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Low cost monolithic accelerometers may be paired with a circuit whose output changes with frequency (V/F) to provide a TTL level frequency output. A microprocessor can be easily programmed to read this signal and directly compute the applied acceleration, and the output of a V/F circuit can be sent down a long transmission line and still be reliably recovered at the other end.

A circuit whose output frequency varies directly with applied acceleration is shown in Figure 1. The circuit operates from a single +9 V or +12 V power supply.

An ADXL05, $\pm 5\text{ g}$ accelerometer directly converts any applied acceleration into an analog output voltage which then controls the output frequency of an AD654 low cost voltage-to-frequency converter IC. The frequency output appears at Pin 1 of the AD654. Total chip cost for this circuit is approximately \$20.00 (in 1000s).

The voltage output at Pin 8 of the ADXL05 is +2.5 volts with no acceleration and varies 200 mV above or below that value for each 1 *g* (positive or negative) of applied acceleration.

Figure 1 is a schematic diagram of the AD654 circuit. The diagram shows the internal components of the AD654, including a DRIVER, OSC, and a differential amplifier. The circuit is connected to $+V_S$ and $-V_S$ supply rails. Key components include resistors R_S , R_5 , R_T , and R_4 ; capacitors C_T and C_4 ; and a diode IN4733. The output is labeled F_{OUT} . A table provides the values for R_S based on the supply voltage:

$+V_S$	R_S
+12V	432 Ω
+9V	249 Ω

Figure 1. A High Performance Acceleration-to-Frequency Circuit

The output scale factor of the accelerometer (at Pin 9) is set by the resistors R3 & R1 of the on-chip buffer amplifier. Resistor R2 is used to change the 0 g output level to a convenient +2.5 V (which provides the maximum output voltage swing). Capacitor C5 and Resistor R3 form a low-pass filter which improves the circuit's signal-to-noise ratio.

Figure 2 shows the same circuit modified for use with the ADXL50, a ± 50 g accelerometer. The accelerometer's 3 dB bandwidth is again set by R3 & C5. In Figure 2, both a zero g offset and a scale factor trim potentiometer have been added to allow the user to adjust the circuit to extremely high accuracy; trim potentiometers may also be added to the circuit of Figure 1. R1a should be approximately 50% the value of R1b (for a $\pm 20\%$ trim range). Note: for the best mechanical stability the trim potentiometers should be measured (after calibration is complete) and replaced with 1% resistors.

Design example: Circuit of Figure 2

Design example: Wanted . . . 0 g frequency = 10 kHz,
Scale Factor = 100 Hz/g, BW = 200 Hz.

A 50 g signal will cause a frequency variation of 5 kHz.

Therefore:

$$F_{OUT} \text{ for } \pm 50 \text{ g} = 10 \text{ kHz} \pm 5 \text{ kHz} = 5 \text{ kHz} - 15 \text{ kHz}$$

Let $C_T = 0.01 \mu\text{F}$, then for a 0 g frequency of 10 kHz:

$$R_T = \frac{0.25}{10 \text{ kHz } C_T} = 2.5 \text{ k}\Omega$$

Let $R_3 = 49.9 \text{ k}\Omega$, for a scale factor of 100 Hz/g:

$$R_1 = \frac{19 \text{ mV/g} \times R_3}{100 \text{ Hz/g } 10,000 R_T C_T} = 52.7 \text{ k}\Omega$$

For R_1 , use a 42.2 k Ω fixed resistor & a 20 k Ω trim potentiometer.

For a 200 Hz bandwidth:

$$C_5 = \frac{1}{2\pi 200 R_3} = 0.016 \mu\text{F}$$

The accelerometer may be self-calibrated by using the Earth's gravity. With the accelerometer's tab pointed 90° to the vertical (i.e., to either side), the accelerometer will measure 0 g, allowing the 0 g offset to be adjusted. With the accelerometer's tab pointing down, its output at Pin 9 will correspond to +1 g. If the accelerometer is rotated 180° it will then measure -1 g. The 2 g difference in the readings can then be used to set the circuit's over-

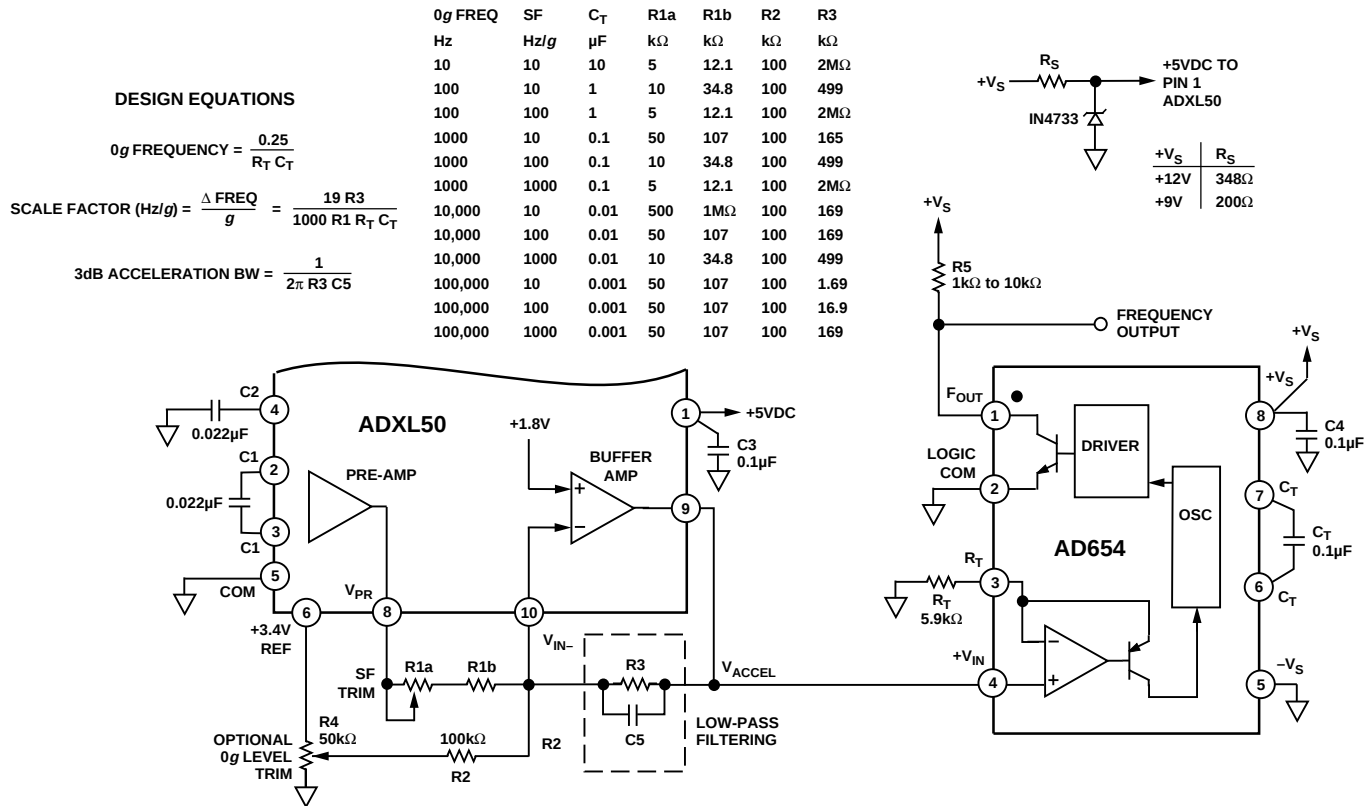


Figure 2. A ± 50 g Acceleration-to-Frequency Circuit

all scale factor. The 0 *g* & full-scale frequency adjustments should be repeated a couple of times to get the highest accuracy.

An Accelerometer Tilt Sensor with a Frequency Output

Figure 3 shows how an ADXL05 accelerometer can be connected to a low cost CMOS 555 timer to provide a frequency output. The component values indicated were selected for a ± 1 *g* tilt application.

The nominal 200 mV/*g* output of the accelerometer appears at Pin 8 and is gained-up by a factor of 2 to a 400 mV/*g* level by the onboard buffer amplifier. The 0 *g* bias level at Pin 9 is approximately 1.8 V. Capacitor C4 and Resistor R3 form a 16 Hz low-pass filter to lower noise and improve the measurement resolution.

The CMOS 555 operates as a voltage controlled oscillator where R5, R6, and C5 set the nominal operating frequency. Resistors R5 & R6 were chosen to give an approximate 50% duty cycle with a +1.8 V (0 *g*) input signal applied to Pin 5 of the 555. To prevent any change in frequency due to supply variations, the 555 operates from the accelerometer's +3.4 V reference rather than directly off the +5 V supply.

The output frequency of this circuit is determined by the charge and discharge times set by R5, R6, and C5.

Using the circuit and component values shown in Figure 3, the output scale factor at Pin 9 of the accelerometer will be ± 400 mV/*g* so the voltage output will be $+1.8$ V $\pm$ 0.4 V. The output scale factor at Pin 3 of the 555 will be approximately 16,500 Hz $\pm$ 2,600 Hz per *g*. Figure 4 shows the circuit's output frequency vs. the voltage occurring at Pin 5 of the 555.

Frequency stability of this circuit is quite good. With a 15.5 kHz 0 *g* frequency, the measured 0 *g* frequency drift over the 0°C to +70°C commercial temperature range was 5 Hz/°C which is 0.03%/°C. The change in frequency vs. supply voltage is less than 10 Hz with a +5.0 volt to +9.0 volt supply range.

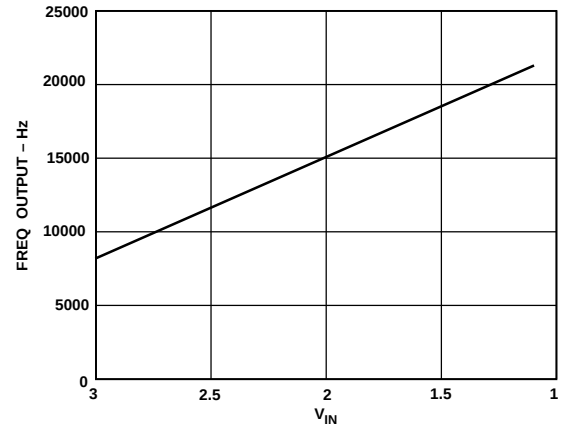


Figure 4. Frequency Output vs. Voltage Input for the Circuit of Figure 3

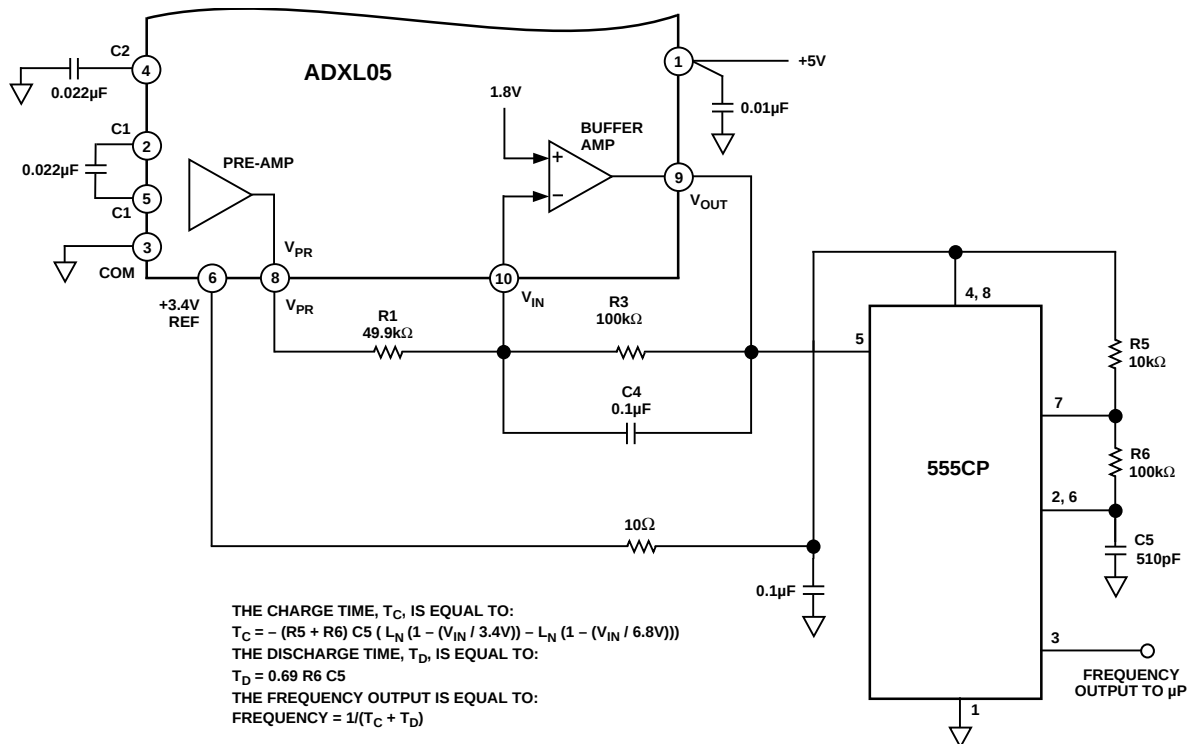


Figure 3. A Low Cost Accelerometer Tilt Sensor with a Frequency Output

