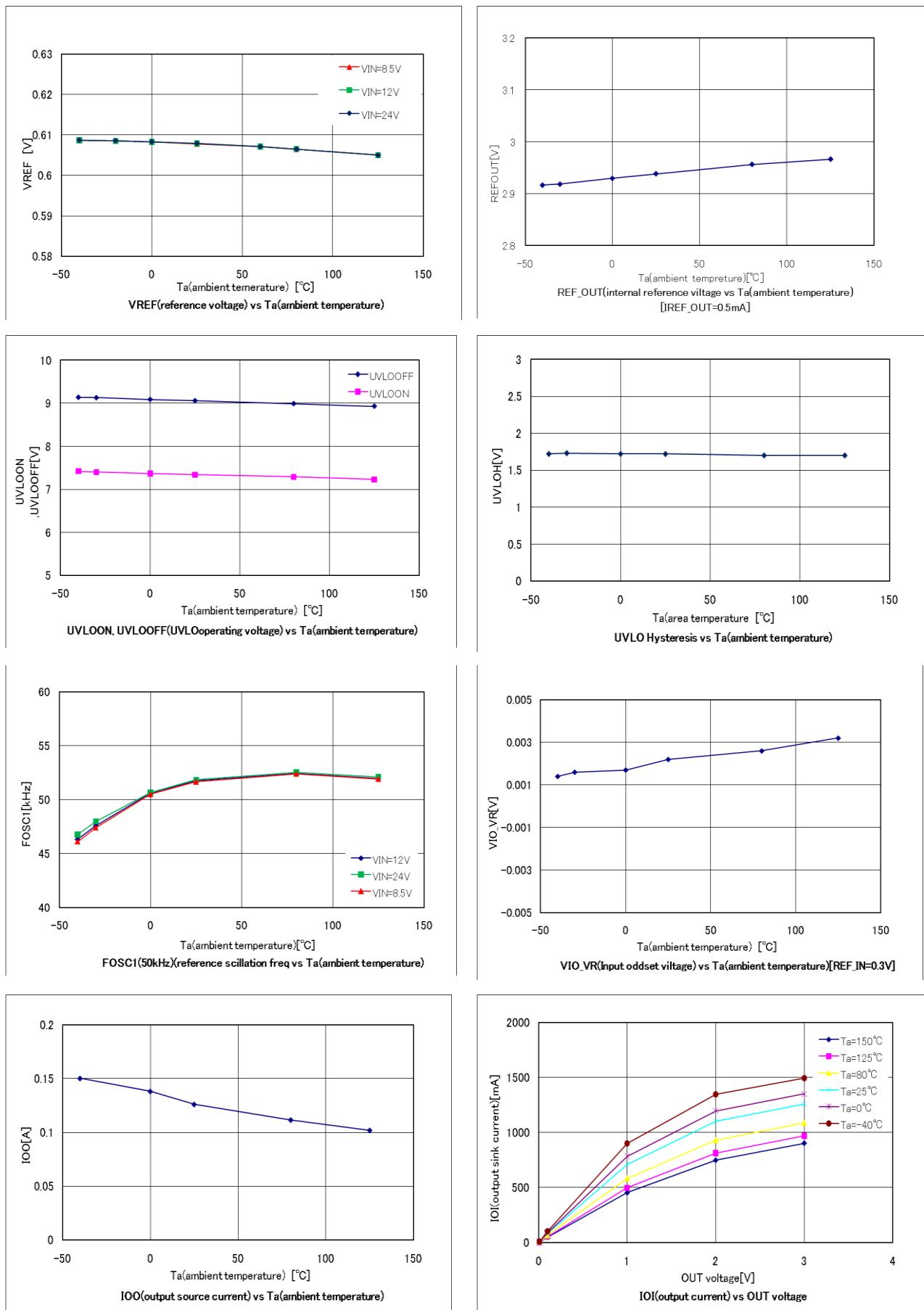
Parameter	Symbol	Conditions	Ratings		Unit
Input voltage	$V_{IN}$		8.5 to 24		V

**Electrical Characteristics** at  $T_a = 25^\circ\text{C}$ ,  $V_{IN} = 12\text{V}$ , unless otherwise specified.

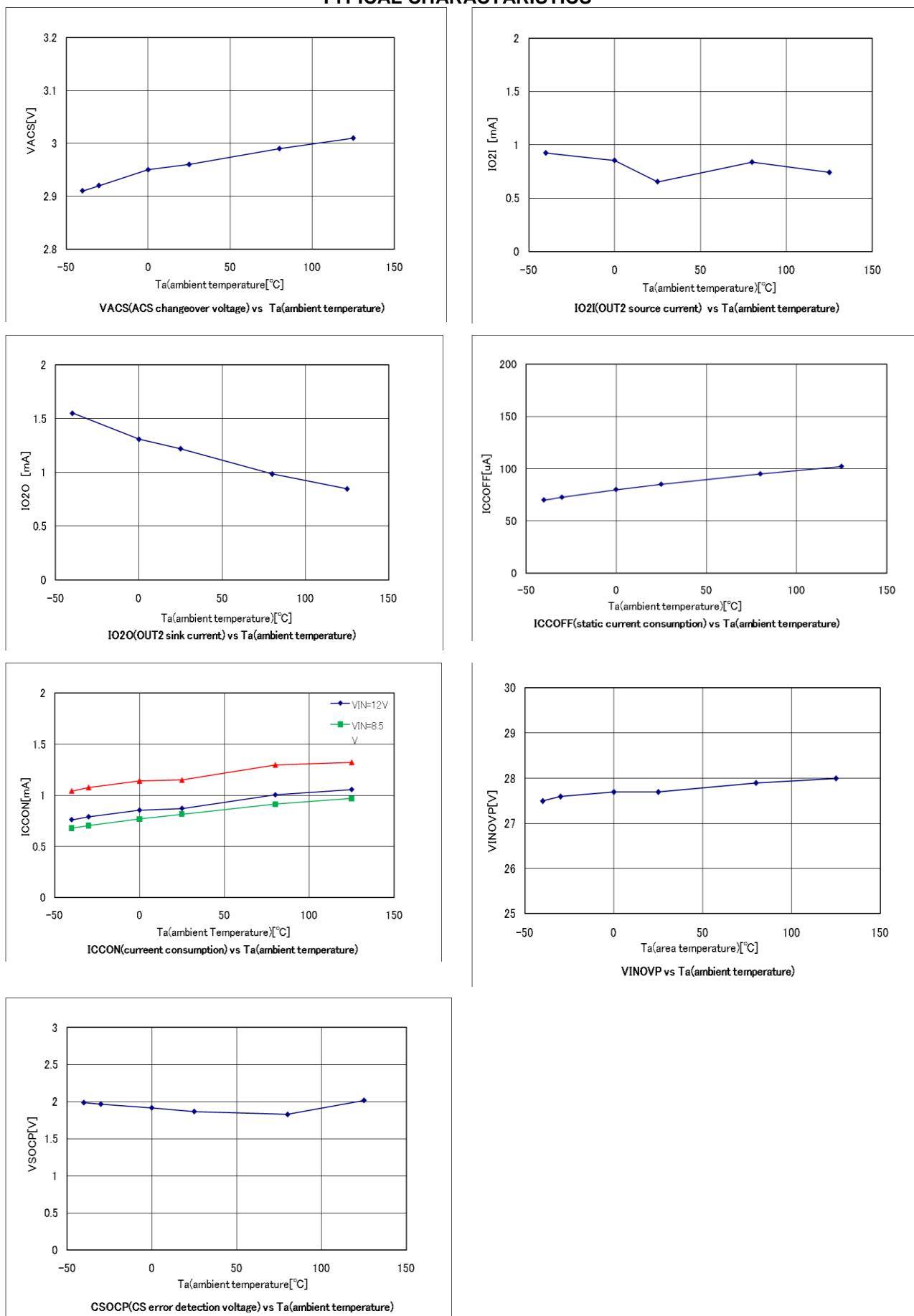
Parameter	Symbol	Conditions	Ratings			Unit
			min	typ	max	
<b>Reference Voltage block</b>						
Built-in Reference Voltage	$V_{REF}$		0.585	0.605	0.625	V
$V_{REF}$ $V_{IN}$ line regulation	$V_{REF\_LN}$	$V_{IN} = 8.5 \text{ to } 24\text{V}$		$\pm 0.5$		%
Reference Output Voltage	$REF_{OUT}$			3.0		V
-Maximum load	$REF_{OUT\_MAX}$		0.5			mA
-equivalent output impedance	$REF_{OUT\_RO}$			10		ohm
<b>Under Voltage Lockout</b>						
Operation Start Input Voltage	$UV_{LOON}$		8	9	10	V
Operation Stop Input Voltage	$UV_{LOOFF}$		6.3	7.3	8.3	V
Hysteresis Voltage	$UV_{LOH}$			1.7		V
<b>Oscillation</b>						
Frequency	$F_{OSC}$		40	50	60	kHz
Maximum ON duty	$MAX_{Duty}$			93		%
<b>Comparator</b>						
Input offset Voltage (Between CS and $V_{REF}$ )	$V_{IO\_VR}$			1	10	mV
Input offset voltage (Between CS and $REF_{OUT}$ )	$V_{IO\_RI}$			1	10	mV
Input current	$I_{IOCS}$			160		nA
	$I_{IOREF}$			80		nA
CS pin max voltage	$V_{OM}$				1	V
malfunction prevention mask time	$T_{MSK}$			150		ns
<b>Thermal protection Circuit</b>						
Thermal shutdown temperature	$T_{SD}$	*Design guarantee		165		°C
Thermal shutdown hysteresis	$\Delta T_{SD}$	*Design guarantee		30		°C
<b>Drive Circuit</b>						
OUT sink current	$I_{OL}$		500	1000		mA
OUT source current	$I_{O\bar{O}}$			120		mA
Minimum On time	$T_{MIN}$			200	300	ns
<b>TRIAC Stabilization Circuit</b>						
Threshold of OUT2	$V_{ACS}$	OUT2=High [ less than right record ]	2.8	3.0	3.2	V
OUT2 sink current	$I_{O2I}$	$V_{IN}=12\text{V}$ , OUT2=6V		0.6		mA
OUT2 source current	$I_{O2O}$	$V_{IN}=12\text{V}$ , OUT2=6V		0.6		mA
<b><math>V_{IN}</math> current</b>						
UVLO mode $V_{IN}$ current	$I_{CCOFF}$	$V_{IN} < UV_{LOON}$		80	120	μA
Normal mode $V_{IN}$ current	$I_{CCON}$	$V_{IN} > UV_{LOON}$ , OUT = OPEN		0.6		mA
<b><math>V_{IN}</math> Over Voltage Protection Circuit</b>						
$V_{IN}$ over voltage protection voltage	$V_{INOP}$		24	27	30	V
VIN Current at OVP	$I_{INOP}$	$V_{IN}=30\text{V}$	0.7	1.0	1.5	mA
<b>CS terminal abnormal sensing circuit</b>						
Abnormal sensing voltage	$CS_{OCP}$			1.9		V

\*: Design guarantee (value guaranteed by design and not tested before shipment)

## TYPICAL CHARACTERISTICS

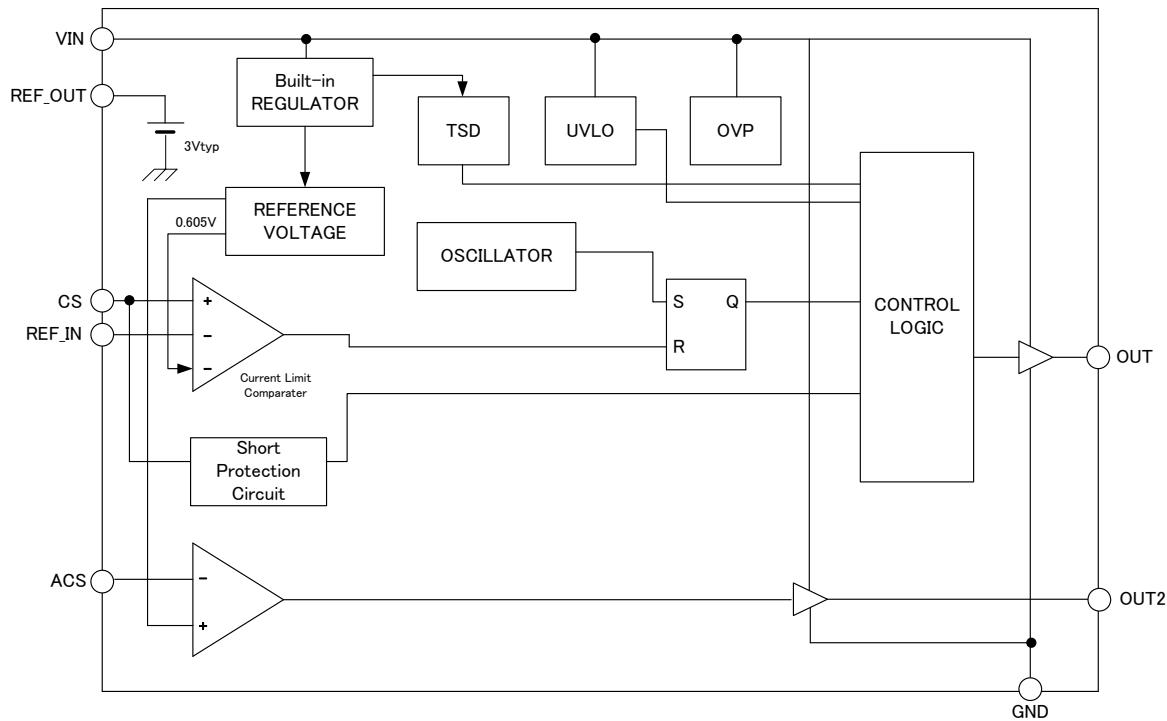


## TYPICAL CHARACTERISTICS



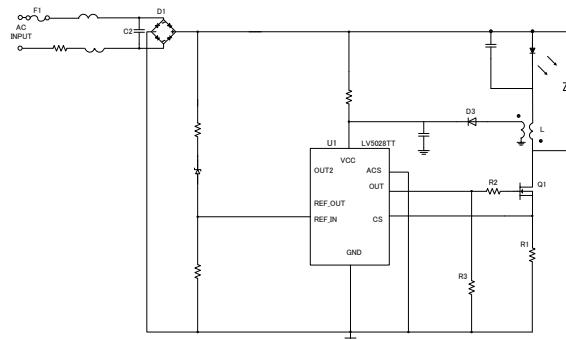
## **TYPICAL CHARACTERISTICS**

## Block Diagram

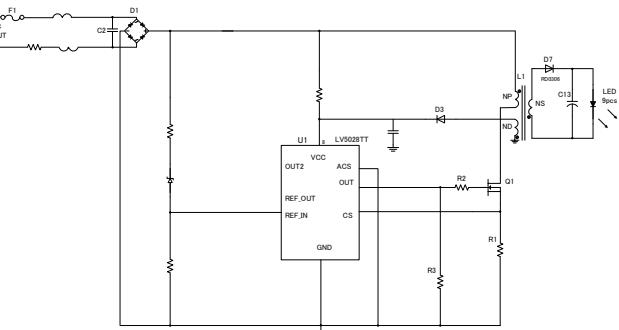


## Sample Application Circuit

## Non isolation

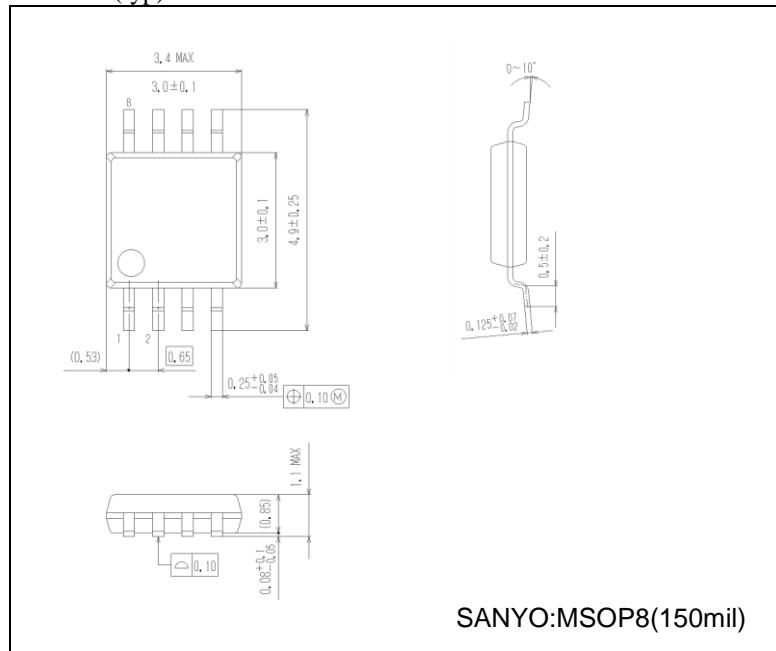


## Isolation

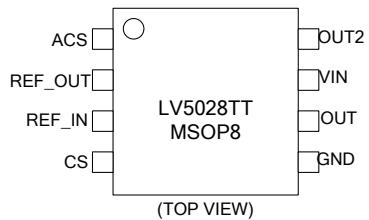


## Package Dimensions

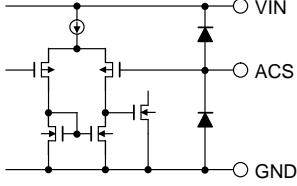
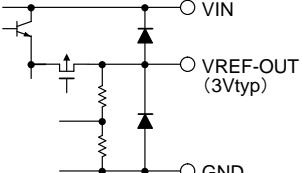
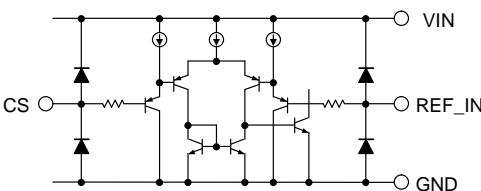
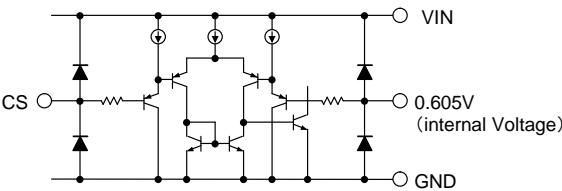
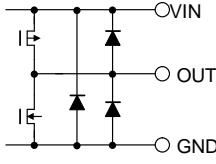
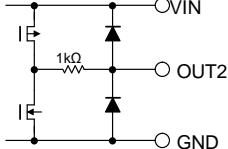
unit: mm (typ)



## Pin Assignment



## Pin Functions

pin No	Pin Name	Pin Function	Equivalent Circuit
1	ACS	ACS pin senses AC Voltage. If this function isn't used, please connect GND.	
2	REF_OUT	Built-in 3V Regulate out Pin. If this function isn't used, please connect to nothing.	
3	REF_IN	External LED current Limit Setting pin. If less than VREF (0.61V) voltage is input, Peak current value is used at the input voltage. If more than REF_IN voltage is input, it is done at VREF voltage. If this function isn't used, please connect nothing.	
4	CS	LED current sensing in. If this terminal voltage exceeds VREF, external FET is OFF. And if the voltage of the terminal exceeds 1.9V, LV5028TT turns to latch-off mode.	
5	GND	GND pin.	
6	OUT	Driving the external FET Gate Pin.	
7	VIN	Power supply pin. Operation : VIN>UVLOON Stop: VIN<UVLOOFF Switching Stop : VIN>VINOVP	
8	OUT2	This pin drive the FET which is stabilized the TRIAC dimming application. If ACS is less than 3V, OUT2 turn High voltage. If this function isn't used, please connect nothing.	

## Relationship between VREF and CS pin voltage

### Relationship between REF\_IN and CS pin voltage (Power Factor Correction (PFC))

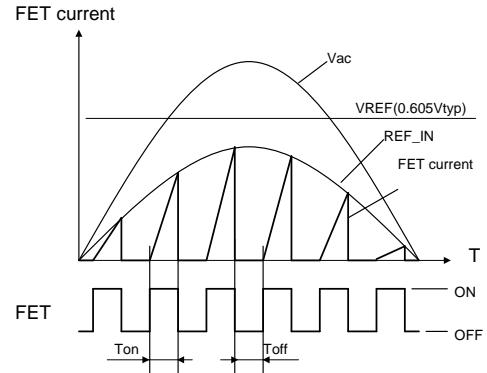
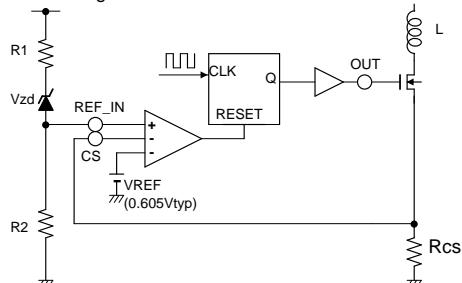
The output current value is the average of the current value that flows during one cycle. The current value that flows into the coil is a triangular wave shown in the figure below. Make sure to set  $I_{pk}$  so that (average of current value at one cycle) is equal to (LED current value).  $I_{pk}$  is set by the relationship between REF\_IN voltage and  $R_{cs}$  voltage. This relationship makes Power Factor Correction (PFC). Therefore, it is available to make LED current a sine curve.

### Setting Zener voltage

$V_{zd}$  depends on LED voltage ( $V_f$ ). Choose Zener diode around  $V_f$  (LED voltage). When  $V_{AC}$  voltage is lower than  $V_f$ , LED operation is not normal. Using Zener diode prevents incorrect operating during  $V_{AC}$  voltage lower than  $V_f$ . In detail, refer to [LED current and inductance setting]

In case of REF\_IN pin open, this error amplifier negative input (-) is under control of internal VREF voltage (0.605Vtyp).

a blockdiagram in outline



$$I_{pk} = \frac{(V_{AC} - V_{zd}) \times \frac{R^2}{R1 + R2}}{R_{cs}}$$

$I_{pk}$ : peak inductor current

$V_f$ : LED forward voltage drop

$V_{AC}$ : effective value, R.M.S value

VREF: Built-in reference voltage (0.605V)

VREF\_IN: REF\_IN voltage (6 pin)

$R_{cs}$ : External sense resistor

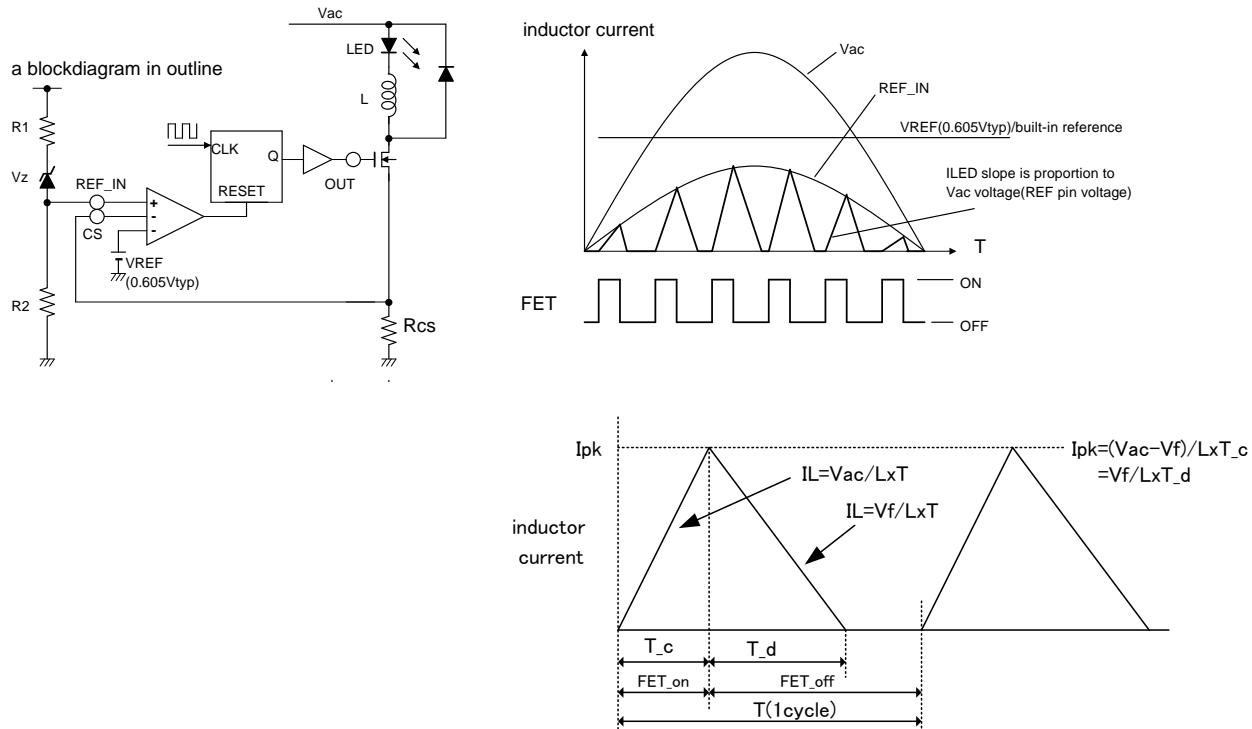
$V_{zd}$ : Zener diode voltage (REF\_IN pin)

## LED current and inductance setting

It is available to use both no-isolation and isolation applications.

### (For non-isolation application)

The output current value is the average of the inductor current value that flows during one cycle. The current value that flows into inductor is a triangular wave shown in the figure below. Make sure to set  $I_{pk}$  so that (average of inductor current value at one cycle) is equal to (LED current value).



Given that the period when current flows into coil is

$$\text{DutyI} = \frac{T_c + T_d}{T},$$

$$I_{pk} \times \frac{1}{2} \times (\text{DutyI} \times T) / T = I_{LED}$$

$$I_{pk} = \frac{2 \times I_{LED}}{\text{DutyI}} \quad (1) \quad \text{since} \quad I_{pk} = \frac{V_{REF\_IN}}{R_{cs}}$$

$$R_{cs} = \frac{V_{REF\_IN}}{I_{pk}} = \frac{\text{DutyI} \times V_{REF\_IN}}{2 \times I_{LED}} \quad (2)$$

$I_{pk}$ : peak inductor current

$V_f$ : LED forward voltage drop

$V_{ac}$ : effective value(R.M.S value)

$V_{REF}$ : Built-in reference voltage (0.605V)

$V_{REF\_IN}$ : $REF\_IN$  voltage(6 pin)

$R_s$ : External sense resistor

$V_{zd}$ :Zener diode voltage( $REF\_IN$  pin)

Since formula for LED current is different between on period and off period as shown above,

$$I_{pk} = \frac{V_{ac} - V_f}{L} \times T_c = \frac{V_f}{L} \times T_d \quad (3).$$

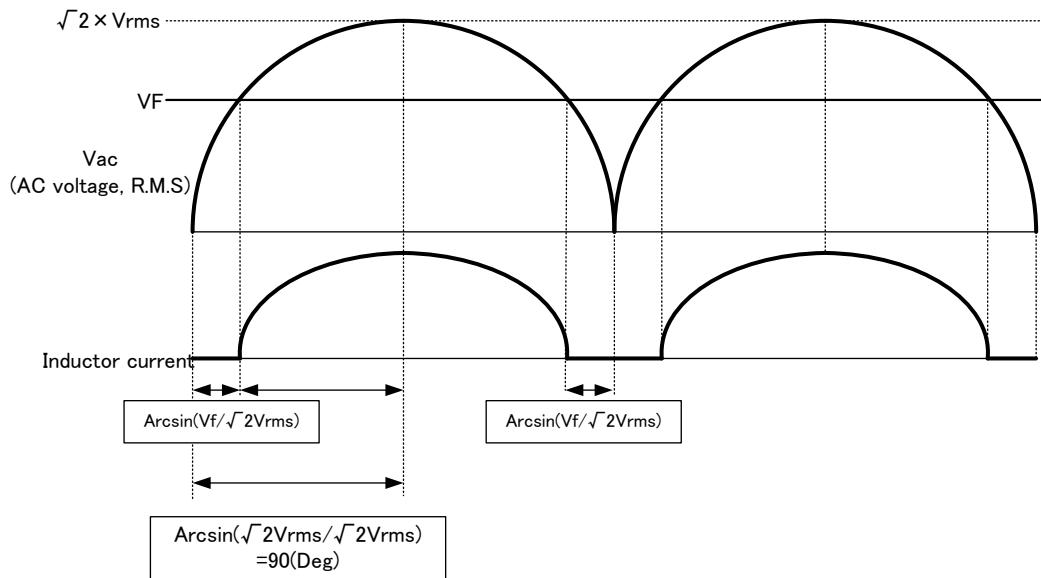
$$\text{Since} \quad T_c + T_d = \text{DutyI} \times T, \quad T_c = \text{DutyI} \times T - T_d \quad (4)$$

$$\text{Based on the result of (3) and (4),} \quad T_d = \text{DutyI} \times T \times \frac{V_{ac} - V_f}{V_{ac}} \quad (5)$$

To obtain  $L$  from the equation (1), (3), (5),

$$L = \frac{V_f \times \text{DutyI}}{2 \times I_{LED}} \times \text{DutyI} \times T \times \frac{V_{ac} - V_f}{V_{ac}} = \frac{V_f}{2 \times I_{LED}} \times \frac{1}{f_{osc}} \times \frac{V_{ac} - V_f}{V_{ac}} \times (\text{DutyI})^2 \quad (6)$$

Since LED and inductor are connected in serial in non-isolation mode, LED current flows only when AC voltage exceed  $V_f$ .



Given that the ratio of inductor current to AC input is DutyAC.

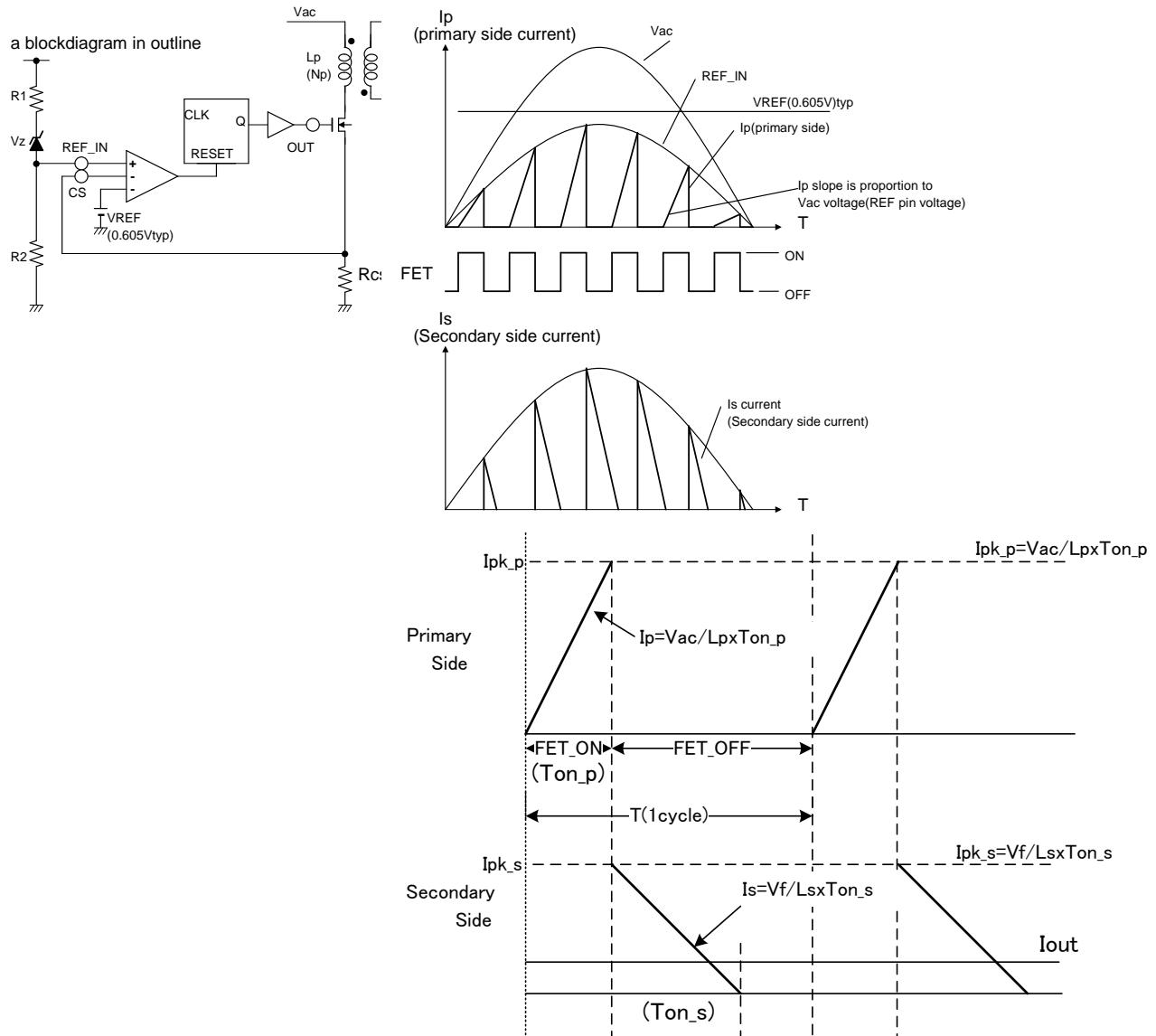
$$DutyAC = \frac{90 - \arcsin\left(\frac{Vf}{\sqrt{2}Vrms}\right)}{90}$$

Since the period when the inductor current flows are limited by DutyAC, the formula (6) is represented as follows:

$$L = \frac{Vf}{2 \times ILED} \times \frac{1}{fosc} \times \frac{Vac - Vf}{VIN} \times (DutyI)^2 \times \left( \frac{90 - \arcsin\left(\frac{Vf}{\sqrt{2}Vrms}\right)}{90} \right)^2 \quad (7)$$

## (for Isolation application)

Using the circuit diagram below, the wave form of the current that flows to Np and Ns is as follows.  
Current waveform flows to primary side and secondary.



[Inductance  $L_p$  of primary side and sense resistor  $R_s$ ]

If a peak current flow to transformer is represented as  $I_{pk\_p}$ , the power ( $P_{in}$ ) charged to the transformer on primary side can be represented as:

$$P_{in} = \frac{1}{2} \times L_p \times (I_{pk\_p})^2 \times f_{osc} \quad (11).$$

$$\therefore I_{pk\_p} = \frac{V_{ac}}{L_p} \times T_{on\_p} \quad (12)$$

$$\therefore L_p = \frac{V_{ac}^2 \times T_{on\_p}^2 \times f_{osc}}{2 \times P_{in}} = \frac{V_{ac}^2 \times D_{on\_p}^2}{2 \times P_{in} \times f_{osc}} \quad (13)$$

$$(D_{on\_p} = \frac{T_{on\_p}}{T} = T_{on\_p} \times f_{osc})$$

To substitute the following to the formula below,

$$\therefore \eta = \frac{P_{out}}{P_{in}} \quad (14)$$

$$\therefore L_p = \frac{V_{ac}^2 \times T_{on\_p}^2 \times f_{osc} \times \eta}{2 \times P_{out}} = \frac{V_{ac}^2 \times D_{on\_p}^2 \times \eta}{2 \times P_{out} \times f_{osc}} \quad (15)$$

Sense resistor is obtained as follows.

$$Rs = \frac{Vref}{Ipk\_p} = \frac{VREF\_IN \times Lp}{Vac \times Ton\_p} = \frac{VREF\_IN \times Lp}{Vsc \times Don\_p \times T} \quad (16)$$

[Inductance Ls of secondary side]

Since output current  $Iout$  is the average value of current flows to transformer of secondary side

$$Iout = Ipk\_s \times \frac{Ton\_s}{T} \times \frac{1}{2} = \frac{Ipk\_s \times Don\_s}{2} \quad (Don\_s = \frac{Ton\_s}{T} = Ton\_s \times fosc) \quad (17)$$

$$Ipk\_s = \frac{Vout}{Ls} \times Ton\_s = \frac{Vout}{Ls} \times \frac{Don\_s}{f} \quad (18)$$

$$Ls = \frac{Vout \times T \times Don\_s^2}{2 \times Iout} = \frac{Vout \times Don\_s^2}{2 \times Iout \times fosc} = \frac{Vout^2 \times Don\_s^2}{2 \times Pout \times fosc} \quad (19)$$

Calculation of the ratio of transformer coil on primary side and secondary side

Since ratio and inductance of transformer coil is

$$\frac{Ns}{Np} = \frac{\sqrt{Ls}}{\sqrt{Lp}} \quad (20)$$

substituted equations (15), (19) for (20)

$$\therefore \frac{Np}{Ns} = \frac{Vdc \min}{Vout} \times \sqrt{\eta} \times \frac{Don\_p}{Don\_s} \quad (21)$$

Calculation of transformer coil on primary side and secondary side

$$N = \frac{Vac \times 10^8}{2 \times \Delta B \times Ae \times f} \quad (22)$$

$\Delta B$  : variation range of core flux density [Gauss]

$Ae$  : core section area [ $\text{cm}^2$ ]

To use Al (L value at 100T),

$$N = \sqrt{\frac{L}{Al}} \times 10^2 \quad (23)$$

L : inductance [uH]

Al: L value at 100T [ $\text{uH/N}^2$ ]

lg (Air gap) is obtained as follows:

$$lg = \frac{\mu_r \mu_0 N^2 A_e 10^2}{L} \quad (24)$$

$\mu_r$ : relative magnetic permeability,  $\mu_r = 1$

$\mu_0$ : vacuum magnetic permeability  $\mu_0 = 4\pi \times 10^{-7}$

N: turn count [T]

Ae: core section area [ $\text{m}^2$ ]

L: inductance [H]

## Bleeder current circuit for TRIAC dimmer

### 1. Operating voltage setting

ACS pin voltage set operating voltage at OUT2. ACS pin threshold voltage is 3Vtyp.

OUT2 operating voltage is set by R1 and R2. R1 and R2 is determined below.

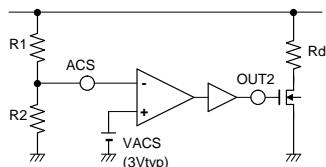
$$ACS = Vac \times \frac{R2}{R1 + R2}$$

### 2. Bleeder current setting

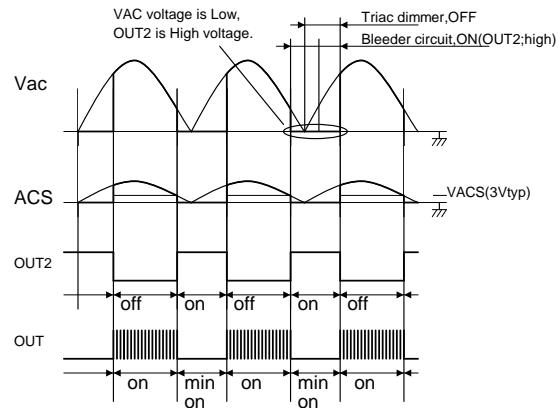
Rd set hold current at Triac dimmer.

Bleeder current is set at Rd depending on Triac dimmer.

a blockdiagram in outline



a blockdiagram in outline

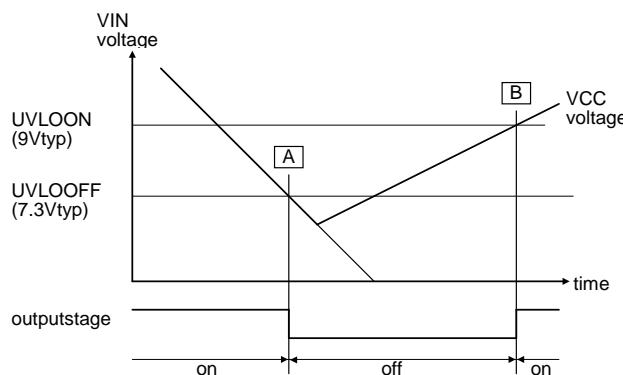


## Description of operating protection function

	title	outline	monitor point	note
1	UVLO	Under Voltage Lock Out	VIN voltage	
2	OCP	Over Current Protection	CS voltage	equivalent FET current
3	OVP	Over Voltage Protection	VIN voltage	
4	OTP (TSD)	Over Temperature Protection (Thermal Shut Down)	PN Junction temperature	

### 1.UVLO(Under Voltage Lock Out)

If VIN voltage is 7.3V or lower, then UVLO operates and the IC stops. When UVLO operates, the power supply current of the IC is about 80uA or lower. If VIN voltage is 9V or higher, then the IC starts switching operation.

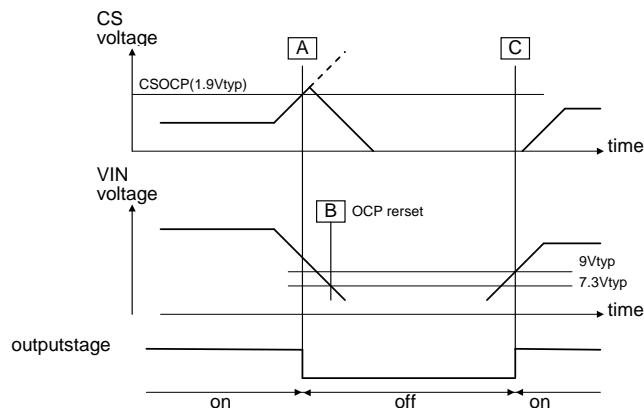


### 2.OCP(Over Current Protection)

The CS pin sense the current through the MOS FET switch and the primary side of the transformer. This provides an additional level of protection in the event of a fault. If the voltage of the CS pin exceeds VCSOCP(1.9Vtyp)(A), the internal comparator will detect the event and turn off the MOSFET. The peak switch current is calculated

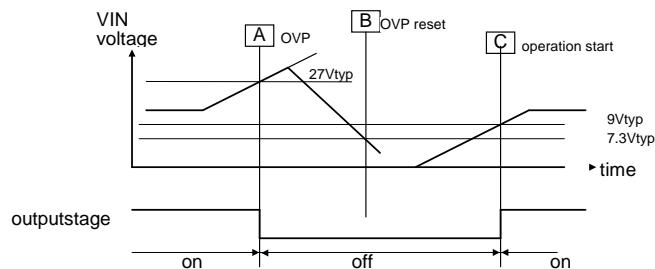
$$I_{o(\text{peak})} [A] = V_{SOCP} [V] / R_{sense} [\text{ohm}]$$

The VIN pin is pulled down to fixed level, keeping the controller latched off. The latch reset occurs when the user disconnects LED from VAC and lets the VIN falls below the VIN reset voltage,UVLOOFF(7.3Vtyp)(B). Then VIN rise UVLOON(9Vtyp)(C),restart the switching.



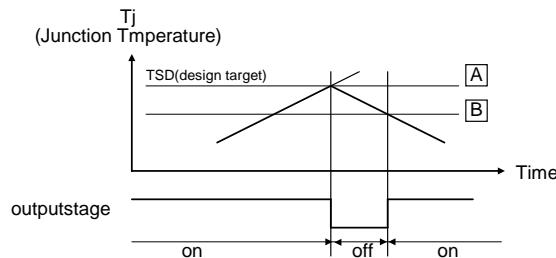
### 3.OVP(Over Voltage Protection)

If the voltage of VIN pin is higher than the internal reference voltage VINOVP(27Vtyp), switching operation is stopped. The stopping operation is kept until the voltage of VIN is lower than 7.3V. If the voltage of VIN pin is higher than 9V, the switching operation is restated.



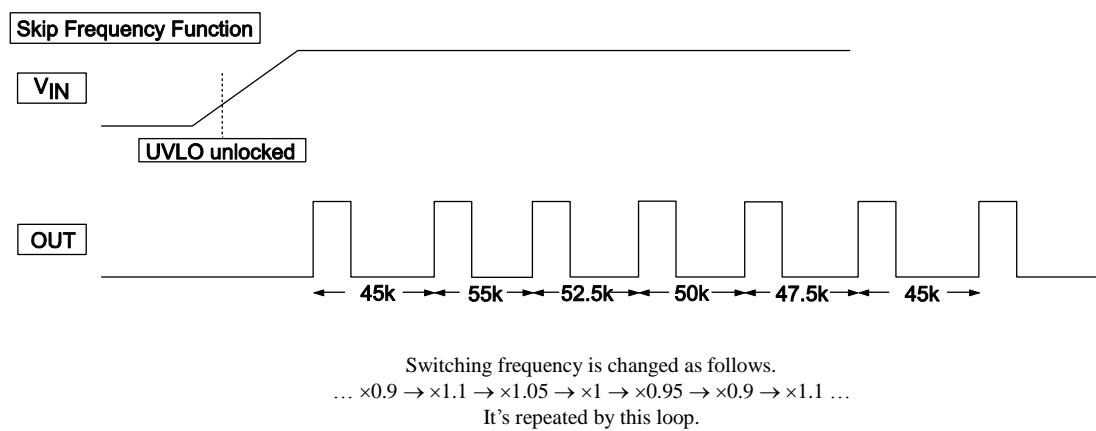
### 4.TSD(Thermal Shut Down protection)

The thermal shutdown function works when the junction temperature of IC is  $165^{\circ}\text{C}$  (typ) (A), and the IC switching stops. The IC starts switching operation again when the junction temperature is  $135^{\circ}\text{C}$ typ (B) or lower.



### Skip frequency function

LV5028TT contains the skip frequency function for reduction of the peak value of conduction noise. This function changes the frequency as follows.



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