

# **Smart Highside Power Switch**

#### Reversave™

 Reverse battery protection by self turn on of power MOSFET

#### **Features**

- Short circuit protection
- Current limitation
- Overload protection
- Thermal shutdown
- Overvoltage protection (including load dump)
- Loss of ground protection
- Loss of V<sub>bb</sub> protection (with external diode for charged inductive loads)
- Very low standby current
- Fast demagnetisation of inductive loads
- Electrostatic discharge (ESD) protection
- Optimized static **e**lectro**m**agnetic **c**ompatibility (**EMC**)

### **Diagnostic Function**

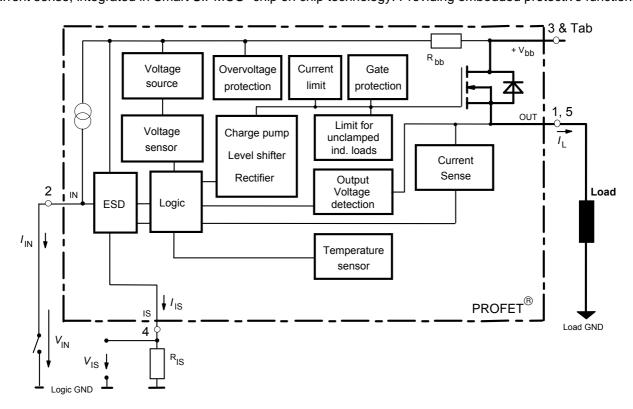
• Proportional load current sense (with defined fault signal during thermal shutdown)

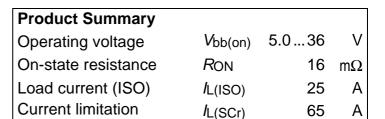
#### **Application**

- Power switch with current sense diagnostic feedback for 12V and 24 V DC grounded loads
- All types of resistive, capacitive and inductive loads (no PWM with inductive loads)
- Replaces electromechanical relays, fuses and discrete circuits

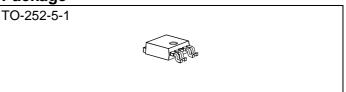
#### **General Description**

N channel vertical power FET with charge pump, current controlled input and diagnostic feedback with load current sense, integrated in Smart SIPMOS® chip on chip technology. Providing embedded protective functions.





#### **Package**





Pin	Symbol		Function
1	OUT	0	Output to the load. The pin 1 and 5 must be shorted with each
			other especially in high current applications!*)
2	IN	I	Input, activates the power switch in case of short to ground
Tab/(3)	Vbb	+	Positive power supply voltage, the tab is shorted to this pin.
4	IS	S	Diagnostic feedback providing a sense current proportional to the load current; high current on failure (see Truth Table on page 6)
5	OUT	0	Output to the load. The pin 1 and 5 must be shorted with each
			other especially in high current applications!*)

<sup>\*)</sup> Not shorting all outputs will considerably increase the on-state resistance, reduce the peak current capability and decrease the current sense accuracy

# **Maximum Ratings** at $T_j = 25$ °C unless otherwise specified

Parameter	Symbol	Values	Unit
Supply voltage (overvoltage protection see page 4)	V <sub>bb</sub>	36	V
Supply voltage for full short circuit protection	$V_{ m bb}$	241)	V
(see also diagram on page 9) $T_j$ =-40150 °C:			
Load dump protection $V_{\text{LoadDump}} = U_{\text{A}} + V_{\text{S}}$ , $U_{\text{A}} = 13.5 \text{ V}$ $R_{\text{I}} = 2 \Omega$ , $R_{\text{L}} = 2.7 \Omega$ , $t_{\text{d}} = 200 \text{ ms}$ , IN= low or high	V <sub>Load dump<sup>2)</sup></sub>	60	V
Load current (Short-circuit current, see page 4)	<i>I</i> L	self-limited	Α
Operating temperature range	T <sub>j</sub>	-40+150	°C
Storage temperature range	$T_{stg}$	-55+150	
Power dissipation (DC) TC ≤ 25°C	P <sub>tot</sub>	42	W
Inductive load switch-off energy dissipation, single pulse U=12V, I=10A, L=3mH $T_j$ =150 °C:	E <sub>AS</sub>	0.15	J
Electrostatic discharge capability (ESD) (Human Body Model) acc. ESD assn. std. S5.1-1993; R=1.5kΩ; C=100pF	V <sub>ESD</sub>	4.0	kV
Current through input pin (DC)	I <sub>IN</sub>	+15, -100	mA
Current through current sense pin (DC)	I <sub>IS</sub>	+15, -100	
see internal circuit diagrams page 7			

<sup>1)</sup> Short circuit is tested with  $100m\Omega$  and  $20\mu H$ 

 $<sup>^{2)}</sup>$   $V_{Load\ dump}$  is set-up without the DUT connected to the generator per ISO 7637-1 and DIN 40839



# **Thermal Characteristics**

Parameter and Conditions		Symbol	Values			Unit
			min	typ	max	
Thermal resistance	chip - case:	$R_{\rm thJC}^{3)}$			1.5	K/W
junction - ambient (free air):		$R_{thJA}$		80		
SMD ve	ersion, device on PCB4):			45		

# **Electrical Characteristics**

Parameter and Conditions	Symbol		Values		Unit
at $T_j$ = -40°C150°C, $V_{bb}$ = 12 V unless otherwise specified		min	typ	max	

## **Load Switching Capabilities and Characteristics**

R <sub>ON</sub>		13	16	mΩ
		25	31	
V <sub>ON(NL)</sub>		50		mV
				Α
I <sub>L(ISO)</sub>	21	25		
$I_{L(nom)}$	6.2	7.6		
<i>t</i> on	150		410	μs
t <sub>off</sub>	70		410	
dV/dt <sub>on</sub>	0.1		1	V/µs
-d V/dt <sub>off</sub>	0.1		1	V/µs
	$V_{ m ON(NL)}$ $I_{ m L(ISO)}$ $I_{ m L(nom)}$ $t_{ m on}$ $t_{ m off}$	VON(NL)          IL(ISO)       21         IL(nom)       6.2         ton       150         toff       70         dV/dton       0.1	25   V <sub>ON(NL)</sub>     50	Image: Control of the control of t

Thermal resistance R<sub>thCH</sub> case to heatsink (about 0.5 ... 0.9 K/W with silicone paste) not included!

<sup>4)</sup> Device on 50mm\*50mm\*1.5mm epoxy PCB FR4 with 6cm² (one layer, 70μm thick) copper area for V<sub>bb</sub> connection. PCB is vertical without blown air.



Parameter and Conditions	Symbol	Values		Unit	
at $T_j$ = -40°C150°C, $V_{bb}$ = 12 V unless otherwise specified		min	typ	max	

## **Operating Parameters**

Operating voltage (V <sub>IN</sub> =0V)		V <sub>bb(on)</sub>	5.0		36	V
Undervoltage shutdown 5)		$V_{bIN(u)}$	1.5	3.0	4.5	V
Undervoltage restart of charge pump (V <sub>IN</sub> =0V)		$V_{ m bb(ucp)}$	3.0	4.5	6.0	V
Overvoltage protection 6)  /bb=15 mA		$V_{Z,IN}$	61	68		V
Standby current	<i>T</i> <sub>j</sub> =-40+25°C:	I <sub>bb(off)</sub>		2	5	μΑ
/ <sub>IN</sub> =0	<i>T</i> <sub>j</sub> =150°C:			4	8	

## Protection Functions 7)

Short circuit current limit (Tab to pin 1,5)					
$V_{\rm ON}$ =8V, time until limitation max. 300 $\mu$ s					
Τ <sub>j</sub> =-40°C: Τ <sub>j</sub> =25°C: Τ <sub>j</sub> =+150°C:	I <sub>L(SC)</sub>	35 35 35	75 65 65	110 110 125	A
Repetitive short circuit current limit, $T_j = T_{jt}$	I <sub>L(SCr)</sub>		65		Α
Output clamp (inductive load switch off) at $V_{\text{OUT}} = V_{\text{bb}} - V_{\text{ON(CL)}}$ (e.g. overvoltage) $I_{\text{L}} = 40 \text{ mA}^{8}$	V <sub>ON(CL)</sub>	38	42	48	V
Thermal overload trip temperature	$T_{jt}$	150			°C
Thermal hysteresis	$\Delta T_{\rm jt}$		10		K

# **Reverse Battery**

Reverse battery voltage	-V <sub>bb</sub>	 	20	V
On-state resistance (pin 1,5 to pin 3)				
$V_{\rm bb} = -8 \text{V}, \ V_{\rm IN} = 0, \ I_{\rm L} = -5 \text{ A}, \ R_{\rm IS} = 1 \text{ k}\Omega,  T_{\rm j} = 25 \text{ °C}$ :	$R_{ON(rev)}$	 	22	$m\Omega$
$V_{\text{bb}}$ = -12V, $V_{\text{IN}}$ = 0, $I_{\text{L}}$ = -5 A, $R_{\text{IS}}$ = 1 k $\Omega$ , $T_{\text{i}}$ =25 °C:		 16	19	
<i>T</i> <sub>j</sub> =150 °C:		25	32	
Integrated resistor in V <sub>bb</sub> line	R <sub>bb</sub>	 200		Ω

<sup>5)</sup> VbIN=Vbb-VIN see diagram on page 11.

 $<sup>^{6)}</sup>$  see also  $V_{
m ON(CL)}$  in circuit diagram on page 7.

<sup>7)</sup> Integrated protection functions are designed to prevent IC destruction under fault condition described in the data sheet. Fault conditions are considered as "outside" normal operating range. Protection functions are not for continuous repetitive operation.

<sup>8)</sup> see also page 12.



## **Diagnostic Characteristics**

Current sense ratio, static on-condition $k_{\rm RLIS} = h_{\rm c} : h_{\rm S}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm S}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c} : h_{\rm c} : h_{\rm c} : h_{\rm c}$ $k_{\rm RLIS} = h_{\rm c} : h_{\rm c$	Diagnostic Characteristics					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		<b>k</b> <sub>ILIS</sub>		8200		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$K_{\text{ILIS}} = I_{\text{L}} : I_{\text{IS}}$					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$V_{ON}$ <1.5 V, $V_{IS}$ < $V_{OUT}$ -5 V, $V_{bIN}$ >4.5 V $^{9}$					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	IL = 20A, Tj = -40°C:		7400			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	•					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	IJ = +25°C: Ti = ±150°C:					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	•					
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	•			8600		
$I_{\text{IN}} = 0$ (e.g. during de-energising of inductive loads): n.a Sense current under fault conditions; $V_{\text{DS}} > 1.5 \text{V}$ , typ. $T_{j} = -40+150^{\circ}\text{C}$ : $I_{\text{IS},\text{fault}}$ 2.5 4 mA Fault-Sense signal delay after negative input slope $t_{\text{delay}(\text{fault})}$ 0.8 ms Current sense leakage current $I_{\text{IN}} = 0: \ I_{\text{IS}(\text{LL})} \qquad \qquad \qquad 0.5  \mu\text{A}$ $V_{\text{IN}} = 0, \ I_{\text{L}} = 0: \ I_{\text{IS}(\text{LH})} \qquad \qquad 4 \qquad 12$ Current sense settling time to $I_{\text{IS} \text{ static}} \pm 10\%$ after positive input slope, $I_{\text{L}} = 0   20  \text{A}  10)$ $T_{\text{j}} = -40+150^{\circ}\text{C}$ : $T_{\text{Son}(\text{IS})} \qquad \qquad  400  \mu\text{S}$ Overvoltage protection $I_{\text{bb}} = 15  \text{mA}$ $T_{\text{j}} = -40+150^{\circ}\text{C}$ : $V_{\text{blS}(Z)} \qquad 61  68   V$ Input Required current capability of input switch $T_{\text{j}} = -40+150^{\circ}\text{C}$ : $I_{\text{IN}(\text{on})} \qquad \qquad 0.7  1.2  \text{mA}$	Tj = +25°C:			8600		
Sense current under fault conditions; $V_{DS}>1.5V$ , typ. $T_j=-40+150^{\circ}C$ : $I_{IS,fault}$ 2.5 4 mA Fault-Sense signal delay after negative input slope $t_{delay(fault)}$ 0.8 ms Current sense leakage current $I_{IN}=0$ : $I_{IS(LL)}$ 0.5 $\mu$ A $V_{IN}=0$ , $I_{L}=0$ : $I_{IS(LH)}$ 4 12 Current sense settling time to $I_{IS}$ static±10% after positive input slope, $I_{L}=0$ $\subseteq$ 20 A $=$ 20 A $=$ 20 A $=$ 30 $=$ 400 $=$ 400 $=$ 50 $=$ 50 $=$ 61 $=$ 68 $=$ 70 $=$ 68 $=$ 70 $=$ 69 $=$ 69 $=$ 69 $=$ 69 $=$ 69 $=$ 69 $=$ 69 $=$ 69 $=$ 69 $=$ 69 $=$ 60 $=$ 60 $=$ 70 $=$ 60 $=$ 70 $=$ 60 $=$ 70	$T_{j} = +150^{\circ}C$ :		6800	8600	10500	
$V_{\rm DS}$ >1.5V, typ. $T_{\rm j}$ = -40+150°C: $I_{\rm lS,fault}$ 2.5 4 mA Fault-Sense signal delay after negative input slope $t_{\rm delay(fault)}$ 0.8 ms Current sense leakage current $I_{\rm lN}$ = 0: $I_{\rm lS(LL)}$ 0.5 μA $V_{\rm lN}$ = 0, $I_{\rm lS(LL)}$ 4 12 Current sense settling time to $I_{\rm lS static}$ ±10% after positive input slope, $I_{\rm L}$ = 0 $\int$ 20 A 10 $t_{\rm lS(LL)}$ 400 μs $T_{\rm j}$ = -40+150°C: $T_{\rm lS(LL)}$ 61 68 V Input Required current capability of input switch $T_{\rm j}$ =-40+150°C: $T_{\rm lN(on)}$ 0.7 1.2 mA	$I_{IN} = 0$ (e.g. during de-energising of inductive loads):			n.a.		
Fault-Sense signal delay after negative input slope $t_{\text{delay(fault)}}$ 0.8 ms Current sense leakage current $t_{\text{IN}} = 0$ : $t_{\text{IS(LL)}}$ 0.5 $t_{\text{IN}} = 0$ . $t_{\text{IS(LL)}}$ 4 12 $t_{\text{IS(LH)}}$ Current sense settling time to $t_{\text{IS static}} \pm 10\%$ after positive input slope, $t_{\text{L}} = 0$ $t_{\text{IS}} = -40 \pm 150$ °C: $t_{\text{Son(IS)}}$ 400 $t_{\text{IS}} = -40 \pm 150$ °C: $t_{\text{IS}} = -40 \pm 150$ °C: $t_{\text{IN}} = -40 \pm 150$ °C	Sense current under fault conditions;					
Current sense leakage current $I_{\text{IN}} = 0: \ I_{\text{IS(LL)}} \qquad \qquad \qquad 0.5 \qquad \mu\text{A}$ $V_{\text{IN}} = 0: \ I_{\text{IS(LH)}} \qquad \qquad 4 \qquad 12$ Current sense settling time to $I_{\text{IS static}} \pm 10\%$ after positive input slope, $I_{\text{L}} = 0   20  \text{A}  10)$ $T_{\text{j}} = -40 + 150^{\circ}\text{C}:$ Overvoltage protection $I_{\text{bb}} = 15 \text{ mA} \qquad T_{\text{j}} = -40 + 150^{\circ}\text{C}: \qquad V_{\text{blS(Z)}} \qquad 61 \qquad 68 \qquad \qquad V$ Input Required current capability of input switch $T_{\text{j}} = -40 + 150^{\circ}\text{C}: \qquad I_{\text{IN(on)}} \qquad \qquad 0.7 \qquad 1.2  \text{mA}$	$V_{DS}$ >1.5V, typ. $T_{j}$ = -40+150°C:	I <sub>IS,fault</sub>	2.5	4		mA
$I_{\text{IN}} = 0: \ I_{\text{IS(LL)}} \qquad \qquad \qquad 0.5 \qquad \mu\text{A}$ $V_{\text{IN}} = 0, \ I_{\text{L}} = 0: \qquad I_{\text{IS(LH)}} \qquad \qquad 4 \qquad 12$ Current sense settling time to $I_{\text{IS static}} \pm 10\%$ after positive input slope, $I_{\text{L}} = 0  \boxed{}  20  \text{A}  {}^{10} \qquad t_{\text{son(IS)}} \qquad \qquad \qquad 400 \qquad \mu\text{s}$ $T_{\text{j}} = -40 + 150^{\circ}\text{C}: \qquad V_{\text{bIS(Z)}} \qquad 61 \qquad 68 \qquad \qquad V$ $\boxed{\text{Input}}$ Required current capability of input switch $T_{\text{j}} = -40 + 150^{\circ}\text{C}: \qquad I_{\text{IN(on)}} \qquad \qquad 0.7 \qquad 1.2  \text{mA}$	Fault-Sense signal delay after negative input slope	<i>t</i> delay(fault)			0.8	ms
$V_{\text{IN}} = 0. \ I_{\text{IS(LH)}}$ $V_{\text{IS(LH)}}$ $V_{I$	Current sense leakage current					
Current sense settling time to $I_{IS \text{ static}} \pm 10\%$ after positive input slope, $I_L = 0 \ \Box \ 20 \ A^{-10)}$ $T_{j=} -40 + 150^{\circ}\text{C}$ :  Overvoltage protection $I_{bb} = 15 \ \text{mA}$ $I_{j=} -40 + 150^{\circ}\text{C}$ : $I_{IN(on)}$ Required current capability of input switch $I_{T_j} = -40 + 150^{\circ}\text{C}$ : $I_{IN(on)}$ $I_{$	$I_{\text{IN}} = 0$ :	I <sub>IS(LL)</sub>				μΑ
positive input slope, $I_L = 0  extstyle 20  extstyle A  extstyle 100  extstyle T_{j=}  extstyle -40 +150  extstyle C: T_{j=}  extstyle -40 +150$	$V_{1N} = 0, I_{L} = 0$	I <sub>IS(LH)</sub>		4	12	
positive input slope, $I_L = 0  extstyle 20  extstyle A  extstyle 100  extstyle T_{j=}  extstyle -40 +150  extstyle C: T_{j=}  extstyle -40 +150$	Current sense settling time to I <sub>IS static</sub> ±10% after					
$T_{j} = -40+150^{\circ}\text{C}:$ Overvoltage protection $I_{bb} = 15 \text{ mA}$ $T_{j} = -40+150^{\circ}\text{C}:$ $V_{bIS(Z)}$ 61 68 V  Input  Required current capability of input switch $T_{j} = -40+150^{\circ}\text{C}:$ $I_{IN(on)}$ 0.7 1.2 mA	<u> </u>	t <sub>son(IS)</sub>			400	μs
Overvoltage protection $I_{bb} = 15 \text{mA}$ $T_j = -40+150^{\circ}\text{C}$ : $V_{bIS(Z)}$ 61 68 V  Input  Required current capability of input switch $T_j = -40+150^{\circ}\text{C}$ : $I_{IN(on)}$ 0.7 1.2 mA	· · · · -	,				•
$I_{bb} = 15  \text{mA}$ $T_j = -40+150^{\circ}\text{C}$ : $V_{bIS(Z)}$ 6168VInputRequired current capability of input switch $T_j = -40+150^{\circ}\text{C}$ : $I_{IN(on)}$ 0.71.2mA	·					
Input  Required current capability of input switch $T_j = -40+150$ °C: $I_{IN(on)}$ $T_j = -40+150$ °C: $I_{IN(on)}$	$I_{\rm bb} = 15 \mathrm{mA}$ $T_{\rm i} = -40 + 150 ^{\circ}\mathrm{C}$ :	$V_{\text{bIS}(Z)}$	61	68		V
Required current capability of input switch $T_j = -40+150$ °C: $I_{IN(on)}$ 0.7 1.2 mA		~.~(=/			<u> </u>	
$T_{\rm j}$ =-40+150°C:	Input					
T <sub>j</sub> =-40+150°C:		I <sub>IN(on)</sub>		0.7	1.2	mA
Maximum input current for turn-off $T_j$ =-40+150°C: $I_{IN(off)}$ 50 $\mu$ A						
	Maximum input current for turn-off $T_j$ =-40+150°C:	I <sub>N(off)</sub>			50	μΑ

 $<sup>^{9)}</sup>$  If  $V_{ON}$  is higher, the sense current is no longer proportional to the load current due to sense current saturation.

<sup>&</sup>lt;sup>10</sup>) not subject to production test, specified by design

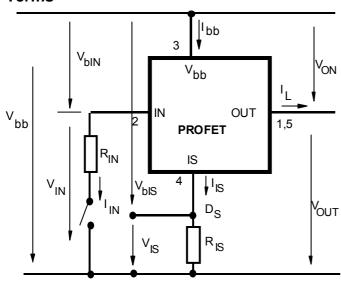


# **Truth Table**

	Input Current	Output	Current Sense
	level	level	lis
Normal	L	L	0
operation	Н	Н	nominal
Overload	L	L	0
	Н	Н	I <sub>ISfault</sub>
Short circuit to GND	L	L	0
	Н	L	I <sub>ISfault</sub>
Overtemperature	L	L	0
	Н	L	I <sub>ISfault</sub>
Short circuit to Vbb	L	Н	0
	Н	Н	<nominal<sup>11</nominal<sup>
Open load	L	Z	0
	Н	Н	0

L = "Low" Level H = "High" Level Z = high impedance, potential depends on external circuit

#### **Terms**

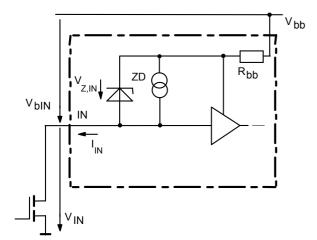


Two or more devices can easily be connected in parallel to increase load current capability.

<sup>11)</sup> Low ohmic short to  $V_{\rm bb}$  may reduce the output current  $I_{\rm L}$  and therefore also the sense current  $I_{\rm IS}$ .



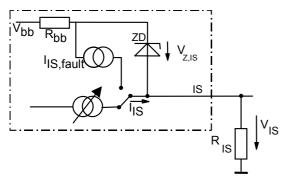
### Input circuit (ESD protection)



ESD-Zener diode: 68 V typ., max 15 mA;

### **Current sense output**

Normal operation

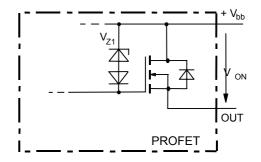


 $V_{\rm Z,IS} = 68\,{\rm V}$  (typ.),  $R_{\rm IS} = 1\,{\rm k}\Omega$  nominal (or  $1\,{\rm k}\Omega$  /n, if n devices are connected in parallel).  $I_{\rm S} = I_{\rm L}/k_{\rm ilis}$  can be only driven by the internal circuit as long as  $V_{\rm out}$  -  $V_{\rm IS} > 5{\rm V}$ . If you want to measure load currents

up to 
$$I_{\rm L(M)}$$
, R<sub>IS</sub> should be less than  $\frac{V_{bb}$  -  $5V}{I_{L(M)}$  /  $K_{ilis}$ 

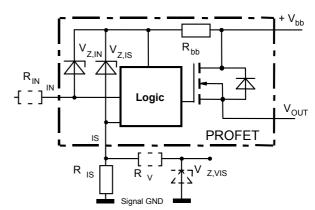
Note: For large values of  $R_{\rm IS}$  the voltage  $V_{\rm IS}$  can reach almost  $V_{\rm bb}$ . See also overvoltage protection. If you don't use the current sense output in your application, you can leave it open.

#### Inductive and overvoltage output clamp



 $V_{ON}$  is clamped to  $V_{ON(Cl)} = 42 \text{ V typ.}$ 

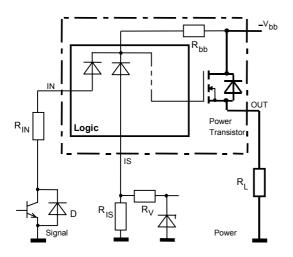
## Overvoltage protection of logic part



 $R_{bb}$  = 200  $\Omega$  typ.,  $V_{Z,IN}$  =  $V_{Z,IS}$  = 68 V typ.,  $R_{IS}$  = 1 k $\Omega$  nominal. Note that when overvoltage exceeds 73 V typ. a voltage above 5V can occur between IS and GND, if  $R_{V},\,V_{Z,VIS}$  are not used.



### Reversave™ (Reverse battery protection)



 $R_V \ge 1 k\Omega$ ,  $R_{IS} = 1 k\Omega$  nominal. Add  $R_{IN}$  for reverse battery protection in applications with V<sub>bb</sub> above 16V;

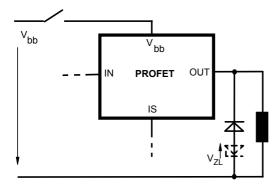
recommended value: 
$$\frac{1}{R_{\text{IN}}} + \frac{1}{R_{\text{IS}}} + \frac{1}{R_{\text{V}}} = \frac{0.05A,}{\mid V_{bb} \mid -12V}$$

To minimise power dissipation at reverse battery operation, the summarised current into the IN and IS pin should be about 50mA. The current can be provided by using a small signal diode D in parallel to the input switch, by using a MOSFET input switch or by proper adjusting the current through  $R_{\rm IS}$  and  $R_{\rm V.}$  Since the current through  $R_{\rm bb}$  generates additional heat in the device, this has to be taken into account in the overall thermal considerations.

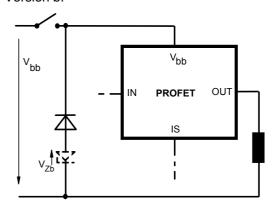
# V<sub>bb</sub> disconnect with energised inductive load

Provide a current path with load current capability by using a diode, a Z-diode, or a varistor. ( $V_{ZL}$  < 73 V or  $V_{Zb}$  < 30 V if R<sub>IN</sub>=0). For higher clamp voltages currents at IN and IS have to be limited to 250 mA.

Version a:



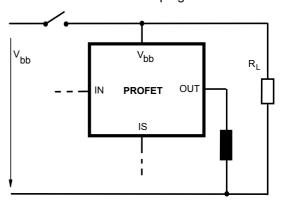
#### Version b:



Note that there is no reverse battery protection when using a diode without additional Z-diode  $V_{ZL},\,V_{Zb}.$ 

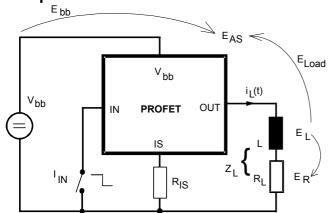
#### Version c:

Sometimes a necessary voltage clamp is given by non inductive loads  $R_{L}$  connected to the same switch and eliminates the need of clamping circuit:





# Inductive load switch-off energy dissipation



Energy stored in load inductance:

$$E_L = \frac{1}{2} \cdot L \cdot I_L^2$$

While demagnetising load inductance, the energy dissipated in PROFET is

$$E_{AS} = E_{bb} + E_L - E_R = V_{ON(CL)} \cdot i_L(t) dt$$

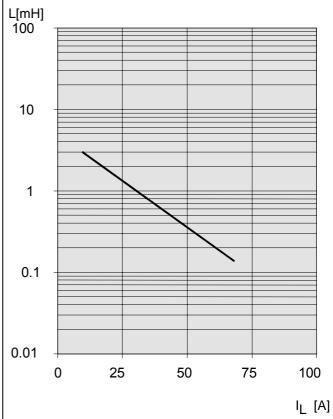
with an approximate solution for  $R_L > 0\,\Omega$ :

$$E_{AS} = \frac{I_L \cdot L}{2 \cdot R_L} (V_{bb} + |V_{OUT(CL)}|) ln (1 + \frac{I_L \cdot R_L}{|V_{OUT(CL)}|})$$

The device is not suitable for permanent PWM with inductive loads if active clamping occurs every cycle.

# Maximum allowable load inductance for a single switch off

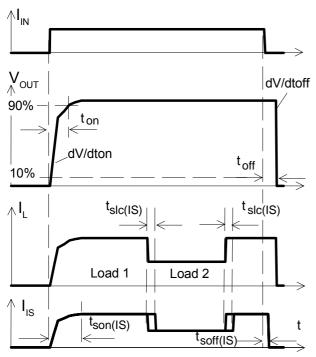
$$L = f(I_L)$$
; T<sub>j,start</sub> = 150°C, V<sub>bb</sub> = 12 V, R<sub>L</sub> = 0  $\Omega$ 





# **Timing diagrams**

**Figure 1a:** Switching a resistive load, change of load current in on-condition:



The sense signal is not valid during a settling time after turn-on/off and after change of load current.

Figure 1b: typical behaviour of sense output:

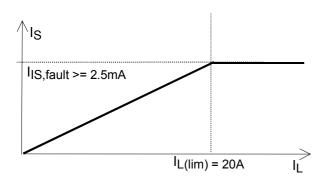
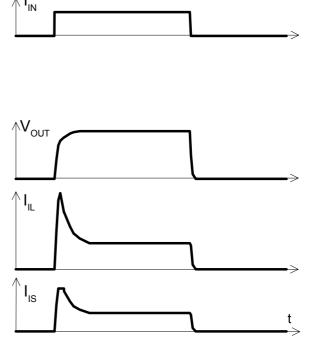


Figure 2a: Switching motors and lamps:



Sense current above I<sub>IS,fault</sub> can occur at very high inrush currents.

Figure 2b: Switching an inductive load:

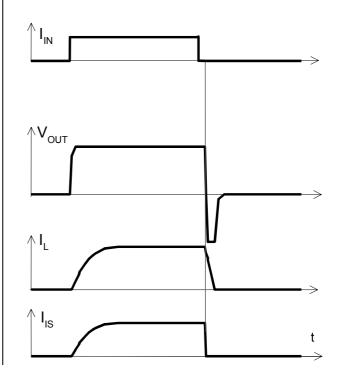
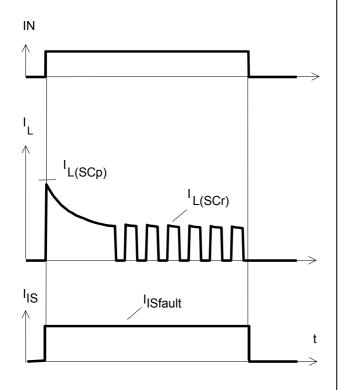
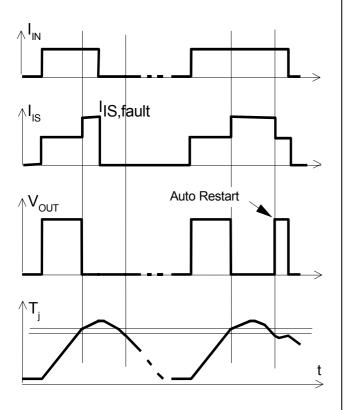




Figure 3a: Short circuit:



**Figure 4a:** Overtemperature Reset if  $T_j < T_{jt}$ 



**Figure 5a:** Undervoltage restart of charge pump, overvoltage clamp

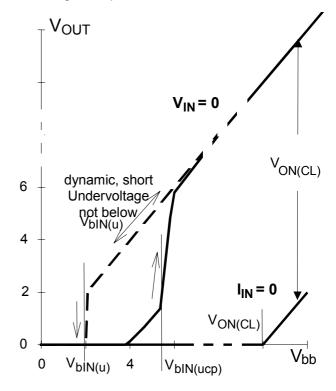




Figure 6a: Current sense versus load current:

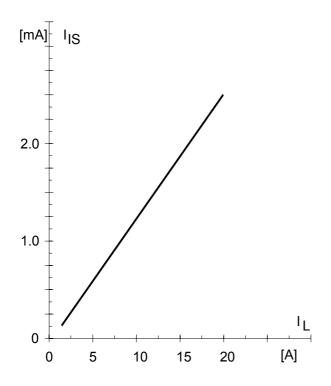
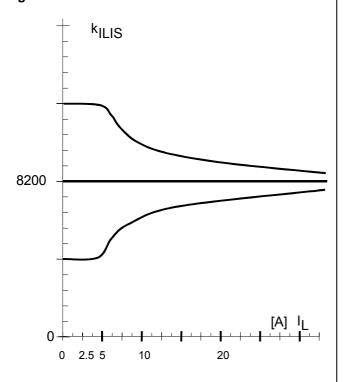
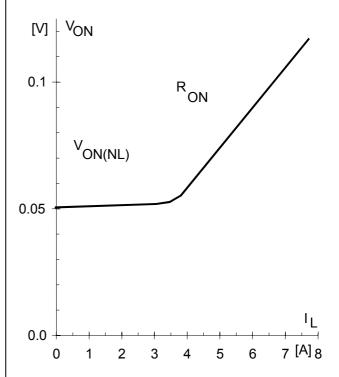


Figure 6b: Current sense ratio<sup>12)</sup>:



 $<sup>^{12\,)}</sup>$  This range for the current sense ratio refers to all devices. The accuracy of the  $k_{\scriptscriptstyle \rm ILIS}$  can be raised by means of calibration the value of  $k_{\scriptscriptstyle \rm ILIS}$  for every single device.

Figure 7a: Output voltage drop versus load current:



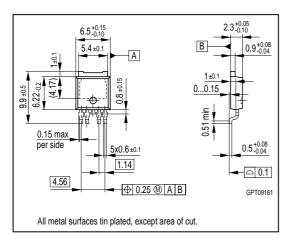


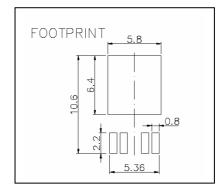
# Package and Ordering Code

All dimensions in mm

D-Pak-5 Pin: TO-252-5-1

Sales Code	BTS443P
Ordering code	Q67060-S7404-A 2





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